Thomas Elmer his Book The SEAMAN's Thomas Elm The SI Daily Assistant, Febres

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A Short, Easy, and Plain Method OF KEEPING

A JOURNAL at SEA;

In which are contain'd

RULE S, RULL Meu SHEWING

How the Allowances for Lee-way, Variation, Heave of the Sea, Set of Currents, &c. are to be made, and to Correct the Dead - Reckoning by an Observation, in all Cases: And also all the TABLES that are any ways necessary for the SEAMAN'S Use in keeping a Journal.

By THOMAS HASELDEN, Late Teacher of the MATHEMATICKS in the ROYAL-NAVY.

LONDON:

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TOTHE

READER.



AVING been educated in the Theory of Navigation, almost from my Childhood, and baving had about Sixteen Years Experience of the practical Part (at Sea) both in the Merchants Service, and also as Teacher of the Mathematicks in the Royal-Navy; and having in the

Course of that Time made a general Observation, that there are Numbers of Seamen who would gladly keep a Reckoning, had they any Short, Easy, and Plain Method to do it by, but are deterr'd from it by the want of such a Thing: And also that there are many who have thrown their Money away to little or no Purpose, by going to School to some Masters (of which Sort there are too many) that they have only got a Smattering of the Theory, and a few Terms of Art by Rote, which enables them to talk in such a manner to deceive those that go to learn of them; by having never been at Sea, cannot know any Thing of the Practice.

Therefore for the Use of such in particular, and of all other Seafaring Men in general, I have written the following Treatise, in which I think I have inserted all the Rules, and all the Tables with their Uses, that are necessary to be used in any Case at Sea: And also particular Rules for keeping a Journal, swith the manner of Correcting the Dead-Reckoning by an Observation, either for one Day, or for a longer Time; the first of which, viz. Correcting for one Day, has been treated of by several Authors; but the latter, viz. Correcting for a longer Time; I know has been barely mentioned in several, but not particularly explain'd in any Author at all I believe, at least in none that I have

Read,

To the READER.

Read; And for that Reason I have done it in the Journal at the latter end of this Book, it being absolutely necessary for every Man that keeps a Reckoning to know it, because they are more likely to be out in their Reckoning, when they have been some Days without an Observation, then when they have one every Day, and consequently more likely to have Occasion to correct for three or four Days, than for a single One.

I have not begun this Book with Arithmetic, as most of the Books on this Subject do, because I think, that if any Person has had so little Education as not to be capable of Adding, Subtracting, Multiplying and Dividing, he will hardly be able to make any Progress, either in Arithmetic or Navigation, by the help of Books alone, without the Assistance of a Master (so that I think putting such Things into Books of this kind, serve only to enhance the Price, and are of no Service to the Reader.) And now having given an Account of the Reasons that enduced me to publish this Book (which I hope, and are pretty well assured, will be found the most useful Book of its kind, now in Print) for the daily Practice at Sea, I have nothing more to add, but to beg the Readers kind Acceptance of my Endeavours.

And am,

Their humble Servant,

Thomas Haselden.



THE

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TABLE

OF

DIFFERENCE of LATITUDE

AND

DEPARTURE

To every Single DEGREE,

And as far as 300 Miles DISTANCE.

7. T *** Difference of Latitude and Departure for 1 Deg.

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40 40.0 00 7 90 90.0 21.6 4c 142 0 02.4 90 100 0 03 7 4c 240.0 04.1 90 290.0 05.0 11.0 00.7 91 91.0 01.6 141 141.0 02.4 191 191.0 0 0.3 3 141 241.0 04.1 191 291.0 05.0 142 142.0 02.5 92 192.0 03.3 42 242.0 04.2 92 292 0 05.0 143 143.0 02.5 93 193 0 03.3 43 243.0 04.2 93 293.0 05.0 144 144.0 02.5 94 194.0 03 3 142 144.0 04.2 94 294 0 05.0 145 145.0 02.5 94 194.0 03 3 142 144.0 04.2 94 294 0 05.0 145 145.0 02.5 95 195 0 03.4 145 245.0 04.2 95 295.0 05.1 17 17.0 00.8 96 96.0 01.7 146 146.0 02.5 97 197.0 03.4 146 246 0 04.2 126 296.0 05.1 147 147.0 00.8 97 97.0 01.7 147 147.0 02.5 97 197.0 03.4 147 247.0 04.2 97 297.0 05.1 148 148.0 02.6 98 198.0 03.4 140 148.0 04.3 98 298.0 05.1 149.0 00.9 95 99.0 01.7 146 149.0 02.6 98 198.0 03.4 140 148.0 04.3 98 298.0 05.1 149.0 00.9 95 99.0 01.7 150 150.0 02.6 100 120.0 03.4 149 149.0 04.3 99 299.0 05.1 150.0 02.6 100 120.0 03.4 149 149.0 04.3 99 299.0 05.1 150.0 02.6 100 120.0 03.4 149 149.0 04.3 99 299.0 05.1 150.0 02.6 100 120.0 03.4 150 120.0 04.3 100.0 05.2	7.3			110			6 39	139,	0 02.4	1 8						8	9 289	0 05.	0
41 11.0 00.7 91 91.0 01.6 141 141.0 02.4 191 191.0 03.3 241 241.0 04.1 191 291.0 05.0 42 42.0 00.7 92 92.0 01.6 42 142.0 02.5 92 192.0 03.3 42 242.0 04.2 92 292 0 05.0 44 44.0 00.8 94 94.0 01.6 44 144.0 02.5 94 194.0 03.3 44 244.0 04.2 94 294 0 05.0 45 45 60.0 00.8 95 95.0 01.7 45 145.0 02.5 95 195.0 03.4 45 245.0 04.2 95 295.0 05.1 46 46.0 00.8 96 96.0 01.7 146 146.0 02.5 97 197.0 03.4 246 04.2 95 295.0 05.1 47 47.0 00.8 97 97.0 01.7 47 147.0 02.5 97 197.0 03.4 47 247.0 01.2 97 297.0 05.1 48 48.0 00.8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 46 246.0 04.3 98 298.0 05.1 49 49.0 00.9 95 99.0 01.7 46 149.0 02.6 98 198.0 03.4 46 248.0 04.3 98 298.0 05.1 99.0 00.7 100.0 01.7 150.0 02.6 99 199.0 03.4 45 249.0 04.3 99 299.0 05.1 50.0 00.0 01.7 150.0 02.6 100 200.0 03.4 250 250.0 04.3 300 300.0 05.2			000					140	0 02.4	11 9	0 100	0 03	4	240.	004.1	9	0 290.	0 05.	0
42 42.c 00,7 92 92.c 01.6 42 142.0 02.5 92 192.0 03.3 42 242.0 04.2 92 292 0 05.c 43 43.c 00,8 93 93.c 01.6 43 143.0 02.5 93 193 0 03.3 43 243.0 04.2 93 293.0 05.0 44 44.c 00,8 94 94.0 01.6 44 144.0 02.5 94 194.0 03 3 44 244.0 04.2 94 294 0 05.c 45 45 0 00 8 95 95.0 01.7 45 145.0 02.5 95 195 0 03.4 45 245.0 04.2 95 295.0 05.3 46 46.0 00,8 96 96.0 01.7 146 146.0 02.5 95 195 0 03.4 45 245.0 04.2 95 295.0 05.3 47 47.0 00.8 97 97.0 01.7 47 147.0 02.5 97 197.0 03.4 47 247.0 01.2 97 297.0 05.1 48 48.c 00 8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 47 247.0 01.2 97 297.0 05.1 49 49.0 00,9 95 99.0 01.7 46 149.0 02.6 99 199.0 03.4 49 249.0 04.3 98 298.0 05.1 50.0 00.0 01.7 150.0 02.6 100 20.0 03.4 250 250.0 04.3 300 300.0 05.3					-	_		1 141.	02.4	1 19	1 191	00,0	1 24	1 241.	0 04.	1 29	J 201.	0 05.	c
43 43.0 00,8 93 93.0 01.6 43 143.0 02.5 93 193 0 03,2 43 243.0 04.2 93 293.0 05.0 44 44.0 00.8 94 94.0 01.6 44 144.0 02.5 94 194.0 03 3 44 244.0 04.2 94 294 0 05.0 45 45 00.8 95 95.0 01.7 45 145.0 02.5 95 195 0 03.4 45 245.0 04.2 95 295.0 05.3 46 46.0 00.8 96 96.0 01.7 146 146.0 02.5 97 197.0 03 4 47 247.0 04.2 196 296.0 05.1 47 47.0 00.8 97 97.0 01.7 47 147.0 02.5 97 197.0 03 4 47 247.0 04.2 97 297.0 05.1 48 48.0 00.8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 46 248.0 04.3 98 298.0 05.1 49 49.0 00.9 95 99.0 01.7 46 149.0 02.6 99 199.0 03 4 46 248.0 04.3 99 299.0 05.1 50.0 00.0 01.7 100 150.0 02.6 200.0 03.4 250 250.0 04.3 300 300.0 05.2										5 9	2 192	0 03.	4	- 4					
44 44.c cc,8 94 94.0 01.6 44 144.0 02.5 94 194.0 03 3 44 244.0 04.2 94 294 0 05.c 45 45 c oo 8 95 95.0 01.7 45 145.0 02 5 95 195 0 03.4 45 245.0 04.2 95 295.0 05.3 46 46.0 00.8 96 96.0 01.7 146 146.0 02.5 97 197.0 03 4 47 247.0 04.2 97 297.0 05.1 48 48.c oo 8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 47 247.0 04.2 97 297.0 05.1 49 49.0 00.9 95 99.0 01.7 46 149.0 02 6 99 199.0 03 4 46 248.0 04.3 98 298.0 05.1 50.0 00.0 01.7 100 150.0 02.6 200.0 03.4 250 250.0 04.3 300 300.0 05.2					3 93	0 01.		3 143.	0 02.	5 9						9			
45 45 c 00 8 95 95 0 01,7 45 145,002 5 95 195 0 03.4 45 245 0 04.2 95 295 0 05.3 46 46.0 00,8 96 96.0 01.7 146 146.0 02.5 196 196.0 03.4 146 246 0 04.2 1296 296,0 05.3 47 47.0 00.8 97 97.0 01.7 47 147.0 02.5 97 197.0 03.4 47 247.0 04.2 97 297.0 05.3 48 48.0 00 8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 46 248.0 04.3 98 298.0 05.3 49 49,0 00,9 95 99.0 01.7 46 149.0 02 6 99 199.0 03.4 46 248.0 04.3 99 299.0 05.3 50.0 00,0 16c 100.0 01.7 100 150.0 02.6 100 200.0 03.4 250 250.0 04.3 300 300.0 05.3					4 94	.10 0.	6 4	144	002.	5 9									
46 46.0 00,8 96 96.0 01.7 146 146.0 02.5 196 196.0 03.4 146 246 0 04.2 296 296,0 05.1 17 47.0 00.8 97 97.0 01.7 47 147.0 02.5 97 197.0 03.4 47 247.0 04.2 97 297.0 05.1 48 48.0 00 8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 46 248.0 04.3 98 298.0 05.1 49 49,0 00,9 95 99.0 01.7 46 149.0 02.6 99 199.0 03.4 46 249.0 04.3 99 299.0 05.1 50.0 00.0 01.7 100 150.0 02.6 200.0 03.4 250 250.0 04.3 300 300.0 05.2	4				5 95	001,	7 4	5 145,	0 02	5 9	5 195	003.	4	5 245	04	2 9	5 295	0 05	3
17 47.0 00.8 97 97.0 01.7 47 147.0 02.5 97 197.0 03 4 47 247.0 01.2 97 297.0 05.1 48 48.0 00 8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 46 248.0 04.3 98 298.0 05.1 49 49.0 00.9 95 99.0 01.7 49 149.0 02 6 99 199.0 03 4 49 149.0 04.3 99 299.0 05.7 50.0 00.0 00.0 150.0 02.6 100 200.0 03.4 250 250.0 04.3 300 300.0 05.3				-11-		-		6 146.	0 02.	5 19	5 196	.003.	4 34	6 246	c 04.	2 29	6 296	0 05	1
48 48.c 00 8 98 98.0 01.7 48 148.0 02.6 98 198.0 03.4 42.48.c 04.3 98 298.0 05.1 49 49.0 00.9 95 99.0 01.7 46 149.0 02 6 99 199.c 03 4 49 149.c 04.3 99 299.0 05.1 52 50.c 00.9 18c 100.0 01.7 1 50 150.0 02.6 10c 200.0 03.4 250 250.c 04.3 300 300.0 05.3										5 9	7 197	.003	4 4						
49 49,0 00,9 95 99.0 01.7 4¢ 149.0 02 6 99 199.0 03 4 49 149.0 04.3 99 299.0 05.1 52 50.0 00,9 100 100.0 01.7 100 150.0 02.6 200.0 03.4 250 250.0 04.3 300 300.0 05.3		8 48	.c 00	8 9				8 148	.0 02,	6 9							8 298	0 05	1
50 (0.0,0,0) 100 100.0 01.7 100 150.0 02.0 100 200.0 03.4 250 250.0 04.3 300 300.0 05.3						.0 01	7 4	9 149	.0 02	6 9									
					100	.001	7 15	0 150	.0 02.	6 20							300	0 05	.2
					iff D	er La	t D	A D	e La	10	A D	et L	O	filDer	D L3	t D	ift De	0	14
	11-			!		-						- 1	40			1. 10	*****		1



for 89 Deg

10.F32.93.93.858.858.85.85

Difference of Latitude and Departure for 2 Deg.

n A	Lat	Deil	Dif	Lat	Deil	Dift	Lat	De 1	Dif	Lat	De. 1	IDit	itLat.	De;	(Did	Lat	Dep
-	-	00,0	51	51.0	-	101	100.9	03.5	-	150.9		-	200 9	-	-		08 8
1 2	02.0		52	52 0	01.8	02	101.9		7.0	151,9		01					08.8
3	03.0	00.1		53.0	C1 8	03	102.9		1.0	152 5		0			53	252 8	08 9
4	24 0		54	54 0	01.9	04	103.9			153.5		04				253 8	08 9
_5	-	00 2	55	55,0	01.9	05	104.9		55	154.9	_	0		-		254.8	-
6		00°2	56	56.0	02.0	lot 07	105.9		15t	155,9		200			255	255.8	09 0
7		20.3	58	57.0	02.0		107.9	450		157,9			207.9			257.8	09 0
9		00.3		590	02.1	09	108 9			158 9		0	1 0		59	258 8	09.1
10	10,0	00 4	6c	60.0	02.1	10	109 9	039	ÓC.	159.4	05:6	10			60	259.8	09.1
11	11.0	00.4	61	61.0	C2 1	111	110.9			150 9		21				260 8	09.1
12		00,	63	62.0	02.2	12	111.9		62	161 9	05.7	1		07.4		261.8	09.2
13		00 5		610	03 2	13	113 9			163 9		1		07.5		263 8	09.2
14	1	00 5		65.0	U2 3	15	1149			164.9		1		07.5		264.8	00.3
15	-	00 6	-	_	02.3	116	115 9	C4 1	16t		_	2.1			266	26; 8	09.3
17	1	00.E	67	67 0	02 3		116 9			166 9	05.8	1	216.4	07.6		266 8	09.3
18		09.6		1.			117.9			167.9		1				267 8	9 4
19	1	00.7		69.0		19	118.9		69			1				268.8	1
20	-	00,7	70	-	02,4		119 9	-	70	-	06 0	20	_	07.7	-		09.5
21		00.7	71	71.0	02.5	121	121.9		72		66.0	22	The state of the s	27.8	72	270 8	09.5
23		00.8	73		02.5	23	122.5		73			1 2		07.8	73		1.000
24	24.0	00.8	74		02.6	24	1239	24.3	74	173.9	06.1	2	-	c7.8	74	273.8	
25	250	00 (75		02.6	25	124.9	04 4	75			2	5 224.	27.9	75		
26	26,0	00,9	76			126	125.9		176			22				275.8	
27		00.9	77 78		02.7	27	120.9	04 4		177.9	06.2	2 2		07.9		274,8	
28	to the same	01,0	79			29		04.5		178.9		2	0	08 0		278.8	09.7
30		01.1	80			30			110		06.3	3		08.1		279.8	09,8
31	-	01.1	81	81.0	02.8	131	130 9	04 6	181	180.0	06.3	23		08.1	281	28c.8	09 8
32		01.1	82				131 9	04.6	82	181.	06.4	3	2 2314	08.1		281.8	1 0 01
1 33		012	83			11	132,9	2. 2.	83		06.4	3		08.9		282.8	1 00
34		01.2	84	83,9	02,9	34	133 9	1. 1. 1.	84			3		08.2		283.8	
35		01.2	86	_		35		-	186	-		23		08.3	-	2858	
36		01.3	10			136	136.9			186.9	06.5	3	7 236	08.3		286.8	
37		01.3	88	87.9	03.1	38	137 9	04.8	88	187 9	06.6	3	8 237.	08.3	88	287.8	10.1
39	39.0	01.4	1 80	185 0	107 1	1 20	138 6	04.9	89	188.9	00,6	3	9 238	08.4	89	288 8	10 1
40	40 0	014	90	89 9	03.1	40	139,9			189 9				08.4		289 8	-
41	410	01 4	91	90.9	03.2	141	140 9		191	190 9	06.7	24		08.4		290.8	
42	42 0	01,5				42	141.9	05.0	92	191.9	06.8	1		08.5		291.8	
43	43.c 44.0	01.5	93		03.2	44	143.9	05.0	93	193 9	66.8	4		08.5		293.8	
45	450	01.6	95		03.3	45	144 9		95	194.9	06,8	4		08.6		294.8	
	46.0				03 4		145,5	05.1	196	195 9		24	6 245.	08.6	196	295.8	10.4
47	47.0	01.6	97	96.9	03.4	47	146.9	05.1	97	196.9	00,9	4	7 246.	9 28,6	97	296,8	10.4
48	48.0	01.7	98	97-9	03.4		147.9		98	197.9	00.9	4	8 247.	08.7	98	297.8	
	49,0	01,7		98.9			148.9			198			9 248.			298.8	
	-				(at		Det			Dei			fluep			Dep	1 1
-	Dep	1-4		,De	al	- I			101	Del	1 Le	1	поер		1101		

Alba Comp				11.718		A long .	10 101					1	1241				
Dift	Lar	Del	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	De	Diff	Lat	Der	Dift	Lat	Dep
1	01.0	00.1	51	50.9	02:7	101	100.9	05.3	151	150.8	07.9	201	200.7	10,5	251	250.6	13.1
	:2.0		52	51 9			101.9			151.8	03.0		201.7			251.6	
3	030	00.2	53		02 8	03	102.9		53	152.8	08.0		202.7		53	252.6	13.2
4	04.0	1000	54		02.8		103.9			153.8	08 1		203.7		54	253 6	13.3
_5	05.0	00.3	55		02.9	05	104.9		55	154.8			204.7		-	254.6	
6	06.0	00 3	56		02.9		105.9		156	155.8			205.7		256	255.6	13.4
7	07.0		57		03.0		106.9		57	156.8			206.7			256.6	
8	€8.c		58		03.0		107,8			157.8			207.7			257.6	
9	09.c		59		03.1	09	108.8		59 60	158.8			208.7			258.6	
10	10,6	_	-		03.1	10		_					209.7	-		159.6	
11	11.0		61		03.2		110.8		161	160.8		1	210.7			260.6	
12	12.C		63		03,2	100	111.8			162.8		1	211.7	1.1		261.6	
13	13,0	00.7	64		03.3	13	113.8			163.8		:	212.7			262.6 263.6	
14	15.0	00.	65		03.4		114.8			164.8			214.7		- 1	264.6	
15				_	-		115.8			165.8	_				-		
16	16.0	100	67	65.9	03.5		1168			166.8		12	215.7	1.3		265.6 266.6	
17	18.0	-	68		03,6		117.8			167.8			217.7			267.6	
19	19.0		69		03.6		118.8		69	168.8	1	19	218.7	11.	- 1	268.6	
20	20.0		70	69.9	03.7	20	119	06.3	70	169.8	08.9		219.7			269.6	
21	21.0	01.1	71	70.9	03.7	121	120.8	26.3	171	170.8	00.0	221	220.7	11.6	-	270 6	
22	12.0		72		03.8	22	121.8			171.8			131.7			271.6	
23	23 0		73		03.8	23	122.8			172.8			222.7			272.6	
24	24.0		74		93.9	24	123.8			173.8			223.7		74	273.6	14.3
25	250	01.3	75	_	03.9	25	124.8		75	174.8	_	25	224.7	11.8	75	274.6	14.4
26	26.0	01.4	76		04 0	126	125.8		176	175.8			225.7		276	275.6	4.4
27	27.C				04 0	27	126,8			176.8			226.7			276.6	
28	28.0		78		04.1	28	127.8	06.8		177.8			127.7			277.6	
29	30.0		79 80		04.2	30	129.8		80	178.7			228.7			278.6 279.6	
30			81		04.2		130.8		181		-			_			
31	31.0				04.3	131	131.8	06 9		180.7	09.5		230.7			280.6 281.6	
32	33.0	01.7	83		04.3		132.8		83	182 7			231.7			282,6	
33	24.0	8.10	84		04.4	34	133.8		84	183.7			233.7			283.6	
35	35.€	31.8	85	84.9	04.4	35	134.8	07.1	85	184.7			234.7			284.6	
36		019	86	85.9	04.5	136	135.8	07.1	186	185.7	09.7		235.7		286	285.6	15.0
37	16.0	019			04.6	37	136.8	07.2	87	186.7	09.8		236.7			286.6	
38	37-9	02.0			04.6	38	137.8	C7.2	88	187.7	09.8	38	137-7			287.6	
39	38.9	02.0	89	88.9	04.7		138.1	07.3		188.7			238.7			288.6	
40	39,9	02.1			04.7	40		07.3	90	189 7	09,0	40	239 7	12.6	90	289.6	15.2
41	40.9	02.1	91	90.9	04.8	141	140.8	07.4		193.7			240.7			290.6	
42	41.9	02.2	92	91.9	04.8		141.8	07.4		191.7			241.7			291.6	
43	42.9	02.2		92.9	04.9	1 43	142.8	07.5		193.7			242.7		93	292.6	15.3
44	43.9	02.3	94	93.	05 0		144.	07.6		194.7			244.7			293.6 294.6	
45					05.0			07.6					-				
46		02.4		95.	05.1		146.	8 07.7	196	195.7	10.3	42	245.7		290	295.6	10.0
47	47.0	02.5	97	97.	05.1		147,	8 07.7		197.7			247.7			297.6	
49		02.6	99	98.	9 05.2	49	148.	8,07.8	99	198.7	10.4	49	248.7			298.6	
50		02,6	100	99.	9 05.2	150	149	8 07.9	200	199.7			249.7			299.	
	Dep						Dep	La	Dif	Dep	Lat	Dif	Dep	Li		Dep	
-		-	••			-	7 10 1		-			-		12.8	-		-

Difference of Latitude and Departure for 4 Deg.

Diff Lat De Diff, Lat Dep Diff Lat De Diff Lat De Diff Lat De Diff Lat	10-
1 01.0 00.1 51 50.9 03 6 101 100 8 07 0 151 150.6 10.5 201 200.5 14 0 251 250 4	
1 2.0 00.1 52 51 9 03.6 02 101 8 07 1 52 151.6 10.6 02 201.5 14.1 52 251.4	
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19	18.9			68.7		19	118.5	10.4		168.4		19	218.2	19.1	69	268.c	23.4
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21	20.9	01.8	73	70.7	06.2	121	120,5	10.5	171	170.4	14.9	221	220.2	19.2	271	270.0	23.6
22	21.9	01.9		71.7	06,3	22	121.5	10.6	72	171.3	15,0	22	221.2	19.3		271.0	
23	22.5	02.0	73	72.7	06,4	23	122.5		73	172.3	15,1	23	222.2	19.4	73	272.0	23.8
24	23.9		74	73.7		24	123.5			173.3		24	223.1	19.5	74	273.0	
25	24 9	02.2	75	74.7	06.5	25	124.5	10 9	75	174.3	15.2	25	224.1	19.6	75	274.0	23.9
26	25 9		76	75,7	06.6	126	125.5			175.3			225,1		276	275 0	24.0
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39	38.9	03.3	80	88.7	07.8	30	138 5	12.7	80	188.3	16.4		238.1		89	286,9 287.9	25.1
40	39.8		90	89,7	07.8	40	139 5		90	189.3	16 5		239 1		90	288.9	25.2
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42	41.8			31.6			141.5		92	191.3	16.7		241.1		92	289.9 190.9	25.3
	42.8			92.6			142.5		93	192.3	16.8		242.1		93	291.9	25.5
	43.8		94	93.6	08.2	44	143.5	12.5	94	193.3	16.9		243.1			292.9	
	44,8	03.9	95	94,6	08.3	45	144.4	12.6	95	194.3	17.0	45	244.1		95	293-9	
	45.8			95.6			145.4			195.3			245.1			294,9	
47	46.8		97	96.6	08.5	47	146.4	12.8		196,3			246.1			295.9	
48	47.8	04.2		97.6			147.4		98	197:2	17.2		247.1			296.9	
49	48.8	04,3	99	98.6	08.6	49	148 4	13.0	99	198.2	17:3	49	248.7	21.7		297.9	16.0
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7	07.0				06.0	07	106.4	11.2	57	156.1	16.4	1	205.9		57 58	255.6	1
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13		01.5			06.7	14	113 4	11.9	64	163 1		14	212.8		64	262.5	
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10		01.7			06.9	116	115.4	12.1	166	165.1		-	214 8		266	264 5	
17		01.8			07.0	17	116 4		67	166,1			215.8			265.5	
1 18		01.9			07.1	18	117.4		68	187.1			216.8		68	266.5	28.0
19		32.0			07.2	19	118.3		69			19	217.8	22 9		267.	
20		02.1		69.6	07.3	20		100 -1	70	169 1	17.8	20	218.8	23.0	70	168.5	28.2
121	20.9	02.2	71	70.6	07.4	121	120,3	12.6	171	170.1	17.9	221	219.8	13.1	271	269.5	28 31
32		02.3			07.5	22	121.3		72	171.1	18.0	22	220.8			270.5	
23	1	02.4			37.6	23			73	172.0	18.1	23	221.8	23,3		271.5	
24		02.5	74	173.6	07.7	24		13.3	74	173.0	18.2	24	222.8			272.5	28 6
25	24 9	32.6	7	74.6	07.8	25	124.9	13.1	75	174-c		25	223.8		75	273-5	28.7
26	25.9	02,7	70	6 75,6	07,9	126	125.3	13.2	176	175.0	13.4	226	224.8	23.6	276	274-5	28,8
27	26.9	32.8			08.0	27	126.3		77	176.0	18.5	27	225,8	0	77	275 5	
28		02.9			1.80	28		13.4	78	177,0	18.0	28	226.7		78	276.5	
29		03.0		78.	08.3	29			79	178.0	10.7	29				277.5	29.2
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32	6	03.3			08.6		131.5		1 82				230.7		82	280.4	
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39	1.00	804.1	8	88.	509,3	1 30	138.	14.5	80	188.0	19.8	39	237-7	25,0	89	287.4	30.2
40		04.2	11 0		5 09,4	40	139	14.6	90	189.0	19.9	40	238.7	25.1	90	288.4	
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42		804.4			509.6	41	141.	14.8	92	190.	20.1	42	240.7				
41		804,5			5 09.7	4:	142.	14.9	93	191.	20.2	43	241.7	25.4	93	291.4	
44	43.8	04.6	9		509.8		143.	15,0	94	192.	20.3	44	242.7		94	292.4	30.7
45	44,	804.7			509.9		144.	15,2	95	193.	20.4	45	243-7			293.4	30,8
46		04 8			5 10.0		145.	15.3	196	194.	20.5	246	244.0			294,4	30.9
47		04.9	9		5 10.1	47	146.	15-4	1 97	195.	20.0	47	245.	25.8	97	295 4	
48	47.7	050	9	8 97.	5 10.2	41	147.	15.5	98	1190.	920.7	40	246.		98	296.	4 31,1
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1 7	06.9	00,9	57	56.6 06.9	07	106.2	3.C	57	155.8	19,1	07	205.4	25,2		255.1	
8		01,0	58	57.6 07.1	08	107.2	3.1	58	156.8	19 2		206.4			256.1	
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111	10 9	01.3	61	50,5,07 4	111	110.2	3 5	161	159.8	196	211	209,4	25.7	261	259.C	31.8
12	11.0	01.5	62	31.5 07.5	12	111.2	3.6	62	160 8	19,7	12	110.4	5.8		260.c	
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16	15 9	01 9	66	65 5 08.0	1116	115.1	14.1	166	164.8	20.2	216	214.4	26.2	266	264.0	22.4
117		02.1	67			116.1	4.2	67	165.7	20.2		215.4		67	265.c	22 5
18		G2.2	68			117.1	2 .		166.7			2164				
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21	20 8	02 6	71	70.5 08.6	121	120.1	147	171	169 7	20.8	221	219.3	26.0	271	269.0	22.0
22		02.7	72		22		14.5	72	170,7			220.3				
		02.8	73		23	122.1		73	1719			221.3			270.0	
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1 26	25.8	03.2	76	75 4 39 3	126	125.1	15.3	176	174-7	21.4	1226	224.3	27.5	276	273.9	22.6
27		3 03.3				126.c	15 5	77	175.7			125.3		14 1 1 1 1 1 1 1		
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				1	11 1	128 c									275.9	
29		03.5	83		11		- 01	79		21.8		227.3			276.9	
30	29	037	11-		30	129 c	15.8	80	170.7	21.9	30	228.3	28 0	82	277.9	34,1
31	10	8 03.8	8	1 80.4 39 9	1 131	130.0	160	181	179.6	22.0	231	229 3	28.1	281	278.9	24.2
32		\$ 03.9		2 81.4 10,0	32	131 6	16.1	82	180.6	22.2		230.3				
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33										22.4					280.9	34.5
34		7 04.1	110					84				232.2		84	281.9	
35	34.	7 04.3		-(35	134.C	16.4	85	103.0	22.5	35	233.2	28.6	85	182.9	34-7
36	135	7 04.4	8	6 85.4 10.	1136	135.0	16.6	186	184.6	22.7	2 3 6	234.2	28 7	286	283.9	
37		7 04 5		7 86 3 10.6	5 37	116.c	15.7	87		22,8	37	235.2			284 5	34.0
38	27	7 04 6	8	8 87.3 10.	38			88	186.6	122.0	3/	236.2	20.9		284.8	34.9
	37.	10:0	9	9 88,3 0.8	30	139.0	16.0	0.	18- 6	1,00		237.2	29.0	00	285.8	35.1
39		7 04 8		0 80,3		138.c			187.6	3.0		237.2	29.1	99	280,8	35 2
40	39	7 04 9	1 7	0 89 3 1.0	40	139.0	17.1	90	100.0	23.1	40	238.2	29,2	90	187.8	35.3
41		7 05 0	9	1 90.3 11,1	141	139.9	17.2	IOI	189,6	23.3	241	239,2	30.2		188.8	
4:		7 05.1				140.9		92	190.6	22.4		240.2		1 22	289.8	33.4
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															290.8	
4		7 05.4				142.9		94		23.6		242.2	129.7		291.8	
4:		7 05.5		5 94.3 11.6	-			95	193.5	23.7	45	243,2	29.8	95	292.8	35 C
41	5 45	05.6	9	6 95.3 11.7	146	144.9	17.8	196	194,	23.9	1246	244.2	20.0		293.8	
47		6 05,7	0	7 96.3 11.8	47	145.9	17.0		195.5	24.0	42	245.1	20.3	7	293.0	36
48	100	6 05.8	1 6	8 97.3 11.0		146.9	18.0	08	196.5	124	1 76	246	130.0	97	294.8	30.3
	1.0	6 25 -									40	246.1	10,2	98	295 8	30 3
49	40	6 06.0		98.3 12.1		147.9		99	197-5	24.2		247.1		99	296 8	36.4
50		6 06.1	-	99.3 12.2		148.9			198 5		250	248.1	30,4	:00	297.8	36.0
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	50.5 07.1 101 100.0 14 51.5 07.2 02 101.0 14		02 200.0 28.1	52 249 6 35.1
	52 5 07.4 03 102.0 14		03 201.0 28.3	53 250.5 35.2
3 73.0 00 4 53 5	53.5 07.5 04 103.0 14		04, 202.0 28,4	54 251.5 35.4
1 1 1 1	54.5 07.7 05 104,0 14		05 203.0 28.5	55 252.5 35.5
1 3	55,5 07,8 106 105.0 14	4.8 156 154 5 21.7	206 204 0 28.7	256 253.5 35.6
1 2	56.4 07.9 07 106.0 14	4.9 57 155.5 21 9	07 205.0 28.8	57 254-5 35.8
8 07 9 01,1 58	57.4 08.1 08 107.01	5,0 58 156 5 22.0	08 206.0 29.0	58 255.5 35.9
0 08.0 01.3 59	58.4 08,2 09 107.91		10 208.0 29.2	60 257.5 36.2
10 09 9 01.4 60	59 4 08.4 10 108.9 1			261 258.5 36 3
11 10.901.5 61	60,4 08.5 111 109 91		211 209.0 29,4	62 259.5 36 5
	51.4 08,6 12 110.91	5 6 62 100 4 22.6	11 6	63 260.4 36.6
11 12 901.8 63	62.4 08.8 13 111.91		1 - 1 01	64 261.4 36.7
14 13.9 01.9 64	63.4 08.9 14 112.91			65 262.4 36 9
15 14 9 02 1 65				266 263.4 37.0
16 15 8 02.2 66	1 3 1 3 1 1 - 1	6.1 166 164 4 23.1 16.3 67 165 4 23.2		67 264.4 37.2
17 16.8 02.4 67		3 1 - 1 - 1 - 1 - 1		68 265.4 37.3
18 17 8 02.5 68	1-1-3-3-3			69 266 4 37.4
19 18.8 02 6 69	1 2 2			70 267.4 37.6
20 19.8 02.8 70	3,3 3,1		1 0 - 0	271 268.4 37.7
21 20.8 02 9 71	1 1 20 1 01		11 0 0	72 269.4 37.9
22 21.8 03.1 72	1/2.3			73 270.4 38.0
	7 2 3 2 4 2 2 9	4	2 24 221.8 31,2	74 271.3 38.1
1-4 -3-1 3 3 1 -4	1/3.3		4 25 222.8 31 3	
			5 226 223.8 31.5	276 273.3 38 4
1 - 1 - 3 1 1 3 1 1	1/3.3		6 27 224.8 31.0	77 274-3 38.6
27 26.7 03.8 75 28 27.7 03.9 75			8 26 225.8 31.	78 275.3 38.7
29 28.7 04.0 7	9 78.2 11.0 29 127 7	18.0 79 177.3 24		79 276.1 38 8
1 - 7 / 1	0 79,2 11,1 30 128.7			
	1 80.2 11.3 131 129 7	18.2 181 179.2 25		2 281 278.3 39.1
1 3- 130-/ - 7 3 1	32 81.2 11.4 32 130.7	18.4 82 180.2 25		0 1-13 3 3 3
33 32.7 04.6 8	3 82.2 11.6 33 131.7	18.5 83 181,2 25	(a - a - a - A -	
1 34 33.9 04.7 8	84 83.2 11.7 34 132,7			
35 34.7 04 9 8	85 84.2 11.8 35 133.7			
1 26 25 7 05 0 1 8	86 85.2 12.0 136 134.7	18.9 186 184.2 25	.9 236 233.7 32. .0 37 234.7 33.	1 0 1 2
37 36.6 05.2 8	87 86.2 12.1 37 135.7	1 20 00 1		11 001 0
38 37.6 05 3 8	89 87.1 12.2 38 136.			3 89 286,2 40.2
		7 19.3 89 187.2 26 6 19.5 90 188.2 26		
40 39 6 05.6				
		6 19.6 191 189,1 26		7 92 289.2 40.6
			5.0 43 240.6 33	8 93 290.2 10.3
43 42.6 06.0 9	93 92.1 12,9 43 141.0 94 93.1 13.1 44 142.0	6 20.0 94 192.1 29	7.0 44 241.6 34	0 94 291.3 40.9
	95 94.1 13.2 45 143.	6 20.2 95 193.1 29	7.1 45 242.6 34	1 95 292.1 41.1
		6 20.3 196 194,1 2	7.3 246 243,6 34	.2 296 293.1 41.
	96 95.1 13.4 146 144. 97 96.1 13.5 47 145.	6 20 5 97 195.1 29	7.4 47 244.6 34	.4 97 294.3 41.
	98 97.0 13.6 48 146.	6 20.6 98 196.1 2	7.6 48 245.6 34	.5 98 295 1 41.
	99 98.0 13 8 49 147.	6 20.7 99 197.1 27		.7 99 296.1 41. .8 300 297.1 41.
		5 20.9 200 198.12		
3- 49.3 -/-		La: Diff Dep L	at Dift Depl L	at Dift Depla
DIN L'epilla [D	III. Dep Ziii Ziii			0 5

Difference of Latitude and Departure for 9 Deg.

	D'4 T D	D'A. T - De-I	Dia TalDall	Did TateDe I	D'A T ID
Diff Lat Dep		Dift Lat Dep			Diff Lat Dep
1 01.0 35.2	51 50.4 08,0	101 99 8 15.8	151 149.1 23.6	201 198.5 31 4	251 247.9 39.3
2 01.0 00.3	52 51.4 08.1	02 100.7 16.0	52 150.1 23.8	02 199.5 31,6	52 248.9 39.4
3 03.0 00 5	53 52 3 08.3	03 101.7 16.1	53 151.1 23.9	03 200.5 31 7	53 249.9 39.6
4 04.0 00.1	54 53.3 03.4	04 102.7 16,3	54 152,1 24,1	04 201.5 31.9	54 250.9 39.7
5 04 9 00.8	55 54.3 08,6	05 103.7 16.4	55 153.1 24,2	05 202.5 32.1	55 251 9 39,9
6 05.9 00.9	56 55,3 08.8	106 104,7 16 6	156 154.1 24.4	206 203.5 32.2	256 252.9 40,0
7 05.9 01,1	57 56 3 08.9	07 105.7 16 7	57 155.1 24.6	07 204 5 32.4	57 253.8 40.2
8 07 9 01,3	58 57.3 09.1	08 106.7 16.0	58 156.1 24.7	08 205.4 32.5	58 254.8 40.4
9 03.9 01.4	59 58.3 09,2	09 107.7 17.0	59 157.0 24.9	09 206.4 32,7	59 255.8 40.5
10 09 9 01.6	60 59 3 09 4	10 108.6 17.2	60 158.0 25 0	10 207 4 32 8	60 256.8 407
	61 60,2 09.5	111 109.6 17.4		211 208.4 33.0	261 257.8 40 8
11 10.901.7	62 61.2 09.7	12 110.6 17 5	62 160 0 25.3		6-1-1
12 11.9 01.9	63 32.2 09.9	13 111.6 17.6	63 161 0 25 5	12 209,4 33.2	63 259.8 41.0
13 12 8 02 0	64 63.2 10,0	14 112,6 17.8	64 162.0 25.6	14 211.4 33.5	64 260.8 41.3
15 14 8 02 3	65 64.2 10.2	15 113 6 18.0	65 163.0 25.8	15 212.4 33.6	65 261.7 41 4
16 15.8 02.5	66 65 2 10.3	116 114,6 18.1	166 164.6 26.0	216 213.3 33.8	266 262 7 41.6
17 16.8 02 7	67 66 2 10.5	17 115.6 18.3	67 164.9 26.1	17 214.3 33.9	67 263.7 41.8
18 17 8 02.8	68 67.2 10 6	18 116.5 18,5	68 165 9 26 3	18 215 3 34,1	68 264 7 +1.9
19 18 8 03.0		19 117-5 18.6	69 166.9 26,4	19 216.3 34.3	69 265.7 42.1
20 19.8 03.1	70 69.1 10.9		70 167,9 26.6	26 217,3 34,4	70 266 7 12.2
21 20,7 03.3	71 70.1 11.1	121 119,5 18.9	171 168.9 26.7	221 218.3 34,6	271 267.7 42.4
22 21.7 03.4	72 71.1 11,3	22 120.5 19.1	72 169.9 26.9	22 219.3 34.7	72 268 7 42.5
23 22.7 03.6	73 72.1 11.4	23 121.5 19.2	73 170,9 27.1	23 220.3 34.9	73 269.6 42.7
24 23.7 03.8	74 73.1 11.6	24 122.5 19.4	74 171.9 27.2	24 221.2 35.0	74 270.6 42,9
25 24,7 03.9	75 74.1 11.7	25 123.5 19 6	75 172.8 27.4	25 222.2 35.2	75 271.6 43.0
25 25.7 04.1	76 75 1 11,9	126 124 5 19.7	176 173,8 27.5	226 223.2 35.3	276 272 6 43.2
27 20.7 04.2	77 76.1 12.0	27 125 4 19.9	77 174.827.7	27 224.2 35.5	77 273.6 43.3
28 27.7 74.4	78 77.0 12.2	28 126 4 20.0	78 175.8 27.8	28 225. 35.7	78 274.6 43.5
29 28 6 04.5	79 78 0 12:4	29 127 4 20.2	79 176.8 28.0	29 226.2 35,8	79 275.6 43.6
30 29 6 04 7	80 79,0 12.5	30 128 4 20.3	80 177.8 28.2	30 227.2 36.0	83 276.6 43.8
31 30.6 04 8	81 80.0 12.7	131 129 4 20 5	181 178.8 28.3	231 228.2 36.1	281 277.5 43.9
32 31.6 050	82 81.0 12.8	32 130.4 20.6	82 179.8 28,5	32 229.1 36.3	82 278.5 44.1
33 32.0 05.2	83 82.0 13.0	33 131.4 20,8		33 230.1 36.4	83 279.5 44.3
34 33.6 05.3	84 83.0 13.1	34 132,4 21.0	84 181,7 28.8	34 231.1 36.6	84 280.5 44 4
35 34.6 05.5	85 84.0 13.3	35 133.3 21.1	85 182.7 28.9	35 232.1 36.8	85 281.5 44.6
36 35 6 05.6	86 84.9 13.5	136 134.3 21.3	186 183.7 :9.4	2 36 233 1 36,9	286 182.5 44 7
37 36.5 05.8	87 85.9 13.6	37 135.3 21.4	87 184.7 29.2	37 234.1 37.1	87 283.5 44.9
38 37.5 05 9	8\$ 86 9 13.8	38 136.3 21.6	88 185.7 29.4	38 235.1 37.2	88 284-5 45.0
39 38.5 06.1	89 87.9 13 9	39 137-3 21,7	89 186 7 29.6	39 236.1 37.4	89 285.4 45 2
40 39.5 06.3	90 88,9,14.1	40 138.3 21.9		40 237 0 37.5	90 286,4 45 4
41 40,5 06.4	91 89 9 14 2 92 90 9 14 4	141 139.3 22.1		241 238.0 37.7	291 287.4 45.5
43 42 5 06 7	93 91 9 14-5			42 239,6 37.8	
44 43,5 06.9	94 92.8 14.7		94 191.6 30.3		
45 44.4 07.0	95 93 8 14.9	45 143 2 22.		45 242.0 38.3	
46 45 4 07.2	96 94 8 15.0	146 144.2 22.8		246 243,0 38.5	296 292.4 46.3
47 46.4 07.4	97 95.8 15.2	47 145.2 23.0			
48 47.4 07.5	98 96.8 15.3			48 244.9 18.8	
49 48.4 07.7	99 97.8 15,5				
50 49.4 07,8	100 98.8 15.6	Commence of the later of the la	Townsell Street, Stree		and the same of the same of
Dift Pep Lat	Dift Dep Lat	Dit Depl La	Diff Dep La	Diff Der La	Dift Der La

for 81 Deg.

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Difty Lat Dep	Dift Lat Dep Dift Lat Dep	Dift Lat De Dift Lat Dep Dift	Lat De
1 01.0 00.2	51 50 2 08.8 101 99.5 17.5	151 148.7 26.2 201 197.9 34.9 251	247.2 43.5
2 02.0 00.3	52 51.2 09.0 02 100.4 17.7		248.2 43.7
3 03.0 00.5	53 52.2 09,2 03 101.4 17.9 54 53.2 09 4 04 102.4 18.0	53 150.7 26,5 03 199.9 35.2 53 54 151.7 26.7 04 200.9 35.4 54	249.2 43.9
5 04 9 00.9	54 53.2 09 4 04 102.4 18.0 55 54.2 09.5 05 103.4 18.2	54 151.7 26.7 04 200.9 35.4 54 55 152,6 26.9 05 201.9 35.5 55	251.144.2
6 05.9 01,0	56 55,1 09.7 106 104,4 18.4	156 153.6 27.1 206 202.9 35.7 256	
7 06 9 01,2	57 56.1 09.9 07 105.4 18.6	57 154.6 27.2 07.203.9 35.9 57	252.144 4
8 07 9 01.4	58 57.1 10,1 08 106.4 18.7	58 155.6 27.4 08 204 8 36.1 58	254.1 44.7
9 08 9 01.6	59 58.1 10.2 09 107.3 18.9	59 156.6 27.0 09 205.8 36.2 59	255.1 44.9
10 09 8 01.7	60 59 1 10.4 10 108.3 19.1	60 157.6 27.7 10 206.8 36.4 60	256.0 45.1
11 10.8 01.9	61 60,1 10.6 111 109.3 19.2 62 61.1 10.8 12 110.3 19.4	161 158.6 27.9 211 207.8 36.6 261 62 159.5 28.1 12 208.8 36.8 62	257.0 45 3
12 11.8 02.1	63 62.0 10.9 13 111.3 19.6		258.c 45.4 259.c 45.6
14 13.8 02 4	64 63.0 11.1 14 112.3 19.8	64 161 5 28.4 14 210.7 37.1 64	260.c 45.8
15 14 8 02 6	65 64.0 11,2 15 113.3 19.9	65 162.5 28,6 15 211.7 37.3 65	261.C 40 O
16 158 028	66 65 0 11.4 116 114,2 20.1	166 163.5 28.8 216 212.7 37.5 266	262,0 46.1
17 16.7 02.9	67 66 0 11 6 17 115.2 20.3	67 164 5 29.0 17 213.7 37.6 67	262.9 46 3
18 17 7 03.1	68 67.0 11.8 18 116.2 20.5 69 68.c 12.c 19 117.2 20 6	68 165 4 29.1 18 214.7 37.8 68 69 166.4 29.3 19 215.7 38.c 69	263.9 46.5
20 19 7 03.3	70 68.9 12.1 20 118.2 20.8	70 167,4 29.3 20 216.7 38.1 70	1
21 20.7 03.6	71 69.9 12.3 121 119,2 21.0	171 168.4 29,7 221 217,6 38.3 271	266 9 47.0
22 21.7 03.8	72 70.9 12.5 22 120.1 21.2	72 169.4 29 8 22 218.6 38,5 72	
23 22.7 04 0	73 71.9 12.7 23 121.1 21.3		268 8 47.3
24 23.6 04.2	74 72.9 12.8 24 122.1 21.5	74 171 4 30 2 24 220.6 38.8 74	
25 24,6 04 3	75 73.9 13.0 25 123.1 21,7	75 172.3 30.5 25 221.6 39.0 75	
26 25.6 04.5		176 173,3 30.5 26 222.6 39.2 276 77 174.3 30.7 27 223.5 39 4 77	271.8 47.9 272.8 48.0
27 20.0 04.7			
29 28 6 05 0	79 77.8 13.7 29 127 0 22.4	a married that that believes I married Direction believes I married	274.8 48,4
30 29 5 05.2		80 177.3 31,2 30 226.5 39.9 83	275.7 48 6
31 30.5 05.4		181 178.2 31 4 231 227.5 40.1 281	1-1-11-1
32 31.5 05.5	82 80.8 14.2 32 130.0 22.9		1-11-11-2
33 32-5 05-7	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	83 180.2 21.7 33 229 5 40.4 83 84 181,2 21.9 34 230.4 40,6 84	
34 33·5 05.9 35 34·5 06.1	0 - 0 - 1 - 1 46	85 182.2 32.1 35 231.4 40.7 85	1-/2/11/2-
36 35 5 06.2		186 183 2 32.3 236 232 4 40.9 286	
37 36.4 06.4	87 85.7 15.1 37 134.9 23.8	87 184.2 32.4 37 233 4 41.1 87	182.6 49,8
38 37.4 06.6	88 86.7 15.3 38 135.9 23,9	88 185.1 32.6 38 234.4 41,3 88	283.5 49.9
39 38 4 06 8	89 87.6 15,4 39 136.9 14.1		284.6 50,1
40 39.4 06.9	0 (0		285.6 50.3
41 40,4 07.1			286,6 50.5 287.6 50.6
43 42.3 07.5	93 91.6 16.1 43 140.8 24.8		288.5 50 8
44 43,3 07.6	94 92.6 16,3 44 141.8 25.0	94 191.0 33.6 44 240.3 42.3 94	289.5 51.0
45 44-3 07,8	95 93.6 16.5 45 142.8 25.1	95 192.0 33 8 45 241.3 42,5 95	290.5 51.2
46 45 3 08.0	96 94.5 16,6 146 143.8 25,3	196 193.0 34.0 246 242.3 43.7 296	
47 46.3 08.1	97 95.5 16.8 47 144.8 25.5 98 96.5 17.0 48 145.7 25.7		292.5 51.5
48 47.3 08.3	99 97.5 17.2 49 146.7 25.8		294.5 51.8
50 49.2 08.7	100 98.5 17.3 150 147.7 26.0	200 197.0 34,7 250 246.2 43.4 1200	295 4 52.0
Dift L'en Lat	Dift Dep Lat Dift Dep La		Dep La

for 80 Deg.

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Ditt	Lat	Dep	Diff	Lat	Dep	Din	Lat	Dep	D.A	Lat	Dep	Dift	Lat	Dep	Dift	Lat	D
-	01.0	00 2	51	50.1	09.7	101	199.1	19.3	151	148.2	28.8	201	197.3	28.4	251	246.4	47
		00 4			09.9		100.1			149.2	100000	02	198.3	28.6	52	247.4	
-		- 2		-			101.1					0:	199 3	28 7		248.	
3		Un.6		52.0		100			53						53		
4		30.8			10.3		102.1			151.2			200.2		54	249.3	
5	04 9	0.10	55	54.0	10.5	05	103 1	20.0	55	152.1	29 0	05	201.2	39.1	55	250.3	
6	05.9	31.1	56	550	10.7	106	104.0	20.2	156	153:1	29.8	206	252.2	39.3	256	251.3	48
-	06 9				10 9	1 1 1	105.0	12		154.1			203.2		57	252.3	
		01.5			11.1	1	106.0			155.1			204.2		58	253,2	
	08.8		_	The second second	11.3		107.0			156.1			205.2		59	254.2	
,		01.9			11.4		108.0		60				206,1		60		
10	-	_					105.0		-	157.1		-		_	-	255 2	-
11	8.01		61	59,9	11.6	111	109.0	21.2		158.0			207.1		261	256.2	49
12	11.8	02.3	62	60.9	8.11	12	109.9	21.4	62	159.0	30.9	12	208.1	40.4	62	257,2	50
13	12.8	02.5	63	61.8	12.0	13	110.9	21.6	63	160.0	31.1	13	209.1	40.6	63	258,2	150
14	1	02.7	64	62.8	12.2	14	111:9	21.8	64	161,0	31.3	14	210 1	40.8	64	259 1	50
		02 9	65	618	12.4	15	112.9	000		162.0			211.0	200	64	260.1	
15	_				_	-	-			_		-	-		-	_	-
10		03.1			12.6		113.5			162 9		1 5 89	212.0	2000		261.1	
17		03.2			12 8		114.8			163 9			213.0			261,1	
18	17.7	03 4	68	66,7	130	18	115.8	12.5		164.9		18	2140	41.6	68	263.1	
19	18 7	03.6	69	67.7	13.2	19	116.8	22.7	69	165 9	32.2	19	215.0	41.8	69	264.C	51
20	19.6	03.8	70	68,7	13.4	20	117.8	22.9	70	166.9	32,4	20	215.9	42.0	70	265.0	51
-	20.6		71	60.7	13.5	121	118.8	22.1		167.9	_		216.9		271	266.0	51
					-		119.8									267.0	
22	21.6			70.7						168.8			217.9		72		
23		04:4			13.9	23	120,7			169 8			218.9		73	268.0	-
24		04,0		72.6		24	121.7			170.8			219.9			269.0	
25	24 5	04.8	75	73.6	14.3	25	122.7	23.9	75	171.8	33-4		220.9		75	269 9	52
26	25.5	05.0	76	74.6	14.5	126	123.7	24.0	176	172.8	33.6	226	221.8	43.1	276	270.9	52
	26.5				14.7	27	124.7			173.7		27	222.8	42.2		271.9	
	27.5			76.6			125.6			174.7	-		223.8		78	272.9	
	28.5			77.5		1	126.6			175.7			224.8		79	273.9	-
			80	78.5	15.0		127.6		80				225,8		80		
30	29 4	35.7				30	_			176 7	_				-	274.8	
31	30.4	05.9			15,5		128 6			177,7			226.7			275.8	
32	31.4	06.1	82	80.5	15.6	32	129.6	25.2	82	178.6	34.7	32	227.7	44.3	82	276.8	53
33	32.4	06,3	83	81.5	15,8	33	130.6	25 4	83	179 6	54.9	33	228,7	44 5	83	277.8	54
	33 4		84	82,5	160	34	131.5	25.6	84	180.6	35,1	34	229 7	44.6	84	278.8	54
35	34-4		85	83.4	16.2	35	132.5	- 0	85	180.6	35,3		230.7		85	279.8	
				84 4					-			-			286	-	-
	35.3					136	133.5			182.6			231.7			280.7	
37	36.3	27.1	07	05.4	166	37	134.5	20.1	87	183.6	35.7	37	232.0	45 2	87	281.7	54
38	37-3	07.3	88	00.4	16 8	38	135.5	20.3	88	184 5	35 9	30	233.6	45 4	88	282,7	55
39	38.3	07.4	89	07.4	17.0	39	136.4	20,5	89	185,5	30.1	39	234.6	45.0	89	283.7	55
10	19.3	27.6	90	88,3	17.2	40	137-4	26 7	90	186 5	36.3	40	235.6	45,8	90	284.7	55
_	40.2				17.4		138 4		IOI	187.5	26.4	241	236.6	46.0		285.6	
		08.0			17,6		139 4		9.	188.5	36.6		237-5			286,6	
	42.2				17.7					189.4	26.8	4.	238.5	46 4	92	287.6	33
13	44.2	00.2					140 4						239 5	16 6		-89 6	33
	43.2	30.4	94	94.3	17 9	44.	141.3			190.4					94	188.6	
15	44,2	08.6			18.1	45	142.3		95	191.4	37.2		240.5		95	289.6	
16	45.2	08.8	96	94.2	18 3	146	143.3	27.9	196	193 4	37.4	246	241.5	47.0	296	290.5	56
17	46.1	00.0	97	95 2	18.5	47	144.3	28.0	97	193.4	37.6		242.5		97	291.5	56
	47.1		08	06.2	18.7	12	145.3	28.2	08	194.4	27.8		243.4		98	292.5	66
					18.9	1	146.3	28.4	7	195.4	18.0		244.4				
				4/.2	10.9	1 49	140.3	20,4	1999	195.4	10.0	1 49	-44.4	+1.2	1 99	293.5	
49	48.1									6	-9 -1	1000	240 4		1.00		100
9 5 2	49.1		100	98.2	19,1	150	Dep	28,6	200	196.3	38.2 Lit		245 4 Dep			294,5 Dep	-

12 Difference of Latitude and Departure for 12 Deg.

			and the	Y Land		C de la la			Spare .	2				-	
Dut	Lat Dep	Diff Lat	Dep	Diff	Lat	Dep	Dift	Lat	Der	Dift	Lat	Dep	Dift	Lat	Dep
1	01.0 00 2	51 49 9	10.6	IOI	98.8	21.0	151	147-7	31 4	201	196,6	41.8	251	145.5	52.2
2	02.0 00.4	52 50,9	10.8	02	99 8	21.3		148.7	31.6		197.6		52	246.5	52,4
1 3	02.9 00.6		11.0	. 03	100.7			149.6			198.5	42.2	53	247.4	52.6
4	03.9 00.8	54 52.8	11.2	04	101.7		54	150.6		1 1 1 1	199 5		54	148.4	
5	04.9 01.0			05	102.7	_	55	151.6		05	200.5	12.6	55	249 4	53,0
6	05.9 01.2				103 7			152.6			201.5		256	250.4	
7	06.8 01.5			07	104.		57	153.5		07	202.4		57	251.3	53-5
8	08.8 01.9				105.6		58	154 5		08	203.4		58	252.3	
10	09.8 02.1			10	107 6			155.5		10	205.4		59	253,3 254 3	53.9
1-	10.8 02.3			111	108.6	-	161	157.5		211			261		
11	11.7 02.5	1 0 0		12	109.5			158.4			206,4		62	255.3 256.2	54.3
113	12.7 02.7	11000		13	110.			159.4			208.3		63	257,2	
14	13.7 02 9	1 2 2 1		14	111.5			160.4			209.3			258,2	
15	14.703.1	65 63 6	13.5	15	112.5	23.9	65	161,4		15	210 3	C	65	259 2	
116	15.6 03.3	66 64,5	13.7	116	113.4	24.1	166	162.3		216	211.2	-	266	260.1	
17	16.6 03 5	67 65.5	13.9	17	114.4	24.3	67	163.3	34.7	1 1 1	212.2		67	261.1	55.5
18	17.6 03.7			18	115 4			164.3		18	213.2	45.3	68	261,1	55.7
19	18.6 04.0			19	116 4		69	165.3	35,2		214.2	-	69	263.1	
20	19.6 04.2			20	117.4			166.3		20	215.2		70	264.1	-
21	20.5 04.4			121	118.3		171	167.2	35.6	221	216.1		271	265.0	
122	21.5 04,6			22	119.3			168.2			217.1		72	266.0	
23	23.505.0			23	120,3			169 2			218.1			267.0	
24	24 5 05.2			25	122.3		75	171.2		25	219.1 220.1		74 75	268.0 269 0	57.0
26		1		126	123.2	-	176	172.1		226			276		-
27	25.4 05.4			27	124.2		77	173.1		The Land	221.0		77	269 9	57.4
28	27.4 05.8		16.2	28	125.2			174.1		28	223.0		78	271.9	
129	28.4 06.0	79 77-3	16.4	29	126.2		79	175.1			224.0		79	272.9	
30	29.3 06,2		166	30	127.1	27 0	80	176 0	37-4	30	224 9	47.8	80	273.8	58.2
31	30.3 06.4	81 79.2	16.8	131	128 1	27.2	181	177,0		231	225,9	48.0	281	274.8	58 4
1 32	31.3 06.7			32	129.1	27.5	82	178.0		32	226.9	48.3	82	275.8	
33	32.3 06.9	1 0 10		33	130.1			179 0			227.9		83	276.8	
34	33 3 37.1			34	131.1		84	180.0			228,9		84	277.8	59.1
35	34.2 07.3			35	132.0		85	_		35	229.8		85	278.7	59.3
36	35.2 07.5		17.9	136	133.0	28.3	186	181.9		236	230.8	49.1	286	379.7	59.5
37			18.0	37	134.0	28.7	87	182.9	30.9	37	231.8	49.3	87	280.7	59.7
39	37.2 07.9		18.5	30	135.9	28.0	80	184.8	39.2		233.8		88	281 7	59.9
40	39.1 08.3		18.7	40	136.9		90	185,8	39.5		234.7		90	283.6	
41	40.1 08.5		-	141	137.9			186.8			235.7	-	291	284.6	_
42	41.1 08.7			42	138.9	29.5	62	187.8	39.9		236.7	50.1		285.6	
43	42.1 08.9				139 9	29.7	93	188.8	40.1		237.7		93	286,6	
	43.0 09.2	9491.9	19.6	44	140 8	30.0	94	189.7	40.4	44	238.6	50.8		287.5	61.2
45	44,009.4	95 92.9	19.8	45	141.8	30.2	95	190.7	40.6	45	239 6	51.0	95	288.5	61.4
	45.009.6	The second second	20.0	146	142.8	30.4	196	191.7	40.8	246	240.6	51.2		289.5	61,6
47	46.009.8	97 94.9	20.2	47	143.8	30.6	97	192.7	41.0	47	241.6	51.4	97	290.5	61.8
48	46.9 10.0	98 95.8		48	144.7			193.6	41.2		242.5		98	291.4	62.0
	47.9 10.2			49	145.7	31.0		194.6		49	243.5	51,8	99	292.4	
	48.9 10.4				146.7			195.6			244.5		300	293.4	
Diff	Dep Lat	Dift Dep	[Lat	Diff	Dep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Dia	Dep	Lat
			4 1 CV	1 10 10	C. V.	- 31.	49.55	184 5.40		1 100	194	Marin I			V 14 3

for 78 Deg.

1 01 0 00.2 51 49.7 11.5 101 98.4 22.7 151 147.1 34.0 201 195.9 45.2 25 2.9 00.7 53 51 6 11.9 03 100.4 23.2 53 149.1 34.4 03 197.8 45.7 54.9 54.9 51.1 55 53.6 12.4 05 102.3 23.6 55 151.0 34.9 05 199.7 46.1 55 53.6 12.4 05 102.3 23.6 55 151.0 34.9 05 199.7 46.1 55 55.5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 57 55.5 13.8 08 105.3 24.3 58 154.0 35.5 08 202.7 46.8 59 09.7 02.2 20.5 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 09 203.6 47.0 59 109.7 22.7 60 58.5 13.5 10 107.2 24.7 60 155.9 36.0 10 204.6 47.2 60 10.7 22.7 62 60.4 13.9 12 109.1 25.4 63 158.8 36.7 13 207.5 47.9 60 15 60.3 64 62.4 14.4 14 111.1 25.6 64 159.8 36.9 14 208.5 48.1 64 15 16.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 60.1 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.8 18 212.4 49.0 19 18.5 04.3 69 67.2 15.5 19 116 26.8 69 164.7 38.0 19 213.4 49.3 66 19 18.5 04.3 69 67.2 15.5 19 116 26.8 69 164.7 38.0 19 213.4 49.3 66 19 18.5 04.3 69 67.2 15.5 19 116 26.8 69 164.7 38.0 19 213.4 49.3 66 19 18.5 04.3 69 67.2 15.5 19 116 26.8 69 164.7 38.0 19 213.4 49.3 66 19 18.5 04.3 69 67.2 15.5 19 116 26.8 69 164.7 38.0 19 213.4 49.3 66 19 18.5 04.3 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 66 164.7 38.0 19 213.4 49.3 164.5 164.7 38.0 164.7 38.0 164.7 38.0 164.7 38.0 164.7 38.0 164.7 38.	Lat 1 244.6 2 245.5 3 246.5 5 248.5 5 249.4 5 2 258.3 5 256.3	56 56 57 57 57 57 58 58 58 58 58
1 01.9 00.4 52 50.7 11.7 02 99.4 22.9 52 148.1 34.2 02 196.8 45.4 53 12.9 00.7 53 51.6 11.9 03 100.4 23.2 53 149.1 34.4 03 197.8 45.7 53 149.1 34.4 03 197.8 45.7 55 150.3 9 00.9 54 52.6 12.1 04 101.3 23.4 54 150.1 34.6 04 198.8 45.9 55 150.3 9 01.1 55 53.6 12.4 05 102.3 23.6 55 151.0 34.9 05 199.7 46.1 55 106.8 01.6 57 55.5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 35 10.8 37.8 01.8 58 56.5 13.0 08 105.3 24.3 58 154.0 35.5 08 202.7 46.8 55 10.0 9.7 92.2 60 58 5 13.5 10 107.2 24.7 60 155.9 36.0 10 204.0 47.2 60 155.9 36.0 10	2 245.5 5 3 246.5 5 4 247.5 5 5 249.4 5 6 249.4 5 7 250.4 5 2 251.4 5 2 252.4 5 2 253.3 5 2 256.3 5 2 257.2 5 3 256.3 5 3 256.3 5 4 257.2 5 5 259.2 5	56 56 57 57 57 57 58 58 58 58
3 2.9 00.7 53 51.6 11.9 03 100.4 23.2 53 149.1 34.4 03 197.8 45.7 5 4 03 9 00.9 54 52.6 12.1 04 101.3 23.4 54 150.1 34.6 04 198.8 45.9 5 5 04.9 01.1 55 53.6 12.4 05 102.3 23.8 156.152.0 35.1 206 200.7 46.3 25 7 06.8 01.6 57 55.5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 35.3 8 07.8 01.8 58 56.5 13.0 08 105.3 24.3 58 154.0 35.5 08 202.7 46.8 57 9 8.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 69 203.6 47.0 57 10 09.7 02.2 <t< td=""><td>246.5 5 4 247.5 5 248.5 5 249.4 5 5 2 251.4 5 2 252.4 5 2 256.3 5 2 256.3 5 2 259.2 5</td><td>56 57 57 57 57 58 58 58 58</td></t<>	246.5 5 4 247.5 5 248.5 5 249.4 5 5 2 251.4 5 2 252.4 5 2 256.3 5 2 256.3 5 2 259.2 5	56 57 57 57 57 58 58 58 58
4 03 9 00.9 54 52.6 12.1 04 101.3 23.4 54 150.1 34.6 04 198.8 45.9 5 5 5 04.9 01.1 55 53.6 12.4 05 102.3 23.8 156 151.0 34.9 05 199.7 46.1 5 6 05.8 01.3 56 54.6 12.6 106 103.3 23.8 156 152.0 35.1 206 200.7 46.3 25 7 06.8 01.6 57 55.5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 5 8 07.8 01.8 58 56.5 13.0 08 105.3 24.3 58 154.0 35.5 08 202.7 46.8 5 9 8.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 69 203.6 47.0 5 5 109.7 24.7 60	4 247.5 5 248.5 5 249.4 5 5 250.4 5 2 2 5 2 .4 5 2 2 5 5 .3 5 2 2 5 6 .3 5 5 2 5 2 5 5 2	57 57 57 58 58 58 58 58
5 04.9 01.1 55 53.6 12.4 05 102.3 23.6 55 151.0 34.9 05 199.7 46.1 5 6 05.8 01.3 56 54.6 12.6 106 103.3 23.8 156 152.0 35.1 206 200.7 46.3 25 7 06.8 01.6 57 555.5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 55 8 07.8 01.8 58 56.5 13.0 08 105.3 24.3 58 154.0 35.5 08 202.7 46.8 55 9 8.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 09 203.6 47.0 55 10 09.7 02.2 60 58 5 13.5 10 107.2 24.7 60 155.9 36.0 10 204.6 47.2 60 11 10.7 02.5 61 59.4 13.7 111 108 2 25. 161 156.9 36.2 211 205.6 47.5 26 12 11.7 02.7 62 60.4 13.9 12 109.1 25. 62 157.9 36.4 12 206.6 47.7 66 13 12.7 02.9 63 61.4 14.2 13 110.1 25.4 63 158.8 36.7 13 207.5 47.9 6 64 12.9 8.6 48.1 66 15 14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 64 15	248.5 5 249.4 5 250.4 5 252.4 5 252.4 5 253.3 5 254.3 5 256.3 5 257.2 5 258.2 5 259.2 5	57 57 58 58 58 58 58
6 05.8 01.3 56 54.6 12.6 106 103.3 23.8 156 152.0 35.1 206 200.7 46.3 25.7 7 06.8 01.6 57 55.5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 5.7 8 07.8 01.8 58 56.5 13.0 08 105.3 24.3 58 154.0 35.3 08 202.7 46.8 5.7 9 08.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 69 203.6 47.0 5.7 10 09.7 02.2 60 58.5 13.5 10 107.2 24.7 60 155.9 36.0 10 204.6 47.2 6.1 60 155.9 36.0 10 204.6 47.2 6.1 110.7 22.7 62 60.4 13.9 12 109.1 25. 62 157.9 36.4 12 206.6 <td>249.4 5 250.4 5 251.4 5 252.4 5 253.3 5 254.3 5 255.3 5 256.3 5 257.2 5 258.2 5 259.2 5</td> <td>57 57 58 58 58 58</td>	249.4 5 250.4 5 251.4 5 252.4 5 253.3 5 254.3 5 255.3 5 256.3 5 257.2 5 258.2 5 259.2 5	57 57 58 58 58 58
7 06.8 01,6 57 55,5 12.8 07 104.3 24.1 57 153.0 35.3 07 201.7 46.6 57 8 07.8 01.8 58 56.5 13,0 08 105.3 24.3 58 154.0 35.5 08 202.7 46,8 59 08.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 09 203.6 47.0 10 09.7 02.2 60 58 5 13.5 10 107,2 24.7 60 155.9 36.0 10 204.0 47.2 60 11 10,7 02.5 61 59.4 13.7 111 108 2 25. 161 156.9 36.2 211 205.6 47.5 12 11.7 02.7 62 60 4 13.9 12 109.1 25. 62 157.9 36.4 12 206.6 47.7 62 13.6 03.1 64 62.4 14.4 14.11.1 25.6 64 159.8 36.9 14.208.5 48.1 15.14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 66.17 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4 48.8 18.17.5 04.0 68 66.2 15.3 18 115.0 26.5 68 163.7 37.8 18 212.4 49.0 69 18.5 04.3 69 67.2 15.5 19 116 0 26.8 69 164.7 38.0 19 213.4 49.3 66.1	250.4 5 251.4 5 252.4 5 253.3 5 254.3 5 255.3 5 3256.3 5 3257.2 5 3259.2 5	57 58 58 58 58 58
8 07.8 01.8 58 56.5 13.0 08 105.3 24.3 58 154.0 35.5 08 202.7 46,8 5 9 08.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 69 203.6 47.0 5 10 09.7 02.2 60 58.5 13.5 10 107,2 24.7 60 155.9 36.0 10 204.6 47.2 6 11 10,7 02.5 61 59.4 13.7 111 108.2 25. 161 156.9 36.2 211 205.6 47.5 6 12 206.6 47.5 6 12 206.6 47.7 6 12 206.6 47.7 6 12 206.6 47.7 6 13 13 207.5 47.9 6 158.8 36.7 13 207.5 47.9 6 6 158.8 36.7 13 207.5 48.1 6 6 159.8 14.4 111.1	251.4 252.4 253.3 254.3 255.3 256.3 257.2 259.2 259.2	58 58 58 58 58
9 88.8 02.0 59 57.5 13.3 09 106.2 24.5 59 154.9 35.8 69 203.6 47.0 59 100.0 09.7 02.2 60 58 5 13.5 10 107.2 24.7 60 155.9 36.0 10 204.6 47.2 60 11 10.7 02.5 61 59.4 13.7 111 108 2 25. 161 156.9 36.2 211 205.6 47.5 26.1 12.7 02.9 63 61.4 14 2 13 110.1 25.4 63 158.8 36.7 13 207.5 47.9 69 14 13.6 03.1 64 62.4 14 4 14 111.1 25.6 64 159.8 36.9 14 208.5 48.1 15 14.6 03.4 65 63.3 14 6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 69 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.8 18 212.4 49.0 18.5 04.3 69 67.2 15.5 19 116 0 26.8 69 164.7 38.0 19 213.4 49.3 69 18.5 04.3 69 67.2 15.5 19 116 0 26.8 69 164.7 38.0 19 213.4 49.3 69	252.4 253 3 254-3 255-3 256-3 257-2 258-2 5 259-2	58 58 58 58
10 09.7 02.2 60 58 5 13.5 10 107,2 24.7 60 155.9 36.0 10 204.6 47.2 60 11 10,7 02.5 61 59.4 13.7 11 108 2 25. 161 156.9 36.2 211 205.6 47.5 26 12 11.7 02.7 62 60.4 13.9 12 109.1 25. 62 157.9 36.4 12 206.6 47.7 66 13 12.7 02.9 63 61.4 14.2 13 110.1 25.4 63 158.8 36.7 13 207.5 47.9 66 14 13,6 03.1 64 62.4 14.4 14 111.1 25.6 64 159.8 36.9 14 208.5 48.1 66 15 14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 66 16 15.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4	253.3 254.3 255.3 256.3 256.3 257.2 258.2 258.2	58. 58. 58.
11 10,7 02.5 61 59.4 13.7 111 108 2 25. 161 156.9 36.2 211 205.6 47.5 12 11.7 02.7 62 60 4 13.9 12 109.1 25. 62 157.9 36.4 13.0 13.0 13.1 13.6 03.1 64 62.4 14.4 14.1 11.1 25.6 64 159.8 36.9 14.208.5 48.1 15 14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 6.1 15 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4 48.8 18 17.5 04.0 68 66.2 15.3 18 115.0 26.1 166 161.7 37.3 18 212.4 49.0 18.5 04.3 69 67.2 15.5 19 116 0 26.8 69 164.7 38.0 19 213.4 49.3 66	254.3 5 255.3 5 256.3 5 257.2 5 258.2 5 259.2 5	58. 58. 59.
12 11.7 02.7 62 60.4 13.9 12 109.1 25.4 62 157.9 36.4 12 206.6 47.7 62 13 12.7 02.9 63 61.4 14.2 13 110.1 25.4 63 158.8 36.7 13 207.5 47.9 66 14 13,6 03.1 64 62.4 14.4 14 111.1 25.6 64 159.8 36.9 14 208.5 48.1 66 15 14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 16 15 60.3 64.3 14,8 116 113.0 26.1 166 161.7 37.3 216 210.5 48.6 17 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4 48.8 69 18 17.5 04.0 68 66.2 15.3 18 115.2 26.5 68 163.7 37.8 18 212.4 49.0 69 19 18	255.35 256.35 257.25 258.25 259.25	58
13 12.7 02.9 63 61.4 14.2 13 110.1 25.4 63 158.8 36.7 13 207.5 47.9 6 14 13,6 03.1 64 62.4 14.4 14 111.1 25.6 64 159.8 36.9 14 208.5 48.1 6 15 14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 6 16 15 60.3 14.8 116 113.0 26.1 166 161.7 37.3 216 210.5 48.6 26 17 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4 48.8 6 18 17.5 04.0 68 66.2 15.3 18 115.e 26.5 68 163.7 37.8 18 212.4 49.0 60 19 18.5 04.3 69 67.2 15.5 19 116 26.8 69 164.7 38.0 19 213.4 49.3 60	256.3 5 257.2 5 258.2 5 259.2 5	59
14 13,6 03.1 64 62.4 14 14 111.1 25.6 64 159.8 36.9 14 208.5 48.1 6.1 15 14.6 03.4 65 63.3 14.6 15 112.1 25.9 65 160.8 37.1 15 209.5 48.4 6.1 16 15 60.3 64.3 14,8 116 113.0 26.1 166 161.7 37.3 216 210.5 48.6 26.1 17 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4 48.8 6.1 18 17.5 04.0 68 66.2 15.3 18 115.e 26.5 68 163.7 37.8 18 212.4 49.0 60 19 18.5 04.3 69 67.2 15.5 19 116 e 26.8 69 164.7 38.0 19 213.4 49.3 60	257.2 258.2 259.2	59
15	258.2	
16 15 6 03 6 66 64 3 14 8 116 113 0 26 1 166 161 7 37 3 216 210 5 48 6 17 16 6 03 8 67 65 3 15 17 114 0 26 3 67 162 7 37 6 17 211 4 48 8 6 18 17 5 04 0 68 66 2 15 3 18 115 6 26 5 68 163 7 37 8 18 212 4 49 0 6 18 18 18 18 18 18 18	259.2	50
17 16.6 03.8 67 65.3 15.1 17 114.0 26.3 67 162.7 37.6 17 211.4 48.8 69 17.5 04.0 68 66.2 15.3 18 115.e 26.5 68 163.7 37.8 18 212.4 49.0 69 18.5 04.3 69 67.2 15.5 19 116 0 26.8 69 164.7 38.0 19 213.4 49.3 69	29.2	
18 17.5 04.0 68 66.2 15.3 18 115.e 26.5 68 163.7 37.8 18 212.4 49.0 69 18.5 04.3 69 67.2 15.5 19 116 e 26.8 69 164.7 38.0 19 213.4 49.3 69		<u>59</u> .
19 18.5 04.3 69 67.2 15.5 19 116 0 26.8 69 164.7 38.0 19 213.4 49.3 6	261.16	60
	262.16	60
20 19.5 04,5 70 68.2 15.7 20 116.9 27.0 70 165.6 38.2 20 214.4 49,5 70	263.16	60.
	264.16	
	265.06	
	266 c 6	
	267.06	
	268.c 6	
26 25 3 05.8 76 74.1 17.1 126 122.8 28.3 176 171.5 39 6 226 220.2 50.8 276	268.96	67
	269.96	
	270.96	52
20 28.3 06.5 79 77.0 17.8 29 125.7 29.0 79 174.4 40.3 29 223.1 51.5 79	271.96	52.
	272.8 6	
31 30.2 07.0 81 78.9 18,2 131 127.6 29.5 181 176.4 40.7 231 225.1 52.0 281	273.8 6	63.
32 31.2 07.2 82 79.9 18.4 32 128.6 29.7 82 177.3 40 9 32 226.1 52.2 82	274.8 6	53.
33 32.2 07.4 83 80.9 18.7 33 129.6 29.9 83 178.3 41.2 33 227.0 52.4 83	275.8 6	53.
34 33.1 07.6 84 81.8 18.0 34 130.6 30.1 84 179.3 41.4 34 228.0 52.6 84	276.76	53.
		64.
36 35.1 08.1 86 83 8 19.3 136 132.5 30.6 186 181.2 41.8 236 230.0 53,1 286	278.76	54.
37 36.1 08 3 87 84.8 19.6 37 133.5 30.8 87 182.2 42.1 37 230.9 53.3 87	279.66	54,
	280.6	54.
	281.66	55.
	282,6	05.
41 39,9 09.2 91 88 7 20.5 141 137.4 31.7 191 186.1 43.0 241 234.8 54.2 291	283.56	55.
42 40.9 09 4 92 89 6 20.7 42 138.4 31.9 92 187.1 43.2 42 235.8 54.4 92	284.5 6	55.
	285.56	5,
	286.5 6 287.4 6	56
46 44.8 10.3 96 93.5 21.6 146 142.3 32.8 196 191.0 44.1 246 239.7 55.3 296	288.4 6	
47 45.8 10.6 97 94.5 21.8 47 143.2 33.1 97 192.0 44.3 47 240.7 55.6 97 48 46.8 12.8 98 95 5 22.0 48 144.2 33.3 98 192.9 44.5 48 241.6 55.8 98	289.4 6	00.
	290.4 6	67.
	292.36	57.
	-	19
Diff Den Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff	Dep 1	

14 Difference of Latitude and Departure for 14 Deg.

Dift	Lat	De	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Del	Dift	Lat	Der	Dif	Lat	De
,	010	00.2	51	49.5	12.3	101	98.0	24.4	151	146 5	36.5	101	195.0	48.6	251	243.5	60
	01.9		52		12.6	02		24.7	52	147.5	36.8		196 0			244.5	
3	-2.9	00.7	53	51 4	12.8	03	99,9	24.9	53	148.5	37.0		197.0			245.5	
4		01.0	54	Name and Address of the Owner, where the Owner, which is the Owner, which is the Owner, where the Owner, which is the Owner,	13,1	04	100.9	_	54	149.4			197.9			246.4	
5	04.9	01.2	55	53-4	13.3	05	101.9	25.4	55	150.4	37 5	05	198.9	49,0		247.4	
6		01.5	56	54 3	13.6	105	102.8		156	151.4	37.7	206	199.9	49.9		248.4	
7		01,7	57		13.8		103.8		57	152.3	38.0		200.8		57	249.4	62,
8		01.9	58		14.0		104.8		50	153.3	38.2		201.8			250.3	
9		02.2	59		14 3		105.8		59	154-3	38.5		202.8			251.3	
10	09.7	02.4	60		14 5	10	106 7	_		155.2			203.8		-00	252.3	02,
11		02.7	61		14,8		107,7			156.2			204.7			253.2	
12		02.9	62	60.2	15.0		108.7			157.2			205.7			254.2	
13	-4.5 Tal	03.1	63		15.2	1	109.6	. 71		158.2		_	206.7			255.2	
14		03.4			15.5	14	110.6			159.1			207.6	1-		256.2	
15	-	03.6	65	-	15.7	15	111.6	_	-	160.1		-		_		257.1	
16		03.9	66		16.0	116	112.6	28.1	166	161.1			209.6	-		258.1	
17		04.1	68	65.0	16 5	17	113.5	20.3		162.0		1	210.5	1 31		259.1	
18		04.4	69		16.7	10	114.5	28.8		163.0		- 3-3	211.5			261.0	
19		04.8	70		16.5	19	115.5			164.0			212.5			262.0	
-	<u> </u>	-	_	_		-			-		1-						
21	20.4		71	1 -	17.2		117.4		171	165.9	41.4		214.4			261.9	
22		05.3	72		17.4		118.4			166.9			215.4			263.9	
23		05.8	73		17.7	11	119 3	10.0	73	168.8			217.3			265.9	
24	24.3		75		18.1	24	121.3	20.2	74				218.3	-		266 8	
25	-			-	-							-	219.3			267.8	
26		06.3	76	73.7	18.6	126	122.3	30.3	176	171.7			220.3			268.8	
27		06.8	77	74.7	18.9		124.2		77	172.7			231.2			269.7	
29		07.0	79	1	19.1		125.2			173.7			222.2			270.7	
30	400 120 200	07.3	80		19.4	30	126,1	31.5	80	174.6			223.2			271.7	
	-	07.5	81		19.6		127.1		181	175.6			124.1			272.6	
31		07.7	82		19.8		128.1			176.6			225.1			273.6	
33	22.0	08 0			20.1		119.0		83			33	226.1	56 4		274.6	
34	22.0	08 2	84		20.3		130.0		84	178.5		34	227.0	56.6		275.6	
35	34.0	08.5	85		20.6	35	131.0	32,7	85	179.5		35	228.0	56.9		276.5	
36		08.7	86	_	20.8	136	132.0		186	180.5			229.0	57.1	286	277.5	60.
37	34.9	09.0	87		21.1	37	132.9		87	181.4			230.0		87	278.5	60.
38	26.0	09.2	88	85.4	21.3	38	133.9		88	182 4	45.5		230.9		00	279.4	16-
39	37.8	09.4	89	86.4	21.5	39	134.9	33.6		183 4			231 9	57.8	89	280.4	69.
40	38.8	09.7	90	87.3	21.8	40	135.8	33.9	90	184.4	46.0	40	232 9	58.1	90	281.4	70.
40	-	09.9		88.3		141	136.8		101	185.3	46 2		233.8			282.3	-
42	40.8	10.2	92	80.2	22.3	43	137.8	34.4	92	186.3	46.5	42	234.8	58.6	92	283.3	70.
43	49.7		93	90.2	22.5	43	138.7	34.6	93	187.3	46.7	43	235.8	58.8		284.3	
44	42.7	10.6			22.7	44	139.7	34.8	94	188.2	46,9	44	236.7	59.0	94	285.3	71,
	43.7	12.9		92.2		45	140.7	35.1	95	189.2	47.2	45	137.7		95	286.2	71.
45	44.6		_	93.1			141.7			190.2	47.4		238.7			287.2	
47	45.6	11.4	97	94.1	23.5	47	142.6	35.6	97	191.1	47.7	47	239.7	59.8	97	288.2	71.
48	46.6	11.6	98	95.1	23.7	48	143.6	35.8	98	192.1	47.9	48	240.6	60 0		289.1	
19	47.5		99	96.1	24.0	49	144.6	36.1	99	193.1	48.2		241.6			290.1	
	48.5						145.5		200	194.1			242.6			291.1	
	-	Lat		Den			Dep		Diff		Lat		Dep	Lat	5:4	Dep	1

for 76 Deg.

Difference of Latitude and Departure for 15 Deg. 15

-	las dies T	Diff	Lat	Deul	Dift	Lat	Dep.	Dia	Lat	Deil	IDia	Lat.	/Dei I	Dia	Lat	Den
DI			_	-	_		-	_			_		-	_	_	
. 1	01.000,3		49,3		101	20			145,8			194.1			242.4	
3	01.9 00 5		50.2	13.5	02	98.5			147.8		02	195.1	52.3		243.4	
3	02.9 00.8		51.2	13.7	03	100.5			148.7			197.0		53	244.4	
4	01.001.0		52.2	14.0	05	101.4		55	149.7		05	198.0	52 1	54	245.3	
_5	04.8 01.3		53.1	_	-		-							55	_	66.0
6			54 1	14.5	108	102.4			150.7			199.0		256	247.3	66.3
7	06.8 01.8			14.8		103.4			152 6			199.9			248.2	66.5
8		_	Mar	15.0	09	105.3	28.2		153.6		09	201.9		58		66.8
9	08.7 02.3		57.0	15.5	10	106.2		60	154.5		10	202.8		59	250.2	67.3
10			_		-		_	161		_	-			-		
11			58,9	15.8	111	108.2			155,5		12	203.8		6-	252.1	
12	11.6 03.1	64	59 9 60.9	16.3	13	109 1			157,4		13			62	253 1	67.8
13	1 5 0		61.8	16.6	14				158 4		14			64		
14			62.8	16.8	15	111.1			159.4		15	207.7		65		
15				17.1	116	112.0	_		160.3		216	208.6		266		
16	15.5 04.1		63 7	17.3		113.0			161.3			209.6			257.9	68.8 69.1
17	17.4 04.7	68	65.7	17.6		114.0			152.3		18	210.6		68		60.4
119	0 1		66.6	17,9	19	114.9		69	163.2		19	211.5			259.8	
20	19.3 05 2		67 6	18,1	20		31.1	70	164.2	44,C	20	212.5			260.8	
1 -			63,6	18.4	121		31.3	171	165.2	44 3	221	213.5		271		
21			69.5	18.6	22		31.6		166.1		22	214.4		72	1 .	70.1
23			70.5	18.9	23		31.8		167.1		23		57.7	73		
24	1 1	1	71.5	19.2	24	119 8	32.1	74	168,1	45.0	24	216.4	58.0	74		70.9
25			72,4	19.4	25	120.7	32.4	75	169 0	45.3	25	217.3	58.2	75	265.6	71.2
1 26		76	73.4	197	126	121.7	32.6	176	170.0	45.5	226	218.3		276	266.6	71.4
27			74.4		27		32.9		171.0		27	219.3	58 7	77	1	
28			75.3		28			78	171.9	46.1	28			78		
29	28.0 07.5	79	76.3		29		33.4		172.9	46 3	29	221.2		79	269.5	72.2
30	29.0 07.8	80	77.3	20 7	30	125.6	33.6	80	100	46.6	30	222.2	59.5	80	270.5	72.5
31	29 9 08 c	81	78.2	21.0	131	126.	33.9	18:	174.8	46.8	231	223.1	59.8	281	271.4	72.7
32		82	79.2		32				1		32	224.1		82	272.4	
33			80.2	21.5	33	128.	34.4	83	176.8		33	225.1	1 -	83	273.4	
34	32.8 08,8	84	81.1		34	129.4		84	177-7		34		60.6	84	274 3	73.5
35	33.8 09,1	85	82.1	22.0	35		34 9				35	_	60.8	85	275-3	73.8
36	34,8 09.3	86	83,1	22.3	136		35.2				236	228.0		286	276,2	74.0
37	35.7 09,6	87	84.0	22.5	37	132,	35.5	87	180.	48.4	37	228.9		87	277.2	74.3
38		88	85.0	22.8	38	133.3	3 35.7	88	181.	40,7	38	229.9	61,6	88	278.2	74.5
39		89	86.0	23 0	39	134.	30.0	89	182.	40.9	39	230	61.9	09	279.2	74.0
40	38.6 10.4	1 90	80.9	23.3		135.2	130.2	90	183.						280.1	
41	39.6 10,6		87.9	23.6	141	136.	36.5	191	184.	49,4	241	232.			281.1	75.3
42		92	88.9	23.8	42	137.2	30,7	92	185.	149 7	42	233,	02.6	92	282.0	
43		93	89 8	24.1	43	138	37.0	93	186.	149.9	43	234.	02.9	93	283.0	
44			90.8	24.3			37.3	94	187.	150.5	44	235.	6 63.4		284.0	
45	A DESCRIPTION OF PERSONS ASSESSED.			24,6	45		37.5		188.				_		284.	
46		90	92.7	24.8	146		37.8	196	189.	3 50.7	246	237.	6 63.7	129	285.	76.6
47		97	93.7	25.1	47	142.	33.0	97	190.	3 51,0			6 63.9		7 286.	70.9
48		90	94.7	25.4	1 48	143	30,3	9	191.	57.4	1 3	239.			287.	
59				25.6	1 49	144.	0 28 9	1 20	193.	2 51.8	250	240.			289.	8 77.4
	Dep 1.a.	_				De			De						A Dep	
-	m Debil'a.	(lom	Inel	Lat	Ilpii	i De	piLat	Hp.	n De	P. La	Di	AlDep	Lat	וטון	a Dep	Lat

Dep 60 7 61 0 61.2 62.0 62.2 62.4 62.7 62.0 63.4 63.9 63.4 63.9 63.4 63.9 63.9 63.8 6

for 75 Deg.

- 0	- 1	B 11	D:0	1	Dani	Dift	Line	Dept	Die	Lat	Derl	Did	Lat.	Decl	Ditt	Lat	1000
_	_	Dep	Dill			-	-		-			-		-	-		_
1	01.0		51	49,0	14.3	101	97.1	27.8		145,1		1	193.2			241.2	69.2
2		00 6	52		14.3	02		28.4	2100	146.1		02	194.1			242.2	1
		00.8		50,9	14.6	03	100.0		54	147.1		04	196.1	55 9	53	243.2	70.0
4		01.1	- 8	51.9		05	100.9		55	149.0		05	197.0		55	245.1	76.3
_5	_	01.4	55	52.9	15.2						-	-	198.0	1			-
6		01.7	56	53.8	15.4	100	101.9		156	149 9		206		57.0	57	246 0	70.6
7		01.9	57	54 8	15.7 16.0	08				151,9		08	1	57,3	58	248.0	
8	08.7	02.2	59	55.7	16.3		104.8			152.8		09		57.6		248.9	
9		02.8	60	57.7	16.5	10	105.7		6c	153.8		10		57.9	60		71.7
-	-	-	61	58.6	16.8	11:	-	30.6	161	-	44.4	211	1	58.2	261	-	
11		030	62			12	107.6	20.0		155,7				8 58.4		100	
12	7	03.3	10	60.6		13		31.1	63	156 7	44.9	13	204.	58.7	63	252.8	
13		03.9	1 4 .	61.5		14	109.6	31.4			45.2			7 59.0	64		72.8
15	1 - 7	04.1	65		10000	15		31.7	65		45.5	15	206.	6 59 3	65		
15	-	04.4	66			116	-	32.0	166	150.	1-15.7	216	207.	6 59.5	266		
17		04.4		64.4				5 32.2	11 .	1 30 .	5 46.c	6 1		6 59 5	67	1 33 .	
18		05 c	68					4 32.5			5 46.3		209.	5 60.1	58		
19		3 05.2	69	66.		19	114.	4 32.8	69	152.				5 60,4		258.5	
20	1	2 05 5		67		20	115.	3 33,1	70	163	4 46.0	1 20	111.	4 60 6	70	259.	74 4
21		2 05.8		68,2	196	121	116.	3 33.3	171	164.	4 47.1	221	212.	4 60.9	271	260.5	74.7
22			1 73	69 2			117.	- 1		16.5.	3 47 4	22		4 61.2		261.4	75.0
23	22.	1 06.3			2 20.1	11	118.	2 33.9	73	166.			214.	3 61.5		262.4	
24	23.	1 06 6	74	1 71.1	20.4	24	1119.	2 34,2			2 48,0	1 1		- 10	11.		1 -
25	24.	c 06 g	7	72,	1 20 7	2	120.	1 34.4	7	-	2 46.2	-		-	1	-	
26	25	0 07.2	1 7	73.0	20.9	120	6 121.	1 34.7	1 17		2 48,			2 62.3			
27	26,	0 07.4	7		21.2			1 35.0			1 48.	1 1 4		2 62.6			. 10
28		9 07.7		8 75.	0 21.			0 35.			1 49.	11		1 62.8			
29	-	9 08		- 10.0				0 35.	- 11 -	9 172.				1 63.4		269.	
30	-	8 08.	- 1 -	- /-	9 22.0	-11-		9 35.		_	0 49		-	_			
31		8 08,			9 22.		1 125	9 36.	1 18		0 49.			063.7		1 270.	
32		8 08,		2 78.	8 22.			9 36.			9 50.			0 63			
3:		7 09,	110		8 22.		-	8 36.			8 50.			9 64.		4 273	
3.		7109.	. 0		7 23			8 36,	- 1 0	5 177				.9 64			
3		_	_	5 81.	_	-	_				.8 51.		_	.8 65.0		6 274	
3	6 34			6 82.				7 37-			7 51.			.8 65.	8	7 275.	
3		.6 10,			6 24			7 37.		8 180		- 1	0 0	.7 65.	6 8	8 276,	8 79.4
3		.5 10.		0 85	6 24.		8 132 9 133	6 28.	2 8	9 181	7 52,	1 3		.7 65.	9 8	9 277.	8 79.
3		4 11.	7 6	0 86.	5 24.	8 4	0 134	.6 38.	6 9		.6 52.	4 4	0 230	7 66.	1. 9	0 278.	7 79.9
40							1 125	.5 38.	9 19	-	.6 52.			.6 66.		1 279.	
4		4 11,		2 88	5 25.	4	2 136	.5 39.	1 0	2 184			2 232	.6 66.	7 9	2 280.	6 80.
4		4 11.		3 89.	4 25.	6 4	3 137	4 39.	4 9	3 185		2 4	3 233	,6 67.	0 9	3 281.	6 80.
4		3 12.		4 90.	3 25.	9 4	4 138	4 39.		4 186			4 234	.5 67.	2 9	4 282.	6 31.
4		3 12.		5 91.	3 26,	2 4	5 139	,4 40.			.4 53.		5 235	. 5 67.		5 283.	
4		.2 12,	-11	6 92.	3 26.	5 14		.3 40.		6 188		0 24	6 236	.4 67.	8 29	6 284	5 81.
14		.2 13,		7 92	2 26.	7 4	7 141			7 189		3 4	7 237	.4 68	1 9	7 285	5 81.
4		.1 13.	2 9	8 94	2 27.	0 4	8 142	.2 40.		8 790		6 4	8 238	.4 68.	3 9	8 286	4 82.
4		1 13.			2 27.	3 4	9 143	.2 41.	1 9	9 191	.3 54	8 4	9 239	.3 68.	6 9	9 287	
1 5	2 48	. 1 13,	8 16		.1 27.		0 144	.2 41.		0 192	.2 55	-	_	.3 68.	- -	288	
1-	70 5	p La	10	ialDe	pLa			eplla	t D	ft D	ei Li	D	if De	p /La	D	if Dep	La

Difference of Latitude and Departure for 17 Deg. 17

-	-	_		.0.	-	Dest	ID:A	Lat	Dep	ID.A	Lat	Davi	ID:A	Les	Dest	10:0	. 1	
A C	Lat	Dep	110	utt	Lat	Dep	חות			Din	Lat	Det	_	Lat.	De;	Dift	Lat	Del
1	01.0	00,3	1 5	1 4	8,8	14.9	101	96.6	29,5	151	144.4	44.1	201	192.2	58.8	251	240.0	73-3
	01.9	00.6	115	2	19,7	15.2	02		29.8	52	145,3	44.4	02	193.2	59.0	52	241.0	73.6
	02.9	00.9				15.5	03	98.5	30.1	53	146.3	44.7	03	194.1	59-3	53	2+1 9	73.9
4	03.8	91.2	11 5	4	51.6	15.8	04	99-4	30.4		147.3		04			54	242.9	74.3
5	04.8	01.		55	52.6	16.1	05	100.4	30,7	55	148.2	45.3	05	196.0	59.9	55	243.8	74.4
6	05.7	01.5	- 1		53.5	16.4	106	101.4	31.0	156	149.2	45 6	206	197.0	60.2	256	244.8	74.7
	06.7					16.7	07	102.3		57	150.1	45.9	07	197.9			245.8	
	07.6			~		17.0	08	103.3		58	151,1	46.2	08	198 9		58	246 7	75.3
9	08.6					17.2	09	104.2	31.9	59	152.0	46.5	09	199 9			247.7	
10	09.6	32.0				17.5	10	105.2	32.2	60	153 0	46.8	10	200.8	614		248.6	75 9
11	_	03:	-11	_		17,8	111	106.1	32.4	161	154.0	47,1	211	201.8	61.7	261	249.6	76.2
12		03.			59.3	18,1		107.1		62	154.9			202.7			250.5	
13		03.	211	_	33 3	18.4			33,0	63	155,9	47.6		203.7		61	251.5	76.8
14		04.				18.7			33.3		156.8			204.6			252.4	
15		04.				19.0	15		33.6	65	157,8	48,2	15		62.8	65	2534	77.4
_			-11	-		_	116			166	158.7		216	-			254.4	
16		04.				19.3			33.9		159.7			207.		67	255.4	77.7
17		05.				19.6			34.5	68	160 6					68	255.3	77,9
18		05.	-11			20.2			34.8		161.6		19		64.0		257.2	78,5
19		05.	- 7 -			20.5			35.1				20		64.2		258.2	10 00
20	-	05.	_ 11	-	_	_												-
21		06.		71	67.9	20 8	121		7 35-4	171	163.			211.	64 6		259.1	
22		06				21.0			35.7		164.				64.9		2000	79 4
23		06.	111			21.3	-		6 36.0		165.4			213.2			261.1	
24	1	07.	- 11			21.6			6 36.2		166.				65.5		262.0	
25		97		_	71.7	-			5 36.5		167.				65.8		263.0	
26	24.	9 07.	6	76	72,7				5 36.8		168.		226		66.1		263.9	
27		07	-11		73.6		11 6		4 37.1		169.			217.			264.9	
28		8 08			74.6		11	A 12 CO	4 37-4		170.			218.0			265.8	
29		7 08				23			4 37.7			2 52.3			66.9	79	266.8	81.5
30	28.	7 08	١	80	76.5	23.4		_	3 38.0		172.	_			67.2		267.7	
31	29.	6 09	,1	81	77.5	23.7	131	125.	3 38.3	18	173.	1 52.9	231	220.	9 67.5		268.7	
32	30.	6 09	4			24.0	32	126.	2 38,6	82		0 53 2	32	221.			269.7	
33	31.	6 09	,6		79-4				2 38 9	1 83	175-	0 53	3:		8 68.1		270.6	
34		5 09			80.3				1 39.2	84	175.			1223.	8 68 4	1 84	271.6	
35		5 10	,2	85	81.5	24.	3	-	1 39.		170.	9 54		-	7 68 7		272.	83.2
36	34,	4 10	.5	86	82.2				0 39.8		1 / /	9 54.4		225.	7 69.0		173.	
37	35.	4 10	.8	87		25.	4 3	131	0 40.0	8	178.	8 54.	3		6 69.3	8	7 274-4	1 83.8
38		3 11		88	84.1	25.	7 3	132	0 40.	3 8	8 179.	8 55.	3	227.	6 69.6		8 275.	4 84.1
39	37.	3 11	4	89	185.1	1 26,	0 3	132	9 40.	8	180.			123			9 276,	
40	38.	2 11	.7	90	86.1	26.	3 4		9 40.		181.	7 55.	5 4	229.	5 70,2	9	0 277.	3 84.7
41		2 12	.0	91	87.0	26.	6 14	1 134	8 41.	2 19	1 182	6 55.	8 24	1 230	5 70.4	1 29	1 278.	3 85.0
42		2 12				26.	0 4	2 135	.8 41.	5 9	183.	6 56.	1 4	2 231		1 9	2 279.	2 85.
43		1 12		93		27.	2 4	3 136	7 41.	8 9	3 184	6 56	4 4	3 232		9	3 280.	2 85.
44		1 12		94	89.	9 27.	5 4	4 1 37	.7 42.	7 9	4 185	.5 56.	7 4	4 233	3 71.	3 9	4 281.	
		0 13		9.5		8 27.	8 4	5 138	7 42.	4 9	5 186	.5 57.	0 4	5 234	3 71,	6 0	5 282.	1 86.
45	44	0 13	- 1	96	01.	8 28.	1 14	6 130	,6 42.	7 19	6 187	4 57	3 24		.2 71.	9 20	6 283.	0 86.
47		9 13		97	02.	8 28.	4 4	7 140	.6 43.	0 9	7 188	.4 57.	6 4	7 236	.2 72.	1 0	7 284	0 36.
4		9 14	.0	08	92.	7 28.	6 4		.5 43.		8 180	.3 57	9 4	8 237			8 285	
45		9 14	, 3	90	94.	7 28.	9 4		.5 43.	6 9	9 190	.3 58	2 4	9 238	.1 72.	-11	9 285	
5	47.	8 14	,6	100	05.	6 29	2 15		4 43.	8 20	0 191	.2 58	5 20	0 239	.1 73	0 30	286	.9 87
	it De	E I							e _i La			er L		if De			ift De	
,		h.3"			100	1100	.112		1	11-	1 2	11.	11-		7 24	III	T.L DC	La



for 73 Deg.

18 Difference of Latitude and Departure for 18 Deg.

_			-		_				151					_	1000	-	-41
DE	t La:	Dep	Dif	Lat	Dep	Dif	Lat	Dep	Dif	t Lat	Dep	Diff	Lat.	Dei	Dif	Lat	De
-	-	200	-	-	_	101	96.		151	1.40	46.7	1	191.2	6-			1-
1		00,3	51													238.7	
2	1 .	00.6	52	7.00	116.1	02		31 5		144.6			1			239.7	
3	02.9	00.9		50.4				31.8		145,5			1			240.6	78.2
4	03.8	01.2	54	51.4	16.7	04	98.	32.1	54	146.9	47.6	04	194.0	63.0	54	241.6	78,5
5	04.8	01.5	1 55	52.3	17.0	05	99-	32.4	55	147.4	47.9	05	195.0	63.3	55	242.5	8.8
6		-			1	105		32.8		148.4		206	-				-
	1 3 "	01.9		53.3												243.5	79.1
7		02.2		54 2				33,1		149.3	40.5	07	196.9			244.4	79 4
8		02.5		100				33.4			48.9		1-21				79-7
9		01.8	59	56.1	18,2			33.7		151,2		09	198 8	64.6	59	246 3	80.0
10	09.	03.1	60	57.1	18.5	10	104.	6 34,0	60	152.2	49,4	10	199.7	64.9	60	247.3	80.3
11			61			111	Los	6 34.3	161	100 1	49 7	211	200.7	500	261	-	
		03.4	62	10	1000000	1				154.1	1 27	12			100		80.6
12		03.7		133 -		12		5 34.6	6-	154.1	50.1	100	201.6	1		249.2	81.0
13		104.0		59.9			107.			155,0		13					81.3
14		04.3		60.9		14	108.			156 0		14	203.5				81.6
15	14.	04.6	05	61.8	20.1	15	109	4 35.5	05	156.9	51,0	15	204.5	66.4	55	252.0	81.9
16	1150	04.9	66	62.8	20.4	1116	110.	25.8	166	157,9	51.2	216	205.4	65.7	-	_	82.2
	1 - 3	05.3		63.7			111.	126.2	62	158.8	51.6	17					
17		1	60	64.7	20.7				68			18			60	253 9	82.5
18		05.6				11		36.5	1 60	1-32			207.3	10	6.	254 9	82.8
19		05 9		65.6		11 -				160.7		19	208.3			255.8	83.1
20	19.0	06 2	79	66.6	21.6	20	114.	37.1	70	161.7	52 5	20	209 2	68.c	70	256.8	83,4
21	200	06 5		67.5		121	115.	37.4	171	152.6	52.8	221	210 2	68 2	271	257.7	33.7
22		06.8	72	68,5	22.2	22		37.7		163.6		22	211.1	68.6		258.7	84.0
		4				11		38.0						100			34.0
23		07.1		69.4		-				164.5		23	212.1			259.6	84.4
24		07.4	74			24		38,3		165.5		24				200.6	84.7
25	23.2	37.7	75	71.3	23 2	25	118.	38.6	75	166.4	54.1	25	2140	09.5	75	261.5	85.0
26	24.7	08 0	76	72.2	23.5	126	110	38.9	176	167.4	54-4	226	214.9	60.8	276	262.5	85.3
27		08.3		73.2	23.8		120.			168.3			2159			263.4	
28		08,7	78	74.2		28		39.6		169.3		28	216.8				85.9
136.7.5						11						1 2 3 3 3	217.8				
29		09,0	79			29		39.9		170.2		29				265.3	86.2
30	28.5	09.3	80	76.1	24,7	30	123.0	40.2	80	171.2	55.6	30	218.7	71.0	80	266.3	86.5
31	20.5	09,6	81	77.0	25.0	131	124.6	40.5	181	172.1	55.9	231	219.7	71.4	281	267.2	86.8
32		09 9	82			32		40.8				32	220.6			268.2	87.1
33		10,2		78.9	25.6	_		41.1	83				221.6			260.1	87.4
34			84		26,0	34	The second second	41.4		175.0		34	222.5			270.1	87.8
		10.5		1000													
35	33.3	10.8		80.8	26.3	35	128.4	41.7	85			35	223.5	72.0	85	271.0	88.1
36	34,2	11.1	86	81.8	26.6	136	129.3	42.0	186	1-/2		236	214.4	72.9	286	272.0	88,4
37		114	87	82.7	26.0	37	130.3	42.3	87			1000	225.4	73.2	87	272.9	88.7
38	36.1	11.7	88	83,7	27.2	38	131.2	42.6	88	178.8	58.1	38	226.3			273.9	89.0
		12.1	180	84.6	27.	30	132,2	42.0	80	179.7	58.4	1 30	227.3	72.0	80	274 8	80.2
			100	8.6	2.3	39	30,2	42.0		180 -	58	40	128 0	73.9	00	276 8	80.6
40	38.0	12.4	90	85.6	27.0		133.1		90	180.7			128.2				89.6
41	39.0	12,7	91	86.5	28.1	141	134.1	43.6	191	181.6	59.0		229.2		291	276,7	89.9
42		13,0	92	87.5	28.4	42	135.0	43.9	92	182.6	59.3		230 1		92	277.7	90.2
42	40.9	13.2	93	88.4	28.7	42	136.0	44.2	01	183.5	59.6		231.1		01	278.6	90,5
44	41.8	12.6	94		29.0	44	136.9	44.5	94	184.5	59.0		232.0		04	279.6	90.8
AF	42 9	13.0	95	00.4		AC	137.9	44 8	100	185.4	60.3		233,0				91.2
끄	42.8		95	90.3	-9.4				95				_				91.2
45 46	43.7	14.2	96	91.3	29.7		1388		196	186.4	60.6	246	233.9	76.0	296	281.5	91.5
	44.7	14,5	97	92.2	30.0	47	139,8		97	187.3	60.9	47	234.9	76.3	97		91.8
	45.6	14,8	98	93.2	30.3		140.7		98	188.3	61.2	48	235.8	76.6	98	283.4	92.1
	46.6		90	94.1	30.6	40	141.7	46.0	99	189.2	61.5		23618			284.3	
	47.6			95.1		150	142.7	46.4	200	190.2	61.8		237.8		200		92.7
	1/.0	3.3	2:0	33.4	30.9	3	/		= 0	-95.2							
utt!	Depl	Lat [Diff	Dep 1	Lat	Diff	Depl	Lat	DH	Dep	Lat	Ditt	Dep	Lat	Dift	Deb	Lat
				1000				20, 20		1 1 2 2		2000	4. 12 mil 3	100 100			~

for 72 Deg.

	-	-		IT -	(Dan)	ID:A	Lat	Deul	Dift	Lat	Deili	Diff	Lat	Derki	Diffi	Lat I	Den
Dift	Lat	Dep	וועו	Lat	Dep	Dill					-				-	_	-
1	00 9	00.3			2 16.6	101	95.5		- 1	142.8			1900		251	37.3	81.7
1		00.7	11 -		2 16.9	02	96.4		3-1	143.7	- 6		191.0		52	238.3	32.4
3		01.0			1 17.3	03		33.5	1 33	144.7			192.9		53	140.1	32.7
4		01,3			1 17.6	04		33.9		146.5		05	193.8		55	241.1	8201
5	-	01.6			0 17.9			34.2	55	-	-	_			-		
6		02.0			9 18 2	106	100.2			147.5			194.8			242.0 243.0	
7		02.3		53.	9 18,6 8 18.9	08	101.2			149.4			196.7		58	243.9	84.0
8		02.6		34	8 19.2	00	103.1		50	150.3	51.8		197.6	4.0	50	244 9	84 3
10		03.3			7 19.5	10	104.0			151.3			198.5			245.8	
-				_	7 19.9	111	-	-	161	152.2	52.4	211	199.5	68.7	-	246.8	
11		103.6	11 -		6 20.2		105.9	26.5		153.2			200.4			247.7	
13		3 04.2	11 0		6 20.5					154.1			201.4	-		248.7	
14		2 04.	- 1		5 20.8		107,8		1	155.1		14	202.3	69.7			86.0
15		2 04,	11		5 21.2				65			15	203.3	70.0	65	250.5	86.3
16	-	105.		6 62	4 21.5	116	109.7	37.8	166	-	54.0	216	204.2	70.3	266	251.5	36.6
17	1 2	1 05.			.3 21.8		110.		67	157.9	54-4	17	205.2	70.7	67	252.4	86,9
18		0 05,	- 11		.3 22.1		111.6	38.4		158.8			206.1			253.4	
19	13.	06.	2 6	9 65	.2 22.9	19		38.7	69	159.8			207.1			254.3	
20	18.	9 06.	5 7	0 66	2 22.8	20	113.	39.1	70		55.4		208.0	-		255.3	
21	19.	9 06.	8 7		.1 23,1		114.	1 39-4	171	161.			208.9				88.2
22		8 07.			.1 23.4	-11		3 39.7	72	162.	56.0	22	209.9			257.2	
23		7 07.	211		.0 23.			3 40.0	73	163.	50.3	1 2	210.8				38.9
24		7 07			.0 24	24	117.	40.4		164.	5 50.7	1	211.8				89.2
25		6 08.		-	1.9 24			_			5 57.0			-	-		-
26	24	.6 08	5 7		.9 24			1 41,0			4 57-3		213.7				989.9
2	25	.5 08.	0 7	_	.8 25.	- 1	120.			168.	2 58.0		215.				8 90.5
21		5 09		1	1.7 25.	11	122.		7	169.	2 58.	20	216				8 90.8
1.7		.4 09			26.		12 17 15 15 15 15	9 42,3		170.	2 58.	6 30	217.				791.2
30	_	.3 10			6.6 26.		1 123			_	1 58		1 218.	4 75.2	281	265	791.5
3		.3 10			7.5 26		124.			172.			2 219.				6 91.8
3		.2 10			8.5 27.		3 125				0 59	6 3	3 220.				6 92.1
13	_	.1 11		-	9.4 27.	4 3	4 126	7 43.	8	4 174.	0 59	9 3	4 221.				5 92,5
		.1 11		85 8	0.4 27.	7 3	5 127	6 44.0	8	5 174	9 60,	2 3	5 222.	2 76.5	-	-	5 92.8
3	6 34	.0 11	.7		1.3 28			6 44			9 60.		6 223.		28	6 270.	4 93.1
3	7 3	,0 12	,0	87 8	2.3 28	3 3	7 129	.5 44.		7 176	.8 60	9 3	7 224.		8	7 271	3 93.4
3	8 3	5.9 12	1.4		3 2 28		8 130	.5 44		8 177	7 01.	2 3	8 225.	0 77.5	8	8 272	393.8
3		5.9 12		89 8	4.1 29	0 3	9 131	4 45	8	9 178	6 61	5 3	9 226.	0 78	11 0	9 273	.2 94.I
14		7.8 1			5.1 29			4 45.		0 179			0 226.				.1 94,4
14	1 3	8.8		918	6.0 29	.6 14	1 133	-3 45	9 19		6 62.		1 227	9 70.	29	1 275	1 94.7
		9.7 1		92 8	7.0 30	.0 4	2 134	.3 40.	6 9	3 182	. 5 62		2 228				.1 95.1
		0.7		93 0	7.9 30	3	13 135	1 46.	0 9	4 183	.4 63	2	3 229	7 79.	4 0	4 278	.095.4
		2.5 1		95 8	39.8 30		15 147	.1 47	2 0	5 184	4 63		5 231	6 79		5 278	.996 1
											.3 63		6 222	6 80			.9 96.4
	46 4	3.5	5.0	96	90.8 31	.6	46 138	0 47	5 19	7 136	.3 64	.1	6 232	. 5 80.	4 6	7 286	.8 96.
	48	4.4 I	5.6	98	92.7 3		48 139	0.9 48.	2 6	8 187	.2 64	.5	8 234	.5 80	7/ 3	8 281	1.7 97.
		6.3	6.0	99	93.6 3	2.2	49 140	0.9 48	5 6	9 188	.1 64	.8 4	9 235	4 81	1 0	99 28:	2.7 97
	50	7.3	6.3	100	94-5 3		50 14	1.8 48	8 20	189	1 65	.1 2	236	.4 81	4 3	00 28	3.6 97.
		Dep			DenL		if De			ill De			if De				ep La
1			V	1		-11											300 3

20 Difference of Latitude and Departure for 20 Deg.

Diel	Lat	Deuli	Diff	Lat	Depl	Din	Lat	Depl	H) (H	Lat	Derl	Dift	Lat	Dep	Dift	Lat	Dep
_			-	-	-	-			-	141.9		-	188.9		-	_	85.8
10.14	00.90			47.9		02	94 9 95.8		52	142.8	52.0		189 8		52	235.9	86.2
	02.8			49.8		03	96.8	25.2	53	143.8			190.8			237.7	86.5
	03.80			50,7		04		35.6	54	4 6 3 4 2	52.7	-	191.7		54	238.7	86.9
	04.7		55	51.7	18.8	05	98.7		55		530		192.6		55	239.6	87.2
-	05.6	_	-	52.6		106		36.3	156	146 6			193.6		256	240.6	87.6
1 1	06.6			53.6			100.5	26.6	57	147.5	53.4		194.5		57	241 5	87.9
	07.5			54.5			101.5			148.5			195 5		58	242,4	88.2
	08.5			55 4		1215	102.4		59	149.4	To 10 1 22 7		196,4		59	243-4	88.6
	09.4			56.4		10	103 4		60	150.4		10	197-3	71.8	60	244.3	88.9
111	10.3			57.3		111	104.3		161	151.3		211	198 3	72.2	261	245.3	89.3
12	11.3	4.1	1 - 1	58.3		12		28,3		152.2		1	199 2		62	246.2	89.6
13	12.2			59,2		13	106.2	38.6		153 2		13	200.2			247.1	89 9
14	13.2			60.1		14	107.1	39 0	64	154.1	56.1	14	201.1	73.2		248.1	90.3
15	14.1		65	61.1	22.2	15	108.1	39 3	65	155.1	56.4	15	232.0	73.5	65	249 0	90.6
16	15.0	05.5	66	62.0	22.6	116	109.0		166	156.0	56.8	216	203.0	73.9	266	250.0	91.0
17	16.0				22.9	17	109.9		67	156.9	57.1	17	203.9			250 9	91.3
18	16.9				23.3	18	110.9			157.9			204.0	74,6	68	251.8	91.7
19	17.9	06,5			23.6	19			69	158.8			205.8		69	252.8	92.0
20	18.8	06.8	70	65.8	23.9	20	112.8	41.0	70	159.7	58.1	20	206,7	75.2	70	253,7	92.3
21	19.7	07.2	71	66,7	24.3	123	113.7	41.4	171	160.7		22 I	207.7	75.6	271	254.7	92.7
122	20.7				24.6	22	114.6	41.7	72	161,6	58.8	22	208.6		72	255.6	93.0
23	21.6	07.9	73	68,6	25,0	23	115.6	42.1	73	162.6	59.2	23	209 6	76.3	73	256.5	93 4
24	22.6		74	69.5	25.3	24	116.5		74	163.5		24	210.5	1	74	257,5	93.7
25	23.5	08.6	75	70.5	25,7	25	117.5	42.8	75	164.4		25	211.4	77.0	75	258,4	94 1
26	24 4	08.9	76	71.4	26.0	126	118.4	43.1	176	165.4		226	212.4		276	259 4	94-4
27	25.4				26.3	27	119.3	43.4	77	166.3	60.5	27	213.3		77	260.3	94.7
28	26.3				26.7	28		43.8	78	167.3	60.9		214.3		78	261.2	95.1
29	27.3				27.0	29	Maria .	44,1	79	168.2			215.2		79	263.2	95.4
30	28.2	_		-	27.4	30		44,5	80	169 1			216.1	-	-	263.1	95.8
31	29.1		81		27.7	131	123.1		181	170.1			217 1		251	264.1	96.1
32	30.1				28.c	32				171 0			218.0	1	82	2650	96.4
33	31.0				28.4				83	172.0	62 0		219.0		84	266.g	
34	31,9				28.7	34		45.8	84		63.3	34	220.8		85	267.8	97.5
35	32.9	_			29-1	35	-		-	-	_		-		286	268.8	
36	33.8				29.4	136			186	174.8		_	222.7		87	269.7	97.8
					29.8		128.7			175.7			223.		88	270 6	
30	35.7 36.6	13.0	80	82,7	30.4	30	130.	47.5		176.7	64.6		224.	81.7			98.8
			00	84 6	30.8	40					65,0	40	225,	82.1	90	272.5	
40	3/10					Name and Address of the Owner, where	100	48 2		179.			226.		291		
42	38.5		91	86	31.1	141	133.	48.2	1 .91	180.4	65.7		227.	82.8	92		
43	39.5		92	87.4	31.8	42	134.4	48.0	02	181.4	66.0	41	228,	821		275.3	
44	41.3		04	88.	32.1	44		49.2	04	182.	66.3	44	229.		94	276.3	100.5
45	42.3		95	89.	32.5	45		49.6	95		66.7	45	230.	83.8	95	277.2	
46	43.2				32.8		137.						231.		296	278.2	
47	44,2				33.2	47	138.	150.2	07	185,	67.4	47	232.	34.5	97	279.1	
48	45.1				33.5			50.6	98	186.	67.7	48	233.0	84.8	98	280,0	
	46.c	16.8			33.9		140.		99	187.0	08.1	49	234.	85.2	99	281,0	
50	47.0		100		34.2	150	140.	51.3	200	187.	68.4	250	234.	85.5	300	281,9	102.6
	Det		Dif				Dep									Dep	Lat
-		The said	1				1	1	11-			"		All Agran			

	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Det	Dift	Lat	Dep
1	00.9	90.4	51	47.6	18,3	101	94-3	36.2	151	141.0	54.1		187.6		251	234.3	90.0
	01.9	00.7	52	48.5	18.6	02	95.3	36.6	52	141.9			188.6		52	235.3	90.3
3	≥2.8	31.1	53	49.5		03	96.2	36.9	53	142.9			189 5		53	236.2	90.7
4	03 7		54	50.4		04		37.3	54	143.8			190.4			237.1	91.0
5	04.7	01.8	55	51.3	19.7	05	98.1	37.6	55	144-7	55.6		191.4			238.1	91.4
6	05.6		56	52.3		106		38 0	156	145 7	55.9		192.3		256	239.0	91.8
7	06.5		57	53.2		07	99.9	38.3	57	146.6			193.2			239.9	92.1
. 8	07.5			54 1		08	100.9			147.5			194.2			240.9	92,5
9	08.4			55,1		09	101.8		59 60	148.5		10	195.1			241.8	92.8
10	09.	-	oc.	56.0	_	10	102.7		-	149.4	_	-				242.7	93.2
11	10,3		61	56.9					161	150.3	57.7		197.0		201	243.7	93.5
12	11.2			57·9 58.8			104.6		63	151.3	58.4		197.9			244 6 245 5	93 9
13	13,1			59.7		13	105.5		64	153.1	58.8		199.8			246.5	94,6
15	14 C		65	60 7		15	107,4		65	154.1	59.1		200.7			247.4	
16	14.9		66	61.6		116	108.3	-	166	155.0			201.6	_		248.3	95.3
17	15 9			ú2.5		17	109.3		10.00	155.9			202.6			249.3	95.7
18		06.5		63.5			110.2			156.9			203.5			250.2	96.1
19		06.8		64.4		19	111.1			157.8		19	204.4	78.5		251.1	96.4
20	18			65.3		20	112.1	43.	70	158.7	60 9	20	205.4	78.8	70	252.1	96.8
21	19.6	07.5	71	66.3	25.4	121	113.0	43 4	171	159.7	61.3	221	206.3	79.2	271	253 0	97.1
22	20.5	07.9	72	67.2	25.8	22	1139	43.7	72	160.6	61.6		107.2			253.9	97.5
23	21.5	08 2		68.1	26.2	23	1149	44.1	73	161.5			208.2			254.9	97.8
24		04.6	1		26.5	24	115.8		74	162.5			209.1			255.8	98.2
25	23 3	090	75	70.0	26 9	25	116.7	44.8	75	-		25	210.0	_	75	-	98.6
26	24 3	09.3		70.9	1	126	117.7			164.3		226				257.7	98.9
27	1 -	09.7	77		27.6	27	118.6		77	165 3			211.9			258.6	99.3
28		10.0		73.7		28	119 5			167 1	-		213.8		1 1	259.5	100,0
30	1 2	10.4		74 7		30	121.4	100		168.1			214.7			261.4	
31	28.9		81	_	19.0	131	122.3	-	-	169.0	1-		215.6			262.3	
32		11.5		76.5		32	123.3			169 9			216 5		82		
33		3.11	83	77.5		33	124.2						217.5			264.2	
34		12,2		78.4		34	125.1	48.0	84	171.8			218.4		84		101.8
35		12 5	85		30 5	35	126,1	48 4	85	172.7	66.3	35	219.4	84.2	85	266.1	102,1
36	33.6	12 9	86	80.3	-	136	127.0	48.7	186	173.7	66.7	236	220.3	84.6	286	267.0	102.5
37		13.3	87	81.2	31 2	37	127.9	49.1		174.6	67.0	37	231.2	84.9	87	267.9	102.9
38	35.5	13.6	88	82.1	31.5	38	128.9	49.5	88	175.5	67.4	38	222.2	85,3	88	268.9	
39		140	89	83.1	31.9	39	129.8	49,8	89	176.5	69	39	223.1	86.0		269.8	
40		14.3			32.3		1 30.7			177.4			224.1			270 7	
41	38 3	14.7	91	84.9	32.6	141	131 7		191	178.3	60 0	341	225.0	86.4		271.7	
42		15.1	32	86 9	33.0	42	132.6	150.9	92	179.3	60.3	42	225.9	87 7		272.6	
43		15.4	93	87.7	33.3	43	134.5	51.6	93		60.5	44	227.8	87.4	93	273.5	
45		16.1	94	88 7	34.0	45	135.4	52.0	95	182.1	69 9	45		87.8		275.4	
46		16.5			34 4		136.3			183.0			229.7			276.3	
47		16.8			34.8		147.3		07	183.9	70.6	47	230.6	88.5	07	277.3	106.4
48		17.2		91.5	35.1	48	138.2	53.0	98	184.9	71.0	48	231.5	88.9	08	278.	106.8
49		17.6			35.5		139.1		99	185.8	71.3	49	232.5	89.2		279.1	
50		17.9	100	93.4	35.8	150	140.1	53.8	200	186.7	71.7	250	233-4	89.6	300	280.	107.
-	2- 52	-					Dep		D:4	Dep	Lat	Dia	Dep	Lai	Die	Don	Lat

Difference of Latitude and Departure for 22 Deg.

Dist Lat Dep Dist Dist
a 0.19 0 7 52 48.2 19.5 02 94.6 38.2 52 140.9 56.9 03 187.7 75.7 53 23.7 94 93.7 01.5 54 50.1 20.2 04 95.4 39.0 53 141.9 57.7 03 188.2 76.6 53 234.6 94.6 39.7 55 51.0 20.6 05 97.4 39.3 55 143.7 58.1 05 190.1 76.8 55 236.4 95 235.9 17.6 4 95.4 96.1 95.9 17.6 4 95.4 95.7 95.1 17.6 95.2 36.4 95 237.4 95 237.4 95 237.4 95 237.4 95 237.4 95 238.3 97 96.0 2.2 56.5 17.2 2.1 99.2 40.1 57 145.6 58.8 206 191.0 77.3 256 237.4 95 238.3 90 96.3 30.3 4 59 54.7 21.1 09 101.1 40.5 58 146.5 59.2 08 199.9 77.9 98 238.3 90 96.3 30.3 4 59 54.7 21.1 102.9 41.6 61 56.6 22.5 110.2 91 101.1 40.5 111.1 40.8 42.3 60.3 121.1 105.0 41.6 62 57.5 23.2 112.0 38 42.0 63 158.4 23.6 63 159.1 44.5 11.1 11.1 104.5 62.5 5.5 23.3 4.0 14.0 105.7 42.7 16.1 11.1 105.7 42.7 16.1 11.1 105.7 6.0 1.3 15.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 105.1 11.1 11
a 0.1900 7 52 48.219.5 02 94.638.2 52 140.956.9 03 187.775.7 52 233.7 94 3 02.8 01.1 53 49.119.9 03 95.538.6 53 141.957.7 03 188.2 76.6 53 234.6 94 5 04.6 01.9 55 51.0 20.6 05 97.4 39.3 55 143.7 58.1 05 190.1 76.8 55 236.4 95 6 05.6 02.2 56 51.9 11.0 106 98.3 39.7 156 144.0 58.4 206 191.0 77.3 256 237.4 95 7 06.5 02.6 57 52.9 21.4 09 99.2 40.1 57 145.6 58.8 207 191.9 77.9 57 238.3 90 9 08.3 03.4 59 54.7 12.1 09 101.1 40.5 58 146.5 59.2 08 192.9 77.9 57 238.3 90 10 09 303.7 60 55.6 22.5 10 102.0 41.2 61 56.6 22.9 111 102.9 41.6 61 56.6 22.9 111 102.9 41.6 62 57.5 23.2 12 10.4 9.6 63 58.4 23.6 13 104.8 42.0 63 159.1 65.0 22.9 13 109.5 79.0 62 242.0 97 15 13.9 05.6 63 58.4 23.6 13 104.8 42.3 63 151.1 61.1 13 197.5 79.8 63 243.9 98 16 14 8 806.0 66 61.2 24.7 116 107.6 43.5 166 153.9 62.2 15 13.0 51.6 17 20.1 88.8 18 20.3 80.9 66 244.8 98
3 02.8 01.1 5 54 90.7 120.2 04 96.4 39 0 4 03.7 01.5 54 90.7 120.2 04 96.4 39 0 5 04.6 01 9 55 51.0 20.6 05 97.4 39.3 6 05.6 02.2 56 57 52.9 21.4 07 99.2 40.1 57 145.6 58.8 07 190.7 77.3 256 237.4 95 8 07 403.0 58 53.8 21.7 08 100.1 40.8 9 08 303.4 59 54.7 12.1 09 101.1 40.8 10 09 3 03.7 60 55 6 22.5 10 102.0 41.2 09 11.1 102.9 41.6 11 10.2 04.1 61 56.6 22.9 111 102.9 41.6 12 11.1 04.5 62 57.5 23.2 12 10 38 42.0 13 12.1 04.9 63 58.4 13.6 13 12.1 04.9 65 56.4 26.7 3.2 12 100.8 42.3 14 13 005.2 64 59.3 24.0 14 13 005.2 64 59.3 24.0 15 13.9 05.6 65 50.3 24.3 15 106.6 43.1 16 14 8 05.0 66 61.2 24.7 17 15 8 06.4 67 63.1 25.1 17 108.5 43.8 18 16.7 05.7 66.7 68 63.0 25.8 19 17.6 07.1 69 64.0 25.8 19 17.6 07.1 69 64.0 25.8 19 17.6 07.1 70 64.9 26.2 20 111.3 14.6 19 17.6 07.1 70 64.9 26.2 20 111.3 14.6 19 17.6 07.1 70 64.9 26.2 21 11.3 14.6 22 11.3 14.5 7 23 21.3 08.6 23 21.3 08.6 24 22.3 09.0 74 68.6 27.7 27.3 23 21.3 08.6 24 22.3 09.0 74 68.6 27.7 2.3 21 19.5 07.9 71 63.8 26.6 22 111.3 14.5 7 23 21.3 08.6 24 22.3 09.0 74 68.6 27.7 2.3 23 21.3 08.6 24 22.3 09.0 74 68.6 27.7 2.3 23 114.0 46.1 73 166.4 8.7 2 24 22.0 19.5 88.7 2.3 10.0 2.0 46.8 25 23.2 09.9 79.2 2.2 113.1 15.7 7 26 24.1 09.7 7 27 26 68.8 27.7 2.3 2 28 118.7 77.9 2.2 2.2 113.1 15.7 7 29 119.6 67.9 2.3 2.8 6 29 12.4 19.5 7 20 12.2 28.6 84.7 7 21 22.2 8.6 84.7 7 22 22 113.1 14.6 7 23 22.0 10.1 7 24 22.0 10.1 7 25 23.2 09.4 7 25 23.2 09.4 7 26 69.5 28.8 27 117.8 84.7 6 28 118.7 7.7 9.3 2.8 6 29 12.0 18.8 7 20 12.1 14.8 8 21 12.1 14.8 8 22 117.8 87.6 6 23 21.3 18.6 6 24 21.0 9.7 78.7 6 24 22.0 18.8 7 25 23.2 09.4 7 26 24.1 09.7 7 27 26 68.8 7.7 2.3 2 28 118.7 7.7 9.3 2 29 12.0 18.8 7 20 22.1 13.1 14.6 6.1 21 22.2 28.6 84.7 7 22 22 23.3 13.0 6.5 7 23 23.0 09.4 7 24 115.0 46.8 7 25 25.0 10.1 7 27 26 68.8 7.7 2 28 26 10.9 7 7 29 26 68
4 03.7 01.5 54 50.1 20.6 05 97.4 39.3 55 143.7 58.1 05 190.1 76.8 55 235.4 95 70.6 05.6 02.2 7 20.6 57 52.9 21.4 07 99.2 40.1 57 144.6 58.8 07 40.30 58 53.8 21.7 08 100.1 40.5 58 146.5 59.2 08 192.9 77.9 58 239.2 96 10.2 04.1 09.3 03.7 05.5 62.2 10 10.2 04.1 06 148.4 59.9 10 194.7 78.7 60 241.1 07 09.2 40.1 11 10.2 04.1 04.5 05.6 62.2 10 10.2 04.1 04.5 06 148.4 59.9 10 194.7 78.7 60 241.1 07 09.3 03.7 05.5 62.2 10 10.2 04.1 06 148.4 59.9 10 194.7 78.7 60 241.1 07 07.3 09.3 09.5 09.5 09.4 09.5 09.4 09.5 09.4 09.5 09.4 09.5 09.5 09.4 09.5 09.
5
6 05.6 02.2 56 51 9 1,0 98.3 39.7 156 144.0 58.4 206 191.0 77.3 256 237.4 95 23.2 1 07 99.2 40.1 57 145.6 58.8 07 191.9 77.5 57 238.3 39.0 90.0 30.3.4 65 53.8 21.7 08 100.1 40.8 59 147.4 59.6 09 193.8 78.3 60 241 1 09 101.1 40.8 59 147.4 59.6 09 193.8 78.3 60 241 1 07 194.7 78.7 59 240.1 194.7
7 36.5 02.6 5 75 23.9 21.4 07 99.2 40.1 57 145.6 58.8 07 191.9 77.5 57 238.3 96 98.3 03.4 58.5 17.7 08 100.1 40.5 58 114 58.5 9.2 08 192.9 77.9 58 239.2 96 10.0 99.3 03.7 60.5 56.2 5 10.1 102.0 41.2 11.1 04.5 62 57.5 13.2 11.1 102.9 41.6 11.1 104.5 62 57.5 13.2 11.1 102.9 41.6 11.1 104.5 63.8 43.3 61.3 104.8 42.0 62 150.2 60.7 11.1 105.7 64.3 63 11.1 105.7 64.5 65.0 50.3 14.3 15.1 106.6 43.1 15.1 15.1 15.1 15.1 15.1 15.1 15.1 1
8 07 4 03.0 58 53.8 21.7 08 100.140.5 59 146.5 59.2 08 192.9 77.9 58 239.2 95 90 8.3 03.4 59 54.7 12.1 09 101.1 40.8 59 147.4 59.6 09 193.8 78.3 59 240.1 97 10 102.0 41.2 61 56.6 22.9 111 102.0 41.6 62 57.5 23.2 12 103 8 42.0 62 153.0 56.5 62.5 57.5 23.2 12 103 8 42.0 62 153.0 56.5 62.5 57.5 23.2 12 103 8 42.0 62 153.0 56.5 62.5 57.5 23.2 12 103 8 42.0 62 153.0 56.5 62.5 64.5 13 104.8 42.3 63 151.1 51.1 13 197.5 79.8 63 243.9 98 14 13 0.05.2 64.5 93.2 4.0 14 105.7 42.7 64 152.1 51.4 14 198 4 80.2 64 244.8 98 15 13.0 0.5 6 6 66.2 24.3 15 106.6 43.1 65 153.0 61.8 15 199 3 80.5 65 245.7 99 17.6 0.7 1 15 8 0.6 4 67 62.1 25.1 17 108.5 43.8 67 154.8 62.6 17 201.2 81.3 67 247.6 108 18 16.7 05.7 70 64.9 25.5 18 109.4 44.2 68 155.8 62.9 18 202.1 81.7 68 248.5 100 18.5 07.5 70 64.9 26.2 20 111.3 45.0 70 157.6 63.7 20 304.0 82.4 22 30.4 08.2 20 2113.3 45.0 70 157.6 63.7 20 304.0 82.4 72 66.8 27.0 22 113.1 45.7 72 159.5 64.4 22 20 5.8 83.2 72 65.3 27.2 2113.1 45.7 72 159.5 64.4 22 20 5.8 83.2 72 66.8 27.0 22 113.1 45.7 72 159.5 64.4 22 20 5.8 83.2 72 252.2 101 253.3 10.4 84.6 17 77 71.4 28.8 27 17 78.4 66.5 16.3 26.5 16.3 26.5 16.3 26.5 16.3 27.7 17 10.8 47.6 77 14.4 28.8 27 17 78.4 66.5 16.3 26.5 16.3 26.5 16.3 26.5 16.3 26.5 16.3 26.5 10.5 78 72.3 29.2 28 118.7 17.8 47.6 77 164.1 66.9 67.4 29 25.0 10.5 78 72.3 29.2 28 118.7 17.8 47.6 77 164.1 66.9 67.4 29 25.0 10.5 78 72.3 29.2 28 118.7 17.8 47.6 77 164.1 66.9 67.4 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 21.2 3 3 5.8 79.2 25.7 10.4 28.8 27.1 17.8 47.6 77 164.1 66.9 67.4 29 21.2 3 3 3.6 12.4 28.7 79.3 1.5 3 122.4 49.4 28.3 160.6 67.1 33 30.6 12.4 28.7 79.3 1.5 34 122.4 49.4 28.3 160.7 68.9 31.8 31.6 0.6 7.8 23.1 14.2 86.5 10.3 31.8 12.1 79.9 11.2 8.7 76.0 30.7 32.1 12.4 49.4 82.1 167.0 66.9 67.4 33 30.6 12.4 83 77.0 31.5 34 122.4 19.0 68.5 171.5 69.3 34 11.0 87.7 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 84.2 60.3 31.6 0.6 77.8 85.
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22 20.4 08.2 72 66,8 27.0 22 113.1 45.7 72 159.5 64.4 22 205.8 \$3 2 72 252.2 101 23 21.3 08.6 73 67.7 27.3 23 114.0 46.1 73 160.4 64.8 23 206,7 83.5 73 253,1 102 24 22.3 09.0 74 68,6 27.7 24 115.0 46,5 74 161,3 65,2 24 207.7 83 9 74 254.1 102 25 23.2 09.4 75 69.5 28.1 25 116 9 46 8 75 162.3 65,6 25 208.6 84.3 75 255 0 103 26 24.1 09.7 76 70.5 28.5 126 116 8 47.2 176 163.2 65 9 226 209.5 84.7 276 255 0 103 27 25.0 10.1 77 71.4 28.8 27 117.8 47.6 77 164.1 66.3 27 210 5 85.0 77 256.8 103 28 26.0 10.5 78 72.3 29.2 28 118.7 47.9 78 165.0 66.7 28 211.4 85 4 78 257,8 104 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 35.8 79 258,7 104 30 27.9 11,2 80 74.2 30.0 30 120,5 48,7 80 166.9 67.4 30 213.3 86.2 80 259.6 104 31 28.7 11.6 81 75.1 30.3 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106.3 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106.3 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.3 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.3 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.3 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.3 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.3 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.3 35 217.5 69.3 35 217.9 88.0 85 264.3 106.3 35 217.5 69.3 35 217.9 88.0 85 264.3 106.3 35 217.5 69.3 35 217.9 88.0 85 264.3 106.3 35 217.5 69.3 35 217.9 88.0 85 264.3 106.3 35 217.5 69.3 35 217.
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23 21.3 08.6 73 67.7 27.3 23 114.0 46.1 73 160.4 64.8 23 206.7 83.5 73 253.1 102 24 22.3 09.0 74 68.6 27.7 24 115.0 46.5 74 161.3 65.2 24 207.7 83.9 74 254.1 102 25 23.2 09.4 75 69.5 28.1 25 116 9 46 8 75 162.3 65.6 25 208.6 84.3 75 255 0 103 26 24.1 09.7 76 70.5 28.5 126 116 8 47.2 176 163.2 65.9 226 209.5 84.7 276 255 9 103 27 25.0 10.1 77 71.4 28.8 27 117.8 47.6 77 164.1 66.3 27 210 5 85.0 77 256.8 103 28 26.0 10.5 78 72.3 29.2 28 118.7 47.9 78 165.0 66.7 28 211.4 85.4 78 257.8 104 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 85.8 79 258.7 104 30 27.9 11,2 80 74.2 30.0 30 120.5 48.7 80 166.9 67.4 30 213.3 86.2 80 259.6 103 31 28.7 11.6 81 75.1 30.3 131 121.5 49.1 181 167.8 67.8 231 214 2 86.5 259.6 104 31 28.7 11.6 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
24 22.3 09.0 74 68,6 27.7 24 115.0 46,5 74 161,3 65,2 24 207.7 83 9 74 254.1 102 25 23.2 09.4 75 69.5 28.1 25 116 9 46 8 75 162.3 65,6 25 208.6 34.3 75 255 0 103 26 24.1 09.7 76 70.5 28.5 126 116.8 47.2 176 163.2 65.9 226 209.5 84.7 276 255.9 103 27 25.0 10.1 77 71.4 28.8 27 117.8 47.6 77 164.1 166.3 27 210.5 85.0 77 256.8 103 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 35.8 79 258,7 104 30 27.9 11,2 80 74.2 30.0
25 23.2 09.4 75 69.5 28.1 25 116 9 46 8 75 162.3 65,6 25 208.6 84.3 75 255 0 103 26 24.1 09.7 76 70.5 28.5 126 116 8 47.2 176 163.2 65 9 226 209.5 84.7 276 255 9 103 27 25.0 10.1 77 71.4 28.8 27 117.8 47.6 77 164.1 66.3 27 210 5 85.0 77 256.8 103 28 26.0 10.5 78 72.3 29.2 28 118.7 47.9 78 165.0 66.7 28 211.4 85 4 78 257,8 104 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 35.8 79 258,7 104 30 27.9 11,2 80 74.2 30.0 30 120,5 48,7 80 166.9 67.4 30 213.3 86.2 80 259.6 104 31 28.7 11.6 81 75.1 30.3 121.5 49.1 181 167.8 67.8 231 214 2 86.5 281 260.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
26 24.1 09.7 76 70.5 28.5 126 116 8 47.2 176 163.2 65 9 226 209.5 84.7 276 255 5 103 27 25.0 10.1 77 71.4 28.8 27 117.8 47.6 77 164.1 66.3 27 210 5 85.0 77 256.8 103 28 26.0 10.5 78 72.3 29.2 28 118.7 47.9 78 165.0 66.7 28 211.4 85 4 78 257,8 104 25,0 10.9 80 74.2 30.0 30 120,5 48.7 80 166.9 67.4 30 213.3 86.2 80 259.6 104 31 28.7 11.6 81 75.1 30.3 121.5 49.1 181 167.8 67.8 231 214 2 86.5 281 260.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 34 217.0 87.3 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
27 25.0 10.1 77 71.4 28.8 27 117.8 47.6 77 164.1 66.3 27 210 5 85.0 77 256.8 103 28 26.0 10.5 78 72.3 29.2 28 118.7 47.9 78 165.0 66.7 28 211.4 85 4 78 257.8 104 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 85.8 79 258,7 104 30 27.9 11,2 80 74.2 30.0 30 120.5 48,7 80 166.9 67.4 30 213.3 86.2 80 259.6 104 31 28.7 11.6 81 75.1 30.3 131 121.5 49.1 181 167.8 67.8 231 214 2 86.5 281 260.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 39.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
28 26.0 10.5 78 72.3 29.2 28 118.7 47.9 78 165.0 66.7 28 211.4 85.4 78 257.8 104 29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 85.8 79 258.7 10.4 30 27.9 11.2 80 74.2 30.0 30 120.5 48.7 80 166.9 67.4 30 213.3 86.2 80 259.6 10.4 31.2 11.6 81 75.1 30.3 131 121.5 49.1 181 167.8 67.8 131 214.2 86.5 281 260.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 10.3 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106.3 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106.3 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106.
29 26.9 10.9 79 73.2 29.6 29 119.6 48.3 79 166.0 67.1 29 212.3 35.8 79 258.7 104 30 27.9 11.2 80 74.2 30.0 30 120.5 48.7 80 166.9 67.4 30 213.3 86.2 80 259.6 104 31 28.7 11.6 81 75.1 30.3 131 121.5 49.1 181 167.8 67.8 231 214.2 86.5 281 260.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 33 30.6 12.4 83 77.0 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1
30 27.9 11,2 80 74.2 30.0 30 120,5 48,7 80 166.9 67.4 30 213.3 86.2 80 259.6 104 31 28.7 11.6 81 75.1 30.3 131 121.5 49.1 181 167.8 67.8 231 214.2 86.5 281 260.5 103 32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
31 28.7 11.6 81 75.1 30.3 131 121.5 49.1 181 167.8 67.8 231 214 2 86 5 261.5 103 2 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 103 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
32 29.7 12.0 82 76.0 30.7 32 122.4 49.4 82 168.8 68.2 32 215.1 86.9 82 261.5 106 33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217.9 88.0 85 264.3 106
33 30.6 12.4 83 77.6 31.1 33 123.3 49.8 83 169.7 68.6 33 216.0 87.3 83 262.4 106 34 31.5 12.7 84 77.9 31.5 34 124.2 50.2 84 170.6 68.9 34 217.0 87.7 84 263.3 106 35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217 9 88.0 85 264.3 106
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35 32.5 13.1 85 78.8 31.8 35 125.2 50.6 85 171.5 69.3 35 217 9 88.0 85 264.3 106
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36 33 4 13.5 86 79.7 32.2 136 126.1 50.9 186 172.5 69.7 236 218.8 88.4 286 265.2 107
37 34.3 13.9 87 30.7 32.6 37 127.0 51.3 87 173 4 70.1 37 219.7 88.8 87 266.1 10
38 35.2 14,2 88 31.6 33.0 38 128.0 51.7 88 174 3 70.4 38 220.7 89.2 88 267.0 10
39 36.2 14.6 89 82,5 33.3 39 128 9 52.1 89 175.2 70.8 39 221.6 89.5 89 268.0 108
40 37 1 15.0 90 83.4 33.7 40 129 8 52.4 90 176 2 71 2 40 222.5 89.9 90 268.9 108
41 38.0 15.4 91 84.4 34.1 141 130.7 52.8 191 177,171.5 241 223.5 90.3 291 269.8 100
42 38.9 15.7 92 85.3 34.5 42 131.7 53.2 92 178.0 71.9 42 224.4 90.7 92 270.7 109
43 39.9 16 1 93 86.2 34,8 43 132.6 53.6 93 178.9 72.3 43 225,3 91.0 93 271.7 109
44 40.8 16.5 54 37 2 35.2 44 133.5 53.9 94 179 8 72.7 44 226.2 91.4 94 272.6 116
45 41.7 16.7 95 83,1 35.6 45 134.4 54.3 95 180.8 73.0 45 227.2 91.8 95 273.5 110
47 43.6 17.6 97 89.9 36.3 47 136.3 55 1 97 182.7 73.8 47 229 0 92.5 97 275.4 11
48 44,5 18.0 98 90.9 36.7 48 137.2 55.4 98 183.6 74.2 48 229.9 92.9 98 276.3 111
49 45 4 18.4 99 91.8 37,1 49 138 2 55.8 99 184.5 74,5 49 230 9 93.3 99 277.2 119
5 46 4 18.7 100 92.7 37.5 150 139 1 55.2 200 185,4 74 9 250 271.8 93.7 300 278.2 112
Ditt De Lat Dift Dep Lat Dift Dep Lat Dift Dep Lat Dift Dep L

Diff	Lat	D	Dift	Lat	Depl	(Dif	Lat	Depl	Diff	Lat	Deil	1Diff	Lat	Dep	1Dif	Lat	IDe
-	00,9	-	-	46,9	-	101	_	39.5	_	139,0	_		185.0			231.0	98
	01.8			47.9		02		39.5		139.9			185.9		1	232.0	
3	02.8			48.8		03		40.2	53	140.8	59.8	03			1	232.9	98
4	03.7	01.6	54	49,7	21.1	04		40.6	54	141,8	60.2	04	187.8			233.8	99
5	0.:.6	02 0	55	50.6	21 5	05	96.7	41.6	55	142.7	50.6	05	188.7	80.1	55	2347	99
6	05.5	02.3	56	51.5	21.9	106	97.6	41 4		143.6	60.9	206	189.6	80,5	256	235.6	_
7	06.4		57	52.5	22.3	07		41 8	57	144.5	61.3	07	190.5	30,9	57	236,6	
8	07.4		58	53.4	22.7	08			58	145.4	61.7	08	191.5	81.3	58	237.5	
9	08.3	03,5	59	54-3	23.1	09	100.3	42.6	59	146.4	62.1	09	192.4		59	238.4	101
10	09.2	03.9	60	55.2	23.4	10	101.3	43.3	60	147.3	62.5	10	193.3	82.0	60	239.3	101
11	10.1	04.3	61	56.1	23,8	111	102.2	43.4	161	148.2	62.9	211	194.2	82,4	261	240.2	102
12	11.0		62		24.2	12	103.1	43.8		149.1			195.1		62	241.2	102
13	12.0			53.0		13	104.0	44 1	63	150.0		13	196.1	_	63	242 1	102
14	12.9		64		250	14	104,9		64	151.0		14	197.0		04	243,0	
15	-	05,9	65	-	254	15	105.9		65	151.9		15	197 9		05	243.9	103
16	14 7		66		25.8	116	106.8	45 3	166	152.8	64.9		198.8		266	244.9	
17		06.6	67		26.2	17	107.7			153.7	65,2		199.7	~	67	245.8	
18	16.6		68	10	26.6	18	108.6		68	154.6	65.0	15000		85.2	68	246.7	
19		07.8	70	10.	27.0	19	109.5			155.6	66.4			85.6		247.6	
-	_			6-4		20	110.5	-	70	156.5	66.0		202.5		1 2 2	248 5	109
21	19.3	08,2	71	05.4		121	111.4		171	157.4	66.8			86.3	271	249.5	
21	1 × × ×	08.6	72	66.3	28.5	22	112,3		72	158.3	67.2		204.4			250 4	
23		09.0	73		28.9	23	113.2			159.2			205.3			251.3	
24		09 8	75	69.0		25	114.1	48,4	74 75	161.1	68.4	24	207.1		74 75	252.2	
26			76	-	-		-			162.0	_		208 0			253.1	
27	24,9	10.2	77	70.0	29.7	125	116.0			162.9	60 2		208.0			254.1	
28	25.8		78	71.6	3	28	117.8	50.0	77 78	163.8			209.9			255.0	
29	26.7		79	12.20	30 9	29		50 4	79	164.8		20	210.8		79	255.9 256.8	
30	27.6	11.7	80			30	119.7			165.7		30	211 7		0	257.7	
31	28.5		31	74.6		131	120 6	51,2	181	166 6		231	212.6		181		
32	29 5		82		32.0	32	121.5	10	82		71.1	32	213.6	-	82	258.7	
33	30.4		83	76.4		33	122.4	-	83	168.5		33	214.5			260,5	110
34	31.3	13.3	84	77-3	12 8	34	123.3		84	169,4		34	215.4		84	261.4	111
35	32.2	13.7	85	78.2	33.2	35	124.3	52.7	85	170.3		35	216.3	91.8	85	262.3	111
36	33 I	14.1	86	79,2	33.6	136	125,2	53.1	186	171.2	72.7	2 36	217.2	92.2	286	263.3	111
37		14,5	87	80.1	34.0	37	126.1	53.5	87		73.1		218.2	-	87	264 2	112
38	35.0	14 8	88	81.0	34.4	38	127.0	53.9		173,1	73.5		219.1	93.0	88	269.1	112
39		15 2	00	31.9	34.8	39	127.9	54.3		174.0	73.8		220.0		89	266.c	112
40	30.8	15.6	90		33	40	128.9			174.9		40	220.9	93.8	90	266.9	113
41	37.7	16.0	91	83.8	35.6	141	129.8	55.1	191	175.8	74.6	241	221.8	94,2	291	267.9	113
42	38,7		92	84.7	35.9	42	130,7	55.5		176 7			222.8		92	208.8	114
		16.8	93	85.0	36.3		131.6		93	177.7	75.4		223.7		93	269.7	114
		17.2			36.7	44	132.6	50.3	94	178.6	75.8		224.6		94	270.6	
45		17.6			37.1	45	133,5			179.5			225 5		95	271.5	115
46	42.3	180	96	88 4	37-5	146	134.4	57.0	196	180.4	76.6		226.4		296	272.5	115
	43.3		97	89.3	37.9	47	135,3	57.4	97	181.3	77.0	47	227.4	96.5	97	273.4	116
	44.2	18.8	98	90.2	38.3	48	136.2	57.8	98	182.3	77.4		228.3		98	274.3	
49	45.1				38.7	49	137.2	58.2	99	183.2	77,7	49	229.2	97.3	99	275.2	
-	Lep				39.1 Lat					184.1 Dep			230.1 Dep		300	276.2	_
	I lan		11 1:44	1 3 mg 93			1100								>in	Der	

24 Difference of Latitude and Departure for 24 Deg.

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Out	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Diff	Lat	Dey	Diff	Lat	Dep 1	Diff	Lat	Den
-	00,9	00 4	51	46,6	30.7	101	92,3	43.1	151	137,9	61.4	201	183.6	81.7	257		
-	01.8			47.5		02	93.2		52	138.9	61.8	02	184.5	82.2	231	229.3	102.1
	02.7			48.4		03		41 9	53	139.8			185.4		52	230.2	102.5
3	03.7		54		22.0	04				140.7			186,4	81.6	53	231.1	
4		02.0			22.4			42.3	54					83.0	54	232.C	
_5	_	_	55	_	-	05		42.7	55	141,6		-	187.3	83,4	55	232.9	103.7
6		02 4	56	51.2	22.8	106		43.1	156	142.5	63.4		188.2	83.8	256	233.9	194.1
7		02.8	57	52.1	23.2	07		43.5	57	143.4	63.9	07	189.1	84.2	57	234.8	
8		03.3	58	53.0	23.6	08	98.7	43.9	58	144-3	64.3	08	190 c	84.6	58	235.7	
9	08.2	03,7	59		24,0	09	99.6	44.3	59	145.2	64 7	09	190.0	85.0		236,6	
10	09 1	04,1	60	54.8	24.4	10	100.5	44.7	60	146.2	65.1		191.8	85.4	60	237 5	
11	10.0	04.5	61	55.7	24.8	111	101.4		161	147.1			_		261		
12		04 9	62		25.2	12	102.	1	62	148.0			192.7	85.8	62	238.4	
13		05.3			25.6			46 0		148.9	66.9		193.7	86.2	63	239-3	
		05.7	64	128	26.0			46 4	64				194.6	86 6			107.0
14		06.1	65		26.4					149.8			195.5	87.0	64	241 2	
15						15	-	46.8	65	150.7	_	-	196.4	87.4	05	242.1	107.8
16		06.5	66		26.8	116		47.2		151.6		216	197.3	87.8	266	243,0	108.2
17		06.9	67		27.2	17	106.9			1-3			198.2	88.3	67		108.6
18	16.4	07.3	68		27.7	18		48.0		153.5	68.3	18	199.1	88.7	68		100.0
19		07.7	69		28.1	19	108.7	48,4	69	154.4	68.7		200.1	89.1	69		109.4
20	.33	08.1	70	63.9	28.5	20	109.6	48.8	70	155.5		26	201.0	89,5	70		109,8
21	10.2	08,5	71	64.0	28.9	121	110	19.2	171	156.2		221	201.9		271		
22		08.9	72		19.3			49.6		157.1				89 9	100000	247.6	
23		09.4	73		29.7	23	1	50.6		158.0			202.8	90,3	72		110,6
24		09.8	74		30.1		113.						203.7	90.7	73		111,0
	1 2	10.2	75					50.8		158.9			204.6	91.1	74		111 4
25				-	-		-	-		159.9			205.5	91,5	75	251.2	111.8
26		10.6	76			126	115.		176	1	71,6		206 5	91.9	276	252.1	112.2
27		11.0			3 31.3	11 6				161.			207.4	92.3	77		112,7
28	1 2	11.4	78		3 31.7			52.1		162.6	72.4	28	208.3	92.7	78		113.1
29		11.8	79		32.1			52.5			72.8	29	209.2	93.1	79		113.5
30	27.4	12.2	80	73.	32.5	30	118.	52.9	80	164.4	73,2	30	110.1	93.5	83		113.9
31	28.3	12.6	381	74.0	32.9	131	110.	53.3	181	165.	73.6	221	211.0	-	281		
32		13.0	82		33.3			53.7	11 0	166.			211.9		82		114,3
33	1 -	13.4	83		33.8		121.		83	167.			212.8		83	257.0	114.7
34	-	13.8	84		34.2			54.5	11 0		74.8		213.8		84		115.1
35		14,2	85	77.			123.		85		75.2		1	95.2	85		115.5
			86						1		_			95.6	-	200,3	115.9
36	32 9			1	133			1000	11 0		75.6		2156	96.0	186	261.3	116.3
37		150	87	79,	35.4	37	125,		87		76.1	- 0	216.5		87	262.2	116 7
38		15.5	0.0	00.4	1 35 8	30	126.		88	1-//	76.5	38	217.4	96.8	88	263.1	117.1
		15.9	09	01.	36.2		127.0			172.	7 76 9	39	218.3		89	264 0	117.5
40	30.5	16.3	30	32.2	36.6	40		56.9		173,6	77-3	40	219.2	97.6	90	264.9	117.9
41	37.5	16.7	91	83.1	37.0	141	128.	57.3	191	174.	77.7	241	320.2	98.0	291		118.3
42		17.1	92	84.0	37-4	42	129.			175.4			221.1		92	266 -	118.8
43		17.5	93	85.0	37.8		130,6		11	176.			222.0			265.7	119.2
44		17.9	94	85.0	38.2		131.			177.2	78.0	44	222,9				119.2
45		18.2	95		38.6		1 32.	59,0	95		79 3		223.8	99.6	95	260.0	119.6
46	-	18.7		-	39.0												120.0
			90	88 6	39.0	4.7	133,4	39.4	196	179.0	79.7			100.0	1296	2704	120.4
47		19.1			39.4	1 47	134.3	59.8	97	180.0	80.1		225.6	100.5	97	271.3	120.8
		19.5			39,9	48	135,2	60.2	98	180.9	80,5		226.5	100.9			121.2
		19.9			40.3		136.1			181.8				101.3	99		121.6
FO	45.7	20,3	100	-						182.7	81.3	250	228.4	101.7	300		122.0
_							- 1000						1	-		Water to the same of	Name of the last
_	L'er	[3.	Dift	Drp	Lat	D.H	Dep	Lat	Diff	Dep.	Lat	Dift	Dep	Lai	Diff	Ther	Lat

D:4:	I at I	Denli	Dif	Lat	Deni	Dift	Lat	Depl	Dift	Lat	Deil	Diff	Lat	Dep 1	Dift	, Lat	Dep
Din										136.9		201	182.2	84.9	251	227.5	-
1	00,9				21.6	101		42.7	151 52	137,8	64.2		183.1	85.4			106.5
2	01.8	1000000	-		22.4	01		43.1		138.7			184.0	85.8			106.9
3		01,3	53		22.8	04		44.0		139.6			184.9	86.2			107.3
4	04.5	01.7	55		23.2	05		44.4	55	140.5		05	185.8	86.6	55	D 70 m	107.8
_5			56		23.7	106	96.1		156	141,4		206	186,7	87.1	256	2 22.0	108,2
6		02.5			24,1	07	100	45.2		142.3			187.6	87.5			108.6
7		03.0	58		24.5	08		45.6	58	143.2	66.8	08	188.5	87.9	58		109.0
		03,8	59		24.9	09		46.1	59	144.1		09	189.4	88.3	59		109.5
9	1000	04,2	60		25.4	10		46.5	60	145.0	67.6	10	190 3	88.7	60	235.6	109.9
-		04.6	61		25.8	111		46.9	161	145.9	68.c	211	191.2	89,2	261	236,	110.3
11		05.0	62		26.2	12		47.3	62		68.5	12	192.1	89.6	62	237.5	110,7
13		05.5	63		26.6	13		47.8	63	147.7	68.9	13	193.0	90.0			111,1
14	12.7	1050	64	58.0	27.0	14		48.2	64	148.6			193.9		64		111.6
15	13.6	06.3	65	58.0	27.5			48,6	65	149.5	69 7	15	194.9	90.9	05	240.2	112.0
16	14-1	06.8	66	59.8	8 27.9	116	105.	149.0	166	150.4	70.2	216	195.8	91.3	266		112.4
17		07.2	67	60.	7 28.3			19.4	67	151.4			196.7	91,7	67	242,0	112,8
18		07.6	68	61.	6 28.7	18	106.	9 49.9	68	152.	71.0		197.6		68	242.0	113.3
19	17	08,0	69	62.	5 29.2	19		8 50.3	69	153.2			198.5	92.5	69	1	113.7
20	18.	08.5	70	63.	4 29.6	20	108.	8 50.7	70	154.1	71,8	20	199.4	93.0	70	244.7	114.1
21	19.0	08.9	71	64.	3 30.0	121	109.	7 51 1	171	155.0	72.3	221	200.3		271		114,5
22		9 09.3	72	65.	3 30.4	22		6 51,6				22	201.2	100	72	240.	114.9
23		8 09.7	73	66.	2 30.1	23	111.	5 52.0				11 -:	202.1		73		1154
24	21.	8 10.1	74					4 52.4	74		7 73.5		203.0		74	248.	
25	22.	7 10.6	-	-	0 31.	25	113.	3 52.8			74.0		203.9		75		-
26	23.	6 11.0					114	2 53.2		1	74.4		204.8		276		1166
27		5 11.4			8 32.		1 3	1 53.7	-0		4 74.8		205.7	1	77		117.1
28	25.	4 11.8					-	0 54.1	11		3 75.2		206 6	1	78		117.5
29		-	11 0		6 33.			9 54.5			75.6		207.5		79		117.9
30	-	2 12.7			5 33.			8 54.9		-	-			-	-		a more of
31		1 13.1		100		41		7 55-4			76.		209.4		82		8.811
32		0 13			3 34			6 55.8		104	9 76.9		210.3		83	1-22	5119.6
33		9 13 9			2 35.	11 4	2	4 56.6			9 77.3 8 77,8		4 212		84		
34		8 14-4			100				11 0.						8		3 120.4
3.		_	-11-		0 35.			-	-	-	-	-	6 213.9		286		
3		6 15		10.0	.9 36. .8 36.			3 57-	1 0		5 79.0				87	1-03	1 121.3
3		5 15.	11		8 37.			.2 57.6 ,1 58.	88	170.	4 79	1 3	01	100.6			0 121.7
3		4 16.	- 1 2	9 80	7 37	6 30	126	.0 58.	8	171.	3 79.	3		6 101.0	89		G 122.1
	0 36	3 16.	9	0 81	.6 38.	0 40	126	9 59,			2 80.			5 101.4			8 122.6
4	-	- 12			.5 38,			.8 59.		173,		-		4 101.8	1	_	7 123.C
4	2 28	1 17.	7 0	2 82	.4 38.	0 4		7 60.0	91	174.	0 81.			3 102.3		264	6 123 4
14		.0 18.	2 0	3 84	.3 30	3 4	129	6 50.	4 9	174.	9 81.	6 4		3 102 7			5 123.8
4	4 30	.9 18.	6 9	4 85	.2 39.	7 4	1 130	,5 60.	9 94	1 175	8 82.	0 4	4 221.	1 103.1	94	4 266.	5 124,2
4	5 40	.8 19.	0 9	5 86	.1 40.	1 4	5 131	.461.	3 9		7 82.	4 4	5 222.	0 103,			4 124.7
4	_	.7 19.	-	6 87	.0 40.	6 14	6 132	.3 61.	7 196	177.	6 82.	8 24	6 222,	9 104.0			3 125.1
		6 19		7 87	9 41	0 4	7 133	,2 62.	1 9	7 178	5 83.	3 4	7 223.	9 104.4	1 9	7 269	.2 125,
4		.5 20,		8 88	8 41.	4 4	8 134	.1 62.	5 9	8 179.	4 83.	7 4	8 224.	3 164 8	3 9	8 270	.1 125.9
4	9 44	4 20,	7 9	9 89	7 41.	8 4	9 135	,0 63.	0 9	9 180	4 84.	1 4	9 225	7 105	1 9		.0 126.4
		-1	11-0	0100	6140	-11 7 50	01125	963	4 20	0 181	2 84.	51125	0 220	6 104.	7 10	0 271	.9 126
5	0 45	3 21.			_	-		p La	-	f Der			_	P Lat			La

), Aı	Lat I	Depl	Dift	Lat	Depl	Dift	Lat	Depl	Dift	Lat	Deil	Dia	Lat	Dep 1	1Diff	Lat	Den
-	00,9	-	51	1	22.4	101		44-3	151	135.7	66.2		180.7	88.1	251	225.6	
-	01.8		52		22.8	02		44.7	52	136.6			181.6	88.6	52	226.0	
1		01,3	53		23.2	03		45.2	53	137,5	67.1	03	182.5	89.0	53	227.4	
4	03.6	01.8	54	48.5	23.7	04	2 200	45.6	54	138.4	67.5		183.4	89,4	54	228.3	
5	04.5	02.2	55	49,4	24,1	05	94-4	46.0	55	139.3	68.0	05	184.3	89 9	55	229.2	111
6	05.4	02.6	56	50.3	24.6	106	95-3	46.5	156	140.2			185.2	90,3	256	230.1	112.5
7		03.1	57		25.0	07		46.9	57	141,1			186,1	90.7	57	231.0	112,
8.	07.2	03.5	58	52.1	25.4	08		47.3	58	142.0			187.c	91.2	58	231.9	
9		03,9	59		25.9			47.8	59		69.7		187.8	91,6	59	232.8	
10	09 0	04,4	60	333	26.3			48.2	60	143.8	70.1	-	188.7	92.1	60	233.7	114.0
11	09 9	04.8		13.	26.7			48,7	161	144-7		211			261		114,
12		05.3	4		27.2			49.1	62		71.0		190.5	92.9	62	235.5	
13		05.7			27.6		the second	6 49.5	63		71.5		191.4	93.4	63	236,4	
14	12.	06.1			28.			5 50.0			71,9		192.3	93.8	65	237.3	
15	-	06.6	-11-	-			103.		65		72.3	15				238.2	_
16	100.00				3 28.9			3 50.9			72.8		194.1		67	239.1	
17		3 07.			2 19.			2 51.3		1 3	73,2		195.0		68	1	117.
18		07.9		The second second	1 29.			1 51,7	11 0	1-3	73.7		195.9		110	241.8	117.
19		08,	411		9 30.			9 52.2	11 -	-	74.1	20		96.4	70		118.
20	-	-	-				-	-		-	-	11-	0.6		-	-	-
21		9 09.				1 121		133			775.0		1		271		118.
22		8 09.			7 31.			7 53.5			6 75.4		200.4		72	244.	
23		7 10.	11 -		6 32.			6 53.9			5 75.8 4 76.3		201.				119.
24	- 100	6 10.	- 11		5 32.			5 54-4	74		3 76.7		202.2				120.
25		5 11.0	-11-									-	_	_			
26		15-1				-11					2 77.2		203.1				121.
27		-			2 33.	-11 -6		o 56.			77,6			99.5	11 -0		121.
28		2 12.			13.	-							1	100.4	11.		122.
25		1 12.	11 0		9 35.		4 100				8 78.		1	100.8	11 6	-	122
30		0 13.	-11-						-11-		_			101.1		-	-
31		9 13.		1 72,				.7 57·4			7 79 4			101.7			123
3	5 -	8 14.	110	3 74	7 35.					164	5 80.2				110-		124
3		7 14,	-		5 36.						10-	3		102.6			3 124
3		5 15	110	5 76							3 81,	3		103.0			2 124
		_	-	-		7 13		.2 59.	-		2 81.			103,5	1	-	1 125
3	32.	4 15.			2 38.			1 60.			1 82.0	411		103.9		258.	
3	33	2 16.						0 60.		169,				104.		258.	
3	34	1 17.			0 39.			.9 60.	8	169.	9 82.	39		104.	89	259.	8 126
		0 17.		80	9.39	d 40		,8 61.	9		8 83.	4	215.	7 105.2	90		
4	136	9 18.						761.			7 83.7			6 105.7			-
4	30.	7 18.	4	2 82	7 40.	3 4		6 62.	9	172.	6 84.1	45		106.1			4 128
4	1 28	6 18.			6 40.		128	5 62.	7 9:	173,	5 84.0	4:	218.	106.	93	263.	3 128
4	1 20.	5 19	3 6		5 41.		129	4 63.	9	1174.	4105.0	1 44		107.		264.	
4		4 19.			4 41.		130	3 63.	6 9	175.	3 85,5	4		107.4		265.	1 129
40		3 20,	-		3 42.			2 64.			2 85.9	246	-	1 107.8		266.	
47		2 20,	6 9	7 87.	2 42.	5 47	132	1 64.	و ال	177.				108.		266.	
45		1 21.	ا ا	8 88.	1 43.	48	133	0 64.	91 98	178.	0 86.8	41	T22,	9 108.7	98	267.	8 130
49		0 21.		9 89.	0 43.	49	133	9 65.		178.	9 87.2	45	223.	8 109.	99	268.	7 131
50		9 21.		89.	9 43.	8 150	134	8 65.	200	179.	8 87.7	250		7 109.	300	269.	6 131
		Lat			PLat					Dep			Da	Lat		De	

for 64 Deg.

Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	De	Dift		-	Ditt	Lat	Dep	Dift	Lat	De
1	00.9	00.5	51	45-4	23.2	101	90.0	45.9	151	134.5	68.6	301	179.1	91.3	251	223.6	114.
	01.8	00.9	52	46.3	23.6	02	90.9	46.3	52	135.4	69.0		180.0	91.7	52	224.5	114.
3	32.7	01.4	53	47.2	24.1	03	91.8	46.8	53	136.3	69.5	03	180,9	92.2		225.4	
4	036	8,10	54	48.1	24 5	04		47.2	54	137.2	69.9	04	181.8	92.6		226.3	
5	04.5	02.3	55	49.0	25.0	05	93.6	47.7	55	138 1	70.4	05	182.7	93.1	55	227.2	115.
6	05.3	02.7	56	49.9	25.4	106	94.4	48.1	156	139.0	70.8	206	183 5	93.5	256	228.1	116.
7		03.2	57	50.8		07	95.3	48.6		139.9		07	184.4	94.0		229.0	100000000000000000000000000000000000000
8		03.6		51.7		08	96.2		58	140.8	71.7		185.3	94.4		229.9	
9	e8.o			52.6		00	97.1			141.7			186.2	94.9		230.8	
ó	08.9		60	53.5		10		49,9		142.6		10	187.1	95,3		231.7	
1	09.8		61	54.4		111		50.4	161	143.5	72.1	211	188.0	95.8		232.6	_
201			1 1 mm 1 mm	55,2		12		50.8		144.3			188.0	96.2		233.4	
2		05.4		56.1		1.00		12.18		145.2	100		189 8	96.7			
3		95,9	64	-		13	100.7			146,1		1	190.7	97.2		234.3	
4		06.4	65	57.0		14	1.4.			147.0			191.6	97.6		235 2	
5		06.8		57-9		15	102.5						_			236.1	
6		07.3	66	58.8	30.0	116	103.4		166	147-9	75 4		192.5	98.1	200	237.0	120:
7		07.7		59.7		17	104.2			148.8		17	-23.3	98.5	07	237.9	[21.
8		08.2		60.6		18	105.1			149.7			194.2	99.0		238.8	
9		08.6		61.5		19	106.0			150.6			195.1	99-4		239.7	
0	17.8	09.1	70	62.4	31.8	20	106.9	54.5	70	151.5	77.2	20	196.0	99.9	70	240.6	122,
1	18.7	09.5	71	63.3	32.2	121	107,8	54.9	171		77.6	221	196.9	100.3	271	241.5	123.
2		10.0		64.2	F 10	22	108.7		72	153.3	78.1	22	197.8	100.8		242.4	
3		10.4		65.0			109.6		73	154.1	78.5	The state of the s	198.7			243.2	
4		10.9		10	33.6	24	110.5		74	155.0	79.0	24	199.6			244.1	
5		11.4	75		34.1	25	111.4		75		79.5	25	200.5	102.2		245.C	
-	_						_			156.8		226	201.4	102 6			-
0.5	- TO A	11.8			34.5	27	112.3			157.7			202.3		77	245.9 246.8	125.
17		12,3	78			28	114 0			158.6	1			103.5		247.7	
. 33		12.7			35.4	29	114.9	68 6		159.5	0	1	1	104.0		248.6	
9		13.2	79 80		35.9 36.3	30	115.8	50.0		160.4			204.9				
30	20.7	13.6	-	1												249.5	
31		14.1	81	72.2		131	116.7		181	161.3			205.8		281	250.4	127.
32	28.5	14.5	82		37.2		117.6			162.2	82.6		200.7			251.5	
33	29.4	15.c			37.7	33	118.5			163.1	83.1			105,8		252.2	
34	30.3	15.4			38,1	34	119 4		84	163.9		12		106.2		253 C	
35	31.2	15.9	85	75.7	38.6	35	120.3	01,3	85	164.8	04.0	35	209.4	106.7	85	253.5	129
36	32.1	16.3	86	76.6	39.0	136	111.2	61.7	186	165 7	84.4	236	210.3	107.1	286	254.8	129
37	33.0	16.8			39.5	37	122.1	62.2	87	166.6	84 9	37	211 2	107.6		255.7	
		17.3			40.0		123.0		88	167 5	85.4	38	212.1	108.1	88	256.6	130
39	34.7	17.7	89	79.3	40.4	39	123.8	63.1	1 89	168.4	85.8	39	212.9	108.5	89	257.5	131
10	35,6	18.2	90	80.2	40.9	40	124.7	63.6	90	169.	\$6.3	40	213.8	109.0		258.4	131
41	26	18.6	91		41.3	141	125.6				86.7			109.4		259.	-
12	37	19.1	1 3	82.0	41.8	42	126,5	64.5	02	171.1	87.2	42		109,9		260.	1 3 2
+3		19.5			42.2		127.4	64.0	02	172.0	87.6	1 42		110.3		261.	
†3 44		20 0			42.7	II AA	128.3	65.4	04	172.9	88.1	1		110.8		262.	133
		20.4	05	84.6	43.1	II AG	129.2	65.8	95	173.7	88.5	45	218	111,2	00	262	8 122
45										73.7	80.0	1 3				262.	-1-33
46	41.0	20.9			43.6	1140	130.1	00.3	196	174.	180.0	240		111.7	290	263.	7 134
47		21,3			44.0	47	131.0	60.7	97	175.	189.4	47		112.1	97	264.	134
48		21.8		87.	44 5	1 48	131.9	07.2	11 98	170.4	1 09.9	40		112.6	98	265.	5 135
49		22.2		88.	44.9	49	132.1	07.6	99	177.	90,3	49		113,0	99	266	4 139
50					45.4		133 7			178.				8 113		267.	
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3		01,9	53	1.7	25.4	04	91.8	48.8		136.0		04	180.1	95.8		224.	
5	_121	02.3	55		25.8	05	*	49.3	55	136.9		05	181,0	96.2		225.2	
6	-	02.8	56	_	26.3	106		49.8		137.7		206	181.9	96.7		226.0	
7		03.3	57		26.8	07		50.2		138 6		07	182 8	97.2		226.9	
8		03.8	58		27.2	08		50.7		139.5		08	183.7	97.7		227.8	
9		04.3	59	52.1	27.7	09		51.2	59	140.4		09	184.5	98.1		228.7	
10	●8.8	04.7	60	53.0	28.2	10	97.1	51.6	60	141.3	75.1	10	185 4	98.6	60	229.6	122.
11	09.7	05.2	61	53.9	28.6	111	98.0	52.1	161	142.2	75 6	211	186.3	99.1	261	230.5	122,
12	10,6	05,6	62	54-7	29.1	12	98.9	52.6		143.0	76.1	12	187.2		62	231.3	123.
13		06.1	63	55,6	29.6	13		53.1		143.9				100.0		232.2	
14		06.6	11 0		30.0	14		53.5		144.8				100 5		233.1	
15	13,2	07.0	65	-	30.5	15	101.	54.0	05		77.5			100.9		234 0	
16		07.5			31.0	116	102.4	54.5	1166		77.9	216		101 4	266	234.9	124.
17	150	08.0			31.5	17		54.9		147.				101 9		235.	
18		08.5	68		31.9	18		55.4			78.9			102.4		236.	
19	1000	08.9			32.4	19	105.1			149.				102.8	1 70	237.	120.
-		09.4		-	-	11-	106.0	-			_				-		
21	115.00	09.9	11		33.3	121		56.8	171	151.	80.3	221		103.8		239.	
22		10.3		1 -	33.8			57.3	72	151.	8 8 7 7			104.2		240.	
23		10.8			34.3		108.	5 58.2	73	153.	6 8	1 2		105.2		241.	
24		111.7			3 34.7		110.	4 58.7	7	154.	5 82.2	2		105,6		242.	
	-	-			-						4 82.6			106.1			-
26		12,2			35.7		111.		176	156.	282.	2		106.6		243.	
27		13.1			36.6			60.1	78	157	2 83.	21		107.0		245	
29		6 13.6			8 37.1			60.6			1 84.0			107.5		246.	
30			11 0.	70.	6 37.6	30					9 84.			108.0		247.	
31	27.		10		5 38,0		115.	61.	181	150.	8 85.0	23	204.0	108.			1 131
32		15.0	11 0		4 38.5	32		6 62.0			7 85.			108.		249.	
33			11 0	,	3 39.0			4 62,4	83	161.	6 85.	3		109.4	8	249.	9 132
34		16.0			2 39.4		118.	3 62.9	84	162.	5 86.	4 3		6 109,9	8.	4 250.	8 133
35		9 16.4	8	75.	1 39.9	35	119	2 63.4	8	163.	4 86.	9 3	207.	5 110.	8	5 251.	7 133
36	31.	8 16.	8	6 75.	9 40.4	136	120.	1 63.9	186	164.	2 87.	3 23	6 208.	4 110.	28	6 252.	5 134
37		7 17.4	8	7 76.	8 40.8	37	121.			165.				3 111,	3 8	7 253	4 134
38	33.	6 17.8	8	77.	7 41.3	38	121.	9 64.1		166.	0 88.	3 3		2 111.7		8 254.	
39	34.	5 18.	8		6 41.8		122.	7 65.	1 89	166.	9 88.	7 3		0 112.		9 255.	
40	35,	3 18.5	9	79.	5 42.5	11		665.		167				9 112.	- 1	256.	
41	36.	2 19.2	9		4 42.7	141	124.	5 66.	1 191	168.	7 89.	7 24		8 113,		1 257.	0 136
42		1 19.	7 9	2 81.	2 43.2	42	125.	4,00.	1 92	109.	5 90,	4		7 113.		2 257	
43		0 20.			1 43.7	43	126,	3 67.	9:		4 90.			6 114.		3 2 58	
44		9 20.			0 44		127.	68.		171.	2 91.			3 115.		1 259	
45		7 21,			9 44 6							_				5 260.	3 - 30
46		6 21.			8 45.1		128.	68.	1196	173				2 115.	5 29	6 261	4 139
47	41.	5 22.			7 45.		129.	-160	97	174	8 02			1 115.		7 262	
48		4 22.	4 1 1000		5 46.0	1 40	130.	6.70		174	7 93.4			9 116.	9	8 263 9 264	
50		3 23.0	11.9	88	3 47.0	150	122	5 70.4	99	176.	6 02	25	220	8 117.	4 20	0 26.4	
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1	00.9	00.5		44.6		101	88.3			132.1			175.8		251	219.5	
2		01.0		45.5		02	89.2			132.9			176.7		52	220,4	
3		01.5		46.4		03	90.1			133.8			177.5	98.4	53	221.3	
4	03.5	01.9	54	47.2	20.2	04	91.0		54	134.7	1 1 1 1 1 1 1 1	04	178.4	98.9	54	222,2	
5	04.4	02.4		48.1		05	91.8	50.9	55	135.6		05	179.3	99.4	55	213.0	
6	05.2		_	49.0		106	92.7			1364			188,2	99,9		223,9	
7	200 W	03.4		49,9		97	93.6		57	137,3	70.1	07	181.0		57	224.8	
8	07.0	March 4		50,7		08	94.5		-	138.2		08	181.9			225.6	
9	07.9		60	51.6		10	95.3		59 60	139.1		10	182.8	2		226.5	
10	08.7	-	_		-		96.2			139.9		-	_				_
11	09.6		61	53.4		111	97.1			140.8		211	184.5	102.3		228.3	
12		05.8		54.2		12	98.0			141.7		12	185,4 186.3	102.8		229.1	
13	11.4	o 6 ,8		55.1		13	98.8		64	342,6 143.4		13	187.2			230,0 230.9	-
14		07.3		56.8		15	100.6		65	144.3		15	188.0		65	231.8	
15						_			166			216	188.9			_	_
61	14.0	07.8		57·7 58.6		12	101.5	56.2		145.2		17	189.8	105.7		232.6	4
17	14.9	08.7		59,5		-0	103.2			146,9		18	190 7		68	233.5 234.4	
19		09.2		60.3			104.1			147.8		10	191.5			235.3	
20	7 1 2	09.7		61.2			105.0			148.7		20	192.4			236,1	
_	.8.	10.2		62.1		121	105.8		171	149.6		221	193.3	107.1	-	237.0	_
21	10.2	10.7		63.0			106.7			150.4		12000	194.2		100	237.9	
23		11,2		63.8			107.6			151.3		23				238.8	
24	27	11.6		64,7			108.5			152.2		24	195.9			239.6	270
25	21.9	12.1		65.6			109 3		75	153.1	84.8	25	196,8	109.1	75	240.5	
26	22.7	12.6	76	66,5	36.8	126	110.2	61.1	176	153.9		226	197.7	100.6	276	241.4	
27		13.1	7	67.3		27	111.1	61.6	77	154.8	85.8		198.5			242,3	
28	24.5	13.6	78	68,2		28	111.9		78	155.7	86.3	28	199 4		78	243.1	134.
29	25.4	14,1	79	69.1	38.3	29	112.8			156.6		29	200.3		79	244.0	
30	26.2	14.5	80	70.0	38.8	30	113.7			157.4		30	201.2	111.5	80	244.9	
31		15.0	81		39.3	131	114.6		181	158.3		231	202.0	112.0	281	245.8	
32		15.5			39.8	32	115.4		82	159.2	88.2	32		112.5	82	246,6	
33		16.0				33	116.3			160.1		33	203.8		83	247.5	
34				1.3.3	40.7	34		65.0	84	160.9	-	34	204.7		84	248.4	
35	30.0	17.0	85	74.3		35	118.1		-	161,8	-	35	205.5			249.3	_
36	31,5		80	75.2			118.9		186	162.7		236	206,4		286	250.1	138
37	32.4	17.9	89	70.1	42.2		119.8			163.6				114.9	188	251.0	139
38 39	33.2	18.9	80	77.0	42.7	30	120,7		80	164.4	01.6	1 30		115.9	80	251.9 252.8	139
		19.4			+3 6		122.4		90	166.2	92.1	40		116.4	90	253,6	140
40 41					14.1		123.3			167.0				116.8			
42	35.9	19.9	01		44.6	42	124.2	68.8	92	167.9				117.3		254.5	
43	37.6	20.8	9		45,1	43		69.3	93	168.8				117.8	93	256.3	142
44	38.	21.3	94		45.6		125.9	69.8	94	169.	94.1	44		118.3		257,1	142
45	39.4	21.8	9		46,1		126.8	70.3	95		94.5			118.8	95	258,0	143
46		22.3			46.							246		119.3		258.	
47		22.8			8 47.0	47	128.	71.3		172.				119.7	97	259.8	144
48	42.0	23.	9	8 85.	7 47-5		129.4			173.		48	216,	120.2	98	260.6	144
49	42.9	23.	9	9 86.	6 48.0	49	130.	72.2	99	174.	0 96.5	49	217.	120.7	99	261.	145
50	43.7	24.2	10	87.	5 48.	150	131.	72.7	200	174.		250	218.	7 121.2	300		1 145
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	-		72.	-11			6 27.	4 5 00			52 0	11 -			77.0	11		7 10	- 11	54.	220,	0 127
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	7	06.1	03	- 11 *			1 28.				53.0				78 0			4 10		156	221.	
1			04.				29				53.5				78.5			3 103		57		128.
1			04.	5			199.		100		54.5				79.0	11		0 104		58		129
1	0	38.7	05.		60	52.0	30.	0 10			55.0				80.0			9 105		59	224.	
1	1	9.5	05.	5	61	52.8	30.	111		_	55.5	16:	1 139	3	80.5	211			_	61		130
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Н	_		06,	~ III - 2	304 B	54.6		5 13				6			81,5		184.			63	227.8	1 3
	_ 1.		07.0				32.0				57,0	64	4 100 100		82.0		185,	3 107	.0	64		1 32.
_	-	-	07.	-11			32.	15		-	<u>57-5</u>	6	142,	9	82.5	15	186	107	.5	65		132.
17		_	08.0			57.2	33.	116	1			166	1 TO 1		83.0	216	187.	1 108	.0 2	66	230 4	133
118			08.		7	8.6	33.	17				67			83.5	17	187.			67	231.2	133.
119			09.5			9,8			103			68			84.0		288.	109	.0	68		134.
20			10.0		- 13	0.6						70			84.5	19	189		-11	69	233.0	134
81		8,2	10.9	7	16	1.5	33	_	104.	-	_		-			-		1-	-11-		233.8	135.
22			11,0				35.0		105.			72	149.		85.5 86.0	221	191 4	110	-11			135
23			11.5		3 6	3.2	36.	23	1 2			73			86.5	23	193.1		- 11			1 36.0
24			12.0	7	4 6	4,1	37.0		107	46	2.0	74			87.0	24	194.0		-11			136.
25	-	1.7	12.5		_	5.0	37-5	25	108.	3 6	2.5	75	151	6	87.5	25	194.9		11 .		238.2	
26	3 3		13.0		66	5.8	38.0		109			176	152.	4	88.0	226	195.7	112	_ _	- 1		138.0
27	9 10		13.5				38.9	27	110.			77	153.		88.5	27	196,6	113.	- 11			138.
29	-	7.2	14,0			7.5	39.0	28	110				154.		89.0	28	197.4					139.0
30		6.0	15.0	8	06	0.1	39.5	30	111.				155.0		89.5	29	198.3			79		139.
31			15.5				40.5			77		80	33	-	90.0	30	199 2		-11-	0	142,5	140.0
32			16.0		2/2	1.0	40.5	131	114.	14	2 3	181	156.		90.5		200.0		-		243-3	140.5
33	2	8.6	16.5	8		1.9	41.5	33		-1-	6.5	83			91.0		200.9 201.8				244.2	141 0
34	2		17.0	8.		2.7	42.0	34			7,0	84	159.	4	92.0		202.6			100		141.5
35		0.3	17.5	8	5 7	3.6	42.5	35	116.		7.5	85	160.		92.5		203.5				46.8	142.0
36			18.0	8		4.5	43.0	136	117.	6	8.0	186	161.1		93.0		204.4			- 1-	47.7	-42.5
37	3	2.0	18.5	8	717	5.3	42.5	37	E18.6			87	161,9		93-5	37	205.2	118.	5 8			143.5
39	3	2.9	19.0	8	17	0.2	44.0	38	119.			88	162.8	19	94 0	38	200,1	119.	o 8	8 2	49 4	144.0
		1.6	19.5	00	7	7.1	44.5	39	120,4			89	163 7		94.5	39	207.0	119.	5 8	9 2	50.3	144,5
40	2	_			1		45,0	40	121.2	-			164.5		95.0		207.8		9	0 2	51.1	145.0
		5.4	10.5	91	7	0.0	45.5	141	122.1			191	165 4	9	5.5	241	203.7	120.		1 2	52.0	145,5
	37	7.2	11.5	9	8	9.7	46,0		123.8	7	.0	92	166.3				209 6		1 9	2 2	52.9	146.0
44	38	1.1	12.0	94	8	1.4	47.9	44	124.7			93	168.0		6.5		210.4	121.		3 2	53,7	146.5
45	39	0.0	2 5		8:	2,3	47.5	45	125.6	72	2.5	95	168:9	13	7.5		211.3			4 2	54.6	147.0
45		,8 2		96			18.0		126 4				169 7				1130		-		55.5	
		.72		97	84	10	48.5	47	127.3	1	3.5	97	170.6	1 3	8.5	47	113.9	123.0	129	2	56.3	480
48	41	. 5 2	4.0	98	84	19	10,0	48	128.2	74	1.0	98	171.5	10	9.0	48	14.8	124.0	0	3 12	57,2	140.5
49	42	4 2	4.5	99	8	5.7	19.5	49	120 C	74	145	00	172.2	0	0.5	40 3	115.6		11 0	9 2	58.9	140:5
50	43	.3 2	5.0	100	86	2.6	50.0	150	129.9	75	5.0	200	173.2	10	0.0	250	16.5	125.0	300	0 2	59.8	150.0
Dif	De	ep L	at	Diff	D	ep	Lar	Ditt	Dep	L	at	Dift	Der				Dep			alr	Den	Lat
A	1		Si.		4.		120					-		-		There is			11	-	-11	

) ft	Lat	Dep	D	ift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat.	Dep	Dift	Lat	Dep
-	00.0	00,5	15	1	43.7	26.3	101	86.6	52.0	151	129.4	77.8	201	172.3	103 5	251	215.1	129.3
2	01.7			_	44.6	26.8	02	87.4	52.5	52	130.3	78.3	02	173,1	104,0	52	216.0	129.8
2	02.6	1		3	45.4	27.3	03	88 3	53.0	53	131.1	78.8	03	174.0	104.5	53	216.8	130.3
4	03.4	02.1	1 5	4	46.3	27.8	04		53.6		132.0		04		105.1	34	217.7	130.8
5	04.	02:0	1 5	55	47.1	28.3	05	90.0	54.1	55	132.8	79.8	05	175.7	105.6	55	218.5	131.3
6	05.1	03.	11 5	56	48.0	28.8	106	90.8	54.6	156	133.7	80.3	206	176.5	106.1	256	219.4	131.8
7	3	03.	-11	-	48,8	29.4	07		55.1		134.5		07	177.4	106.6	57	220.2	132.4
8	06.	04.	1 5	58	49,7	29.9	08	92.6			135.4		08	178.3	107.1	58	221.1	1 32.9
9.	07.	041	6 5	59	50.6	30 4	09	93.4			136.3	81.9	09		107.6		222.0	
10	08	05.	2 9	50	51.4	30.9	10	94 3	56.7		137.1	82.4	10	180.0	108,2	60	222.8	133.9
11	09.	05.	7116	61	52.3	31.4	111	95.1	57.2	161	138.0		211	180 8	108.7	261	223.7	134.4
12		06.		62		31 9	12	96.0	57.7		138.8	83.4	12	181.7	109.2	62	224.5	134 9
11	10.2	06:	اار	63	54 0	32.4	13	96.8	58.2		139.7	83.9	13	182.5	109.7	63	225.4	135.4
14	12.	07.	2 (64	54.8	3300	14		58.7	04	140.5		14		110.2	64	226.2	136.0
15	12	9 07	711	65	55,7	33.5	15	98.6	59.2	•5	141.4		15	184.3	110.7	05	227.1	136.
16	13.	708.	2	66	56.6	34.0	116	99-4	59.7		142.3		216	185.1	111:2	266	228.0	137.0
17	14.		8	67	57.4	34,5	17	100.3	60.3	67	143.1	86.0	17		111.8		228.8	137.5
18	15.	4 09,	3 (68	58.3	35.0	18	101:1		68	144.0	86.5	18	186.8	112.3	-68	229.7	138.0
19	16.	3 09.	8 (69	59.1	35.5	19	102.0		69	144.8		19		112.8	69	230.5	138.5
20	17.	1 10,	311	70	60.0	36.1	20	102,8	61.8	70	145,7	87.6	20	188.5	113.3	70	231.4	139.1
21	18.	0 10.	8	71	60.8	36,6	121	103.7	62.3	171	146.5	88,1	221	189.4	113.8	271	232.2	139.
22		9 11.	- 11	•	61.7	100 100 100	22	104.6		72	147.4	00 6	22	190.3	114.3			140.
23			211	73	62.6	37.6	23	105.4	63.3	73	148.3	89 1	23	191.1			234.0	
24		6 12.	.11	74	63.4	38.1	24	106.	63.9	74	149.1	89.6	24		115.4		234.8	141.1
25	21.	4 121	9	75	64.	38.6	25	107.1	64,4	75	150.0	90.1	25	192.8	115.9	75	235.7	141.6
26	22.	3 13.		76	65.1	39.1	126	108.0	64.9	176	150.8	90.6	226	193-7	116.4	176	236,9	142.
27	23.		111	77	66.0	39.7	27	108.8	65.4	77	151,7		27	194.	116.9	77	237.4	144.
28		0 14	- 14	78	66.	8 40.1	28	109.7	65.9	78	152.	91.7	28	1954	117.4	78	238.2	143,
29	24.	9 14,	9	79	67.	7 40.	29	110.6	66.4	79	153.4		29	196.	117.9	79	239.1	143.
30	25.	7 15	5	80	68,	6 43.2	30	111.4	67.0	80	154-	92.7	30	197.1	1118.5	80	240.0	144.
31	26.	6 16		81	60.	4 41.	131	112.	67.5	181	155,	93.2	231	198.0	119.0	181	240.8	144.
32	1 1000	1-0	- 11	82	70.	3 42.	32		100 .		156		32	198.	119.	82	241.7	
33	1 2	3 17	.cll	83	71.	1 42.	33	114.0	68,	83	1156.	94.2	33	199.	120.0	83	242.	145.
34		1 17	5	84	72,0	043	34	114.	69,0		1	94.8	34	200.	120.		243.4	16
35		0 18	ol	85	72.	8 43.	35	115.	69.	85	158.	95 3	35	201.	121.0	185	244.2	146,
36		0 18	.5	86	73.	7 44.	3 136	116.	79 0	186	159.	4 95.8	236	202.	3 121.	186	245.1	147.
37			III.	87	74	6 44	37		170.	87	160.			203.	1 122.	87	246	
38	122	6 10	6	88	75.	4 45.	3 38	1118.	71.1	88	161.	1 96.8	38	204.	122.	88	246:	148.
39	33	4 20	IIr.	80	176.	2 45.	8 20	IIIO	171.6	N 80	152.	0 97.3	1 20	204.	8 123.	1 89	247.	148,
40	34	3 20	.6	90	77	1 46.	4 40	120	72.1	90	162.	8 97.9	40	205.	7 123.	6 90	248.	149.
41	25	1 21		91	78.	0 46.	9 141	120.	8 72.	191	163.	7 98.4	241	206.	5 124.	1 291	240.	149
42	126	0 31	.6	92	78.	8 47	4 42	121.	7 33	92	164.	5 98.9	42	207.	4 124.	6 92	2 50:	2 150.
4:	26	9 22	. 2	93	79.	7 47,	9 43	122.	6 73.	9	165.	4 99.4	4:	208.	3 125.	1 93	251:	1 150.
44		7 22	.6	94	80.	6 48,	4 44	123.	4 74-	1 94	166.	3 99,9	44	209.	1 125.	6 94	252	0 151
		6 23		95	81.	4 48.	9 4	124.	3 74	7 9	; 167.	1 100.4	4	210	0 126.	2 9	252	8 151
45	20	4 23	-11	06	82	3 40.	4 14	125.	175.	2 19	168.	0 100.	24	210	8 126.	7 20	252	7 1 12
41		3 24		97	82.	1 50.	0 4	126.	0 75.	7 0	168.	\$ 101.	5 4	7 211.	7 127.	2 0	254	5 152
4	41	1 24	,7	-08	84	0 50.	5 4	126.	8 76.	2 0	160	7 102.	0 4	8 212	5 127.	7 0	255	4 153
4		0 25	.2	99	84	8 51.	0 4	127.	7 76.	7 9	170	.5 102.	5 4	9 213	4 128.	2 0	9 256	2 154
5	42	9 25	8	100	85.	7 51.	5 150	128.	6 77.	3 20	0 171	4 103	0 25	0 214	3 128	8 30	0 257	1 154
												e Lat			La			

D	R	Lat	De	pliD	iñ,I	Lat	Dep) Di	ft La	De	ep\/D	ift L	at 1	Dep	IIDi	ft Lat.	Dep	[Dif	1	
-		8,00	00,	1 -	-12	3.2	27.0	10	85.	6 52	-		-	_	-11-	-	-	-11-	Lat	Dep
	- 1		01.	1 3		4	27	0:		5 54		1 128		80.6		1 170.			212.8	133.0
	- 1.		OI.	113		4.9	28.1	0		3 54	e 11		-	81.3	11	1	3 107.		213.7	133.6
	3	3.4		11 3	- 1 -	5.8				2 55		4 130		81.6		- 1 .	1 107.	11 33	214.5	134.3
	10	4.2	02.	11 2		6.6				0 55	-	5 131		82.2	11		-	11 24	215.4	134.6
1 -	6	15.1	-	-11 =	-1-	-	-	-		_			-:1-				8 108	7 55	216.2	135.2
	-10		03:			7.5	29.7		1 -2.					82.7				11 3	217.1	135.7
			04.			_	30.7			7 56.		7 133		83.2			5 109.		217.9	136.2
		- "	04.	11 -	- 1	0.0		00	1 3-			8 134	69	83.7			4 110.	011	218.8	136.7
1,		8 5		3 6	- -	0.9	31.8	10	-	4 57.	3 6			84.8		1		11 33	219.6	1 31 3
-	- 1-	_		- 11	-1-		=	-	1 33	3 30.	-	- 33	-		10		1111.		220.5	137.8
		-	06.	11	12	1.7	32.3	11	77			-		85,3	21		111.		221 3	138.3
1			06.0	11 -	10	2.0	32.9		1 33.		11 0	-31		85.9	1:		112.4	•	222.2	138.0
1	٠١.		07.4		- 1-	4.3	33.9	13	22		- 11 -			86.4 86.9			112	11 /	223.0	139 4
1		-	08	11 -	. 1.	5,1	34.5	15		61.		-1-00		87.5			113.4	04	223.9	139.9
1	- 1-	_	08,	- 11	- -	6.5	31/3	-	-	4-	-11-	5 139	_		1		114.0		224.7	140 5
			09,0	11 -			35.0							88,0	216	183.2	114.	266		141.0
1			09.	11 -			36.0		100.	62	5 6	0	0	88 5	17		115.0		226.4	141.5
1	1-	2 -	10,1	11 -	12	-	36,6	19			- 11			89 0			115.	11 .	227.3	142.0
20	- 1		10.6	11 '	. 1-		37.1	20						90.1	20	1 -		11	228.1	142.6
-	- -	-	_	11 -	-		== 6	-	_		- -				-	_	-	11-	2290	143,1
2:	-		11.1	11 /			37.0 38.2	121						90.6	221	187.4	117.1	271	229.8	143.6
2	_	0.5	12.2				38.7	22	1 3.				-	91,2	22	1 7			230.7	144.2
24		0.4	12.7	1 74		-	39.2	23		16 -	_ 11 _		2	91.7		189.1		11.	231.5	144.7
2			13.3			-	39.8	24	106	24				92,2	24	1	118.7		232 4	145.2
26	- -		_	-	_		-	-	_	-	7.	-	- -	92 8	25	190.8	119 3	75	233.2	145.8
27	-		13.8	11			40.3	126		12.	. - / -			93.3	226		1198	276	2310	146.3
28		-1	14,8	11		. 3	40.8	27	107.7	67				93.8	27		120.3		234 9	146,8
29			15,4	79			41.0	11.	109.4	100		-	ál	94-3	28		120.8			147.3
30			15.9	80			42 4	30	110.2				_	94.9	29		121.4		- 1	147,9
31	-		16,4	81				-				-	- -	95 4	30	1950	1219	80	37.4	148.4
32		-	17.0			"	42.9	131	111.1			1 33		95.9	231	1959		281	38.3	148,9
33			17.5	83		5	13.5		111.9			154.		96.5	1000	196,7		82	39.1	149.5
34			18 0	84			44.0		112.8			155,		97,0	-33		123.5	0 1	40.0	150.0
35)	18.6	85			15.3		114.5	/	11	156		97.5	34	198 4			40.8	150.5
36			_	86	-			35					_	98.1	35	199.3	_	85 2	41.7	151.1
37	_	-	19,1	8-	1/ -		2.0	13.10	115 3	72.1		157,				200.1				151 6
38		-1	19.0	88	73		6.6	37	116.2			158		99.1		201.0		87 2		52.1
700			10.7	80	75		7.2	30	117.0	73 7	80	160.		9,0		201.8		88 2	44.2	52.6
40			1.2	00	76		7,7	40	118.7	74 2	00	161	1	00.2	40	202.7	120.7	09 2	45 1 1	53.2
41		-		12	1	-1	2 -						-		_	203.5		90 2	45.9	53-7
		,8 2		91	77	2 4	8.8	41	1196	747	191	152 0			241	204 4	13.7	291 2	46.8	54.2
							9.3		120.4	75 8	92	102.8	110	1.3		20: 2		92 2	47.6	54 8
							9.8		122.1	76.2	93	764	170	2.3		206 1		93 2	48.5	55.3
45	38	.2 2	3 9	95	80.	6 5	0.4	45	123.0	76.0	94	166	10	2 4	44	206 9	129.3	94 2	49 : 1	55.81
45				-6	0.		-:	146	1000		73	-66	-	3					50.2	
47		0 2		07	80	43	7.4	40	123.8	77.4	190	100.2	10	3 9	240	208.6	130.4	196 2	5101	56.9
48	40	7 2	5.4	08	82.	3 3	1.0	48	124.7	78 4	97	167.1	10	4 4	47	209.5	130 9	97 2	51.9 1	57.4
	41	6 2	6.0	90	84	9	2.5	40	26.4	70.0	90.	168 9	10	4 9		210.3		98 2	52.7 1	57.9
		4 2			84	8 4	2.0	150	27.2	79.5	100	160.6	100	6.0	250	211.2	32.0	99 2	53 6 1	58.5
-				Dia	De		-	2:4	Dep	10:	17:4	D	1					Die =	54.4	
	_	h 1.	at il.	Jill]	De	LIL	atil	JHI,	Deli	Lat.	DIR	De) L	at III	Dilli)	Dep /	La:	Diff D	ep ·	Lat
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for 58 Deg.

		1	11. 1		Libert	11 3.141	1 25	11)e	Ditt	Lat	Den 1	Det	Lat.	(Dep	Dut Lat	1)=11
DH	Lai	Det	Din	Lat	_	Dift	Lar	-	-			-		_		
1	00.8	00,5	51	42.8		101		55.0	151	126 6	82.2		1.00	109.5		
2		01.1	52	43.6	28.3	02	85.5			127.5	82.8	1		110.0		
3		01.6	17.7	44.4		03	86.4			128.3	83.3			111.1		1
4		02.2	54	45.3		04	88 1	57.2	54	130.0	84.4	05		111.6		1 1
_5	04.2	02.7	55	_	300	-		_			_	_		_		-
6		03 3	56		30.5	105	88,9	57.7		130.8	85,0			112.2	256 214.7 57 215.5	
7		03.8		47.8		07	89.7	58.8	- 60	131.7	85.5 86.0		173,6	113.3	0 0	
8		04.4		49,5	31.6	09	91.4		4	133.3	86.6			113.8		
9		04.9	11 6 -	1000	32.7	10		59.9	60	134.2	87.1	10		114.4	60 218 0	
10	-	05.4	-	1		-		60.5	161	135.0	87.7	211	176 0	114.9	261 218.9	142.1
11		06.0		3	33 2	111	93.9	61.0	C-	135.9	88,2	12		115.5	62 219.7	
12		06.5	11		34,3	13		61.5	1 -	136.7	88.8	13	2 0	116.c		
13		7 07.6	11 0		34,9	14	95.6	62.1		137.5	89 3	14	179.5	116.5	64 221.4	
15		6 08 2		133 .		15	96.4	62 6		1 38.4	89.9	15	180.3	117.3	65 222.2	144.3
16	-	4 08,7	-		35.9	116	97.3	-	166	139.2	90.4	216	181.1	117.6	266 223.1	144.9
17		3 09,3	110	13303	36.5			63.7	67	140.0	90.9	17	182.0	113.2	67 223 9	
18		1 09.8	11 - 2		37.0		99.0	64,3	68	140.9	91,5			118.7	68 224.7	146.0
19		9 10,3	11 0		37.6		99,8	64.8	69	141.7	92,0			119 3	69 225.6	
20		8 10 9			38.1	20	100.6	65.4	70	142.6	92.6	20	184.5	119.8	70 226 4	147.0
21	17.	6 11 4	11		38.7	121	101.5	65.9	171	143.4	93.1	221		120,4	271 227.3	147,6
22	1 -	4 12.0	11		39.2	22	102.3	66.4	72	144.2	93-7			120.9		
13	19.	3 12.5	73	61.2	39.8	23	103.1			145.1	94.2			121.4		
24	20.	1 13.1	74		40.3		104.0	67.5	74		94.8	11		122.0	11	
25	21.	0 13.6	75	62.0	40.8	25	104.8			146.8				122.5		149.0
26	21.	8 14.	76	63.	7 41.4		105.7							123.1		1
27		6 14,			6 41.9		106.5			148.4				123.6		
28		5 15,			4 42.5		107.3		11				1 /	124 2	11	
29		3 15.			1 43.6	- 11					0 -			125.3		152.5
30		2 16.		-	_		-	-		-	2.0	-		125.8		153.0
31		c 16,	11 -		9 44 2		110.			151,8				126.3	11 0 1 33	
32		7 18.	*11		6 45.		111.			153.5				126.9	1 0 1-3 13	
34				- 1 -	4 45.					154.				127.4		154.7
35		-	10		3 46.			73.		155,1		35	197.1	128.0	85 239.0	
36		_	-11 -	_	1 46.		114.0				101.	3 236	197.0	128	286 239.8	155.8
37		0 20.	2 8	7 73.	0 47.	4 37	1114.	9.74.	87	156.8	101.8	37	198	7 129.1	87 240.7	1 56.3
38		.9 20.	7 8	8 73.	8 47,	9 38	115.	7 75-2	88	157,7	102.4	1 38	199.	6 129.6	6 88 241.	156.8
39	32	7 21.	2 0	9 74	0 40.	5 39	1116.	6 75	7 89	158.	5 102.9	9 39		4 130.		157.4
40		.5 21.		0 75.	5 49.	0 40	117-	4 76.	2 90	159.	3 103	5 40		3 130		
41	34	.4 22.		1 76.	3 49.	6 141	1118.	76.	191	160.	2 104	241	202.	1 131.	2 291 244.0	158.5
42	35	.2 22.	9	2 77.	2 50.	1 42	110.	1 77.	3 92	161.	0 104	42	202.	9 131.	8 92 244.9	9 159.0
4	3 36	.1 23,	4 9	3 78.	0 50	4:	119.	9 77.	9 9:	161.	8 105.	4	203.	6 132.	3 93 245	7 59.6
4	4 36	.9 24.	0 9	4 78.	8 51.	2 44	120.	6 78.	94	1:2.	7 105. 5 106.	2 4		5 133.	9 94 246.	4 160.1
4		.7 24,			7 51.			6 79						_		
4	38	.6 25.	1 9	0 80	.5 52.	3 14	122.	4 79.	5 19	104.	4 106,	7 24	200	3 134	0 296 248.	2 101.
1	39	.4 25.	6 9	7 81	3 52.	4	7 123	2150.	111 0	7 1105.	2 107.	8 4	8 208	0 125	5 97 249. 1 98 249.	0 162
4		.3 26		0 82	.2 53		124	081	1 9	166	0 108	4 4	9 208	8 125	6 99 250	7 162
4	2 41	.1 26.	2/10	00 82	0 54	5 15	0 125	8 81.	7/20	0 167	7 108	.9 25	0 209	7 136	.2 300 251	6 103.
			-115	10 5	37	3	a D	1 2	1	# 0	Ta		f Der	Ia	Diff De;	La
-	III(D	ep La	11.	שוחו	chira	וטוויי	II. De	Pira	. HOI	1, 10	1 213	. 10				

-	-			33			11/1/4		Capital S			7				ST	2	5.
DH	Lat	De	PID	Pif	La	Dej	Di	il Lar	Dep)Di	t Lat	Dep	1/Di	ft Lat.	Dep	IND: #		
-	00.8	800,	6 6	1	42.2	28.	101	83	56.9	1	1	-	_	-		חוש	La	De
2	01.	1	-11 -	43	43.1	120.1	02		57.0		1 .			1 166.			208.	1 140
3	02.	5 01.			43.9	1 4	11	85.4	57.6	53		- 37		2 1167.	5 113.	52	208	9 140
4	03.5	02.	_ 11	54	44.8	30 2	11 -		58.2			1 . 3.	- 11 '		3 113.		209	7 141
5	04.1	02.	8	55	45.6	30.8			58 7	55						1 34	210.	6 142
6	05.0	03		_	46.4	21.5	105		59.3		-				9 114.	55	211	4 142.
7		03.			47.3	31 9		88.	59.8					1	1 3.		212.	2 143
8		04.	-11		48.1				00.4				8 07		115.	57	213.	
9		505.	-11			33.6				58			4 01		116.	58	213.	9 144.
10	08	-	-11 7	c	49.7	33.6				60	1 -					59	214.	7 144
11	09.1	06	2 6	1	50.6	-	111	-	62.1	161	3				117.	60	215.	5 145.
12	-	06.		-	51.4	34,7	12	1 0		62	133.		211			261	216.4	146,
13		07.		!	52.2		13		63.2	63			-	1-13-1		62	217.2	
14		07	A 1 4	4	52.1	35.8	11 -		63.7	64	1	1			119.	63	218.0	147.
15	12.4	08.		5	53.9	36.3	15		64,3	65	1					64	218.	147,
16	13 3	08,		6	£ 1 7	36.9	-			-				178.	120.2	65	219.7	148.
17		09,			55.5	37.5	116		64.9	166	1.31.			179.1	120.	266	220.	-
18		10,				38.0			65.4	67				1-13.				149.
19		10.				33.6			66.5	68	139.						222.2	149.
20		11.	11		58.0	39.1	20		67.1	69 70	140.1					69	223.0	150
21	17 4	11	-11 -	- 1	_	_	-		_	-	140.9		-11			70	223.8	151.0
12	18.2		11		58.9	39·7 40·3	121	100.3		171	141.8			3			224.7	151
23	19.1	12.0	-11			40.8	11	101.1		72	142.6			184.0	124.1	72		152.
24	19.9	1	111		61.3	41.4	23	102.8	60,0	73	143.4			184.9	124.7	73	226.3	162
25	20.7			- 1	62.2	41.0	25	103.6	60.3		144.2			185.7	125.3		227.1	153.2
16	21.6	-	5 7	- I-			-			75	145.1	_	-	186.5	125.8	75	228.0	
27	22.4	15,1	11/7		3.3	42.5	126	104.5		176	145,9		N. Contraction		126.4	276	28.8	40000
28		15.7	11		4.7		27	105.3			146.7			188.2		77 3	229.6	154.9
29	24.0	1 3 '	11		5.5	44.2	29	106.9	71.6	78	147.6			189.0	127.5	-01	130.5	134.5
30	24.0	16,8				44 7	30	107.8	72.1	79	148.4		11 -2	189.8	128.1		-	156.0
1	257	17.3	-	- 1:		11/	-	-	72.7	80	149.2	100.7	30	190.7	128 6		32.1	156.6
	26,5			- 1	7.1	45.3	131	108.6	33,3	181	-	101,2		191.5	120.2	281	32.9	
!		18.5		-	8,8		32	1 2 77 78	73.8	82		101.8		192.3	129.7	0 . !	33.8	157.1
	0	19,0	11 0			47.0	33	111.1	74-4	83	151,7	102.3		193.2	130.3	0-1	6	157.7
	29.0		11 0		2	17.5	34		74.9	84	152.5	102.9	3.	194.0	130.9	84 2	-	158.8
- 1	29.8	20.1	86	-				-	75.5	-	153.4	103.5	35	194.8	131.4	85 2	36,3	159.4
		20.7	110	1/	1.3	18.1		112.7		186	154.2	104.0	236	195.6	132.0	286 2	37.1	-
0 1	31.5					18.7	37	113.6	76.0	87	155,0	104.6	37	196.5 197.3 198.1	132.5	87 2	37.0	159.9
	32.3		80	1/2	3.0	9.8	30	114.4	77.2	88	155 9	105.1	38	197.3	133.1	88 2	28.8	161.0
	3.2		90	1/2	4 6	0.3	39	115.2	77.7	89	156.7	105.7	39	198.1	133,6	89 2	19.6	161.6
			-		_		40	116.1	0.3	90	57,5	100.2	40	199.0	134.2	90 2	40.4	162.2
	4.8	22.9	91		5.4 5	0.9	141	116 9	8.8	191	158.3	106,8	241	700 Q			41.0	.6.
	5.6	43,5	92	7	6.3 5	1.4	42	117.7 7	9.4	92 1	59.2	107.4	42	200.6	135.3	92 2	42.1	102.7
4 3	6.5	4.6	04	77		2.0	431	210	0.0	2314	00.0	107.9	43	201.4	135,9	91 2	42.0	163.8
5 3	7.3	15.2		135	7.9 5	2.0							44	202.3	136.4	94 2	42.7	6
			95				45	21.08	1.1	95 1	61.7	109.0	4.5	202 7			44.6	65.0
7 3	9.0 2	5.71	90		.6 5	3.7				9011	2.5	100.0	340 I:	202.0	1 A - 6	- 46		
8 3	9.8 2	6.0	08	00	.4 5	4.2	47 1	21.9 8	2.2	97 1	63.3	110.2	47	204.8	138.1	97 2	15 4	65.5
1 -0 .	0.6			0.1	.2 5	4.81	48 1	22.7 8	2.8	08 I T	64.1	10.7	7-14	003.01	20.71	07 94		
2 4	1.62	8 6	100	02	. 1 5	5.4	49 1	23.58	3.3	99 1	65.0	111.3	49 2	06.4	39.2	00 2	17.0	6-0.0
10	-		-	62	29 5	3 9 1 at [201	24.40	3.9 2	00 1	05.8	11.8			39.8	300 2	18.7	67.2
עיי	epil.	3 1	71H	D	er If.	at	Diff!	Det	at D	fift)	Der	Lat	Diff	Dep	Lat	D:# D		
		in year			1 1 1		1000		Market 1		V P.			-	1	Dia D	ep	Lat
																		~

for 56 Deg.

D.61	Tati	Der	Ditt	Lat	Dep[Dift	Lat 1	De I	Dith	Lat	Dep	D:#1	Lat	Dap 1	Dift Lat	Dep
-	00.8			41 8	-	101	82.7			123 7		301	164.6	115,3	251 205 6	142.0
1	01.6			42.6		02	83.5			124.5	87.2			115.8	52 206.4	
- 1	2.5			43.4		03	84.4			125.3	87.7		156.3	116.4	53 207.2	
	-	02.3		44.2		04	85 2			126.1	88.3			117.0	54 208.0	
	04.1	-		45 0	31.5	05	86,0	60.2	55	1 2 6 . 9	88.9	05	167.9	117.6	55 208.8	146 2
	04.9	03.4	56	45.9	32.1	105	86 8	60.8	156	127.8	89.5	206	168.7	113.1	256 209.6	146 8
	05.7		- 1	46.7		07	87.6		57	128.6	900			118.7	57 210.5	
	06.6	04.6		47-5		08	88.5		1 - 1	129.4	90.6			1193	58 211.	
	07.4	-	4 1	13.5	33.8	09		62,5		130.2	91.2			119,9	59 212.1	
10	08 2	05.7	60	49.1	3+4	-10	90.1		-	131.0	918			120.4	60 212.9	
	09.0			50.0	35.0	111	90.9			131.9	92.3			121,0	261 213 8	
		00.9			35.6	12	2 1	64.2		132.7	92.9			121.6	62 214.6	
	10,6				36.1	13	92.5			133 5	93.5	14		122.7	64 216.2	151 4
14	12.3	08.0			30.7	14	04 2	66 c		135.1	94.6		176 1	123.7		152,0
-			_	-			950			136.0	95 2	-	176.9	-	266 217.8	
16	13.1			54.9	37.9	116	95 8	67 1	67	136.8	95.5	17		124.4	67 218.7	
18	13,9				39.0	18		57.7	68	137.6	96 3	18		125 C	68 219.	
19		10.9	69	56.5	39 6	19		68.2	69	138 4	96 4	19	179 4	1256	69 220.	
20	16.4	11.5	11	57.3		20	93.3	68 8	70	139.2	97.5	20	180 2	126 2		1 154,8
21	17.2	12,0	71	58 1	40.7	121	60 1	69,4	171	140.0	98.1	221	1810	126.7	271 221.0	155.4
22		12.6	44		41.3	22	99.9		72	140.9	98.6	22	181,8	127.3	72 222 1	
23	14.	13.2			41.9	23	100.7	70.5	73	141.7	99 2			127.9	73 223.	6 156.6
24	19.6	13.8			42.4	24	101.6		74	142.5	99 9			128.5		4 157.1
25	20.5	14 3		_	43.0	25	102 4	71.7	75	143.3	100 4	11-	-			2 157.7
26	21.3	14.9	76	62.2	43.6	126	103.2		175	144.1	100 9			129.6	276 226	
27	22.1	15.5			44 2	27	104.	72.8		145.0				130 2	77 226.	
28	22.9			1 -	44 7		104.8		11	145 8	102.1			130.8	78 227.	
29	23.8	1000	11 3-	1	45 3	30	105 6		79		1 3000		188.4		79 228. 80 229.	
30	24.6	_	-		45.9	-		-	-	148.2	1-	-	-		281 230	
31	25.4				46.5	131	107,3		181	140.1				132,5	82 231.	
33		18.4		1	47.6		108.9		11 -		105.0	- 11	1	133.6	83 231.	
34	- A	19.			48.2	34	109.							134 2	84 232.	
35		20 1	1 0		48.7	35		77 4	11 0						85 233.	
36	29.	-			-	136	113.4	78.0	186	152.	106.	236	193.	135.3	286 234	
37		21,2			3 49.9	37	112.5	78.6	87	153.	107.	2 37	194	1 135,9	87 235.	0 164.6
38	31.1	21.	88	72.1	1 50.5	38	1113.0	179.1	88	154.0	107.	8 38	194.	136.5	88 235	9 165.2
139		22.4	4 89	72.9	9 51.0	39	113.	8 79.7	1 89	154.	108.	4 39	195.	7 137.1	89,236.	7 165.7
40		23.0	90	73.	7 51.6	40	114	80.	90		109.			6 137.6		.5 166.3
41	33.	6 23.		1 74.	5 52.2	141	115.	5 80.9	191	1 56.	109.	5 24	197.	4 138.2	291 238.	3 166.9
42	34.	4 24	1 92	75.	3 52.8	42	115.	3 81.4	92	157.	110.			2 138.8	92 239	.1 167.5
43	35,	2 24.	7 93	76.	2 53 3		144/		11 2	158.	110.	7 4	1199.	8 139.4	93 240	.0 168 o
44	30.	0 25			0 53.9	94	117.	282	94	159.	7 111.			6 140.		.6 169.2
45	30.	25.			8 54		1	-		-			-	-		_
46	37.	7 26.	4 9	78.	6 55.	146	119	18.	119	161	5 112.	0 4		3 141 7	97 242	169.8
47	38.	5 27. 3 27.	9	7 79.	4 55.	45	120.	2.84		162.	2 112.	6 4	8 203	1 142.	98 244	.1 170.9
49		1 28.	1 0	81	1 56.	40	122.	0.85.	51 91	0 163.	0 114.	1 4	9 203	9 142.	8 99 244	1.9 171.5
150	41.	0 23.	7 10	0 81.	9 57-	4 150	122.	8 86.	6 20	0 163.	8 114.	7 25	0 204	7 143	4 300 24	5.7 172.1
Di	A De	D I	T D	D.	La	Di	Den	La	D	A Dep	La	Di	A De	Lat	Diff De	
-		7 24	101			11-11		1	11-			4		-		

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0.6	.1	D	ID:A	11.00	10	017:4	-	10- 1	1:3:4		D 1	Dis	I T	10	D'0		-
Dif		-	חות	_	Dep	-		De	Dill		-	Ditt	_	Dep	Dift	Lat	Dep
1		00.6	51		30.0		81.7			122 2	88.8		162.6	1000	251	203.1	147.5
2	01.6		52			02		60.0		123.0	89.3		163.4			203.9	
3	1	01,8	53		31.2	03		60.5	53	123.8	899		164.2		1000	204.7	
+	1 -	02.4	54		31.7	05	84.1	61.7	54	124.6	90.5	1 1	165.8			205.5	
5		-	56		-	106				116.1	-	-			_	206.3	-
6	05.7	03.5	57	45.3	1	07		62.3	57	127.0	91.7	206	156.7	121,1		207.1	
7 8	06.5		58		34.1	08		63.5		127.8	92.9		168.3			207.9	
9	07.3		59		34-7	09		64.1	59	128.6	93.5		169.1			209.5	
10		=5,9	60	48.5		10		64.7	6c	129 4	94.0	10	169.9			210.3	
11	05.0	06.5	61	49.3	35 9	111	89.8	65.2	161	130.2	94.6	211	170.7			211.1	_
12	09.7		62		36.4	12		65.8		131.1	95.2	1	171.5			212.0	
13		07.6	63		37.0	13	91.4	66.4	63	131.0	95.8		172.3		63	212.8	154,6
14		08.2	64		37.6			67.0	64	132.7	96.4	14	173.1	125.8	64	2136	155.2
15	12.1	08.8	65	-	38,2	15	_	67.6	65	133.5	97.c	15	173 9	126.4	65	214.4	155.8
16		09 4	66	53-4	38.8	116		68.2	166	134.3	97.6	216	174.7	127.0		215.2	
17		10.0	67	54 2	39.4	17		68.8		135.1	98.2		175.6		67	216.0	156.9
18	1 1 1 1 1	10.6	68		40.0	1		69.4		135.9	98.7		176 4	_		216.8	
19	1 .	11.2	70		40.6	19		69,9		136.7	99.3		177.2			217.6	
10	-		-	-	-	-		70.5	70	137.5	-		178.0			218.4	
21		12,3	71		41.7	121		71.1	173	138 3		11	178 8			219.2	
22	1 -	13.5	72	1	42.3	22	99.5	71.7		139.1	101.7		179.6		1	220.0	
24	1	14 1		1	43.5	24	100.3		73		102.3		181,2		74	220.9	161.1
25	1	14.7	75		44 1	25	101.1		75		102,0		182.0		7.5		161.6
26	210	15.3	76	-	44 7	126	101.9	-	176	-	103.4	226	182.8	_		223.3	_
27		15.0	77		45.3	27	102.7		77		104.0		183.6		77		162.8
28		16.5			45.8	28	103.6				104 6		184.5			224.9	
29	23.5	17.0	79	63.9	46.4	29	104.4	75.8	79		105.2	29	185.3		79	225.7	164.0
30	:4.3	17.6	80	64.7	47.0	30	105.2	76.4	80	145.6	105.8	30	186.1	135.2	80	226.5	164.6
31	25.1	18.2	81		47.6		106 c		181	146.4	106 4	231	186.9	135,8	281	227.3	165.2
32	25 9	1.0 6			48.2		106.8		82		107.0		187.7		82		165.8
33		19.4	83		48.8		107,6		83		107.6		188.5		83	228.9	
34		20 0	84		49.4	34	108.4	10	84		108.2		189.3		84		166.9
35	28.3	-	85		50.0		109.2	79.4	85	_	108.7	35	190.1	138.1	85	_	167.5
36	29.1	21,2	86	69.6			110.0		186		109.3		190.9			231.4	
37		21.7	87	1	51.1	37	110.8		87	151.3	109.9	37		139.3	1 00	232.2	
38	30.7	22.6			51.7	20	112.5	87.7	80	152.0	110.5	30	192.5	140.5	80	233.0	160.3
		23.5	90	72.8	52.9	40	113.3	82.2	90					141.1		234.6	
40		24.1			53.5		114.1			-							
	33.2	24.7			54.1	42	114.9	82.5	02	155.2	112.0	42	105.8	141.7	91	235.4	171.6
43	34.8	25.3	91		54 7	43	115.7	84.1	92	156.1	113.4	42	196.6	142.8	02	237.0	
44	35,6	25.9	94	76.0	55-3	44	116.5	84.6	94	156.9	114.0	44	197.4	143.4	94	237.8	
45	36.4	26.5	95	76.9	55.8	45	117.3	85.2	95	157.8	114.6	45	198.2	144.0		238.7	
46	37.2	27.0	96	77.7	56.4		118.1			158.6	115.2			144.6		239.5	
47.	38.0	27.t	97	78.5	57.0	47	118.9	86.4	97	159.4	115.8	47	199.8	145,2		240.	
48	38.8	28.2	98	79.3	57.6	48	119 7	87.0	98	160.2	116.4	48	200.6	145.8	98	241.1	175.2
					58.2						117.0			146.4		241.9	
														146.9		242.7	
Dill	Dep	+La	Dia	Dep	Lat	Dift	Dep	(La	Diff	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat
	N. visi	100						4.		3175		Nin's		•			

for 54 Deg.

Din	Lat	De	Dif	Lat	Dep	(D:n	Lat	Dep	D.F	Lat	Dep	Dif	l Lat	Dep	Dift	1 Lat	Dep
1	00.8	00 6	51	40.7	30.7	101	80,7	60.8	151	120.6	90 9	201	160.5	121.0	251	200.4	-
2		01.2	7.		31.3	02		61.4	52				1 .			201 2	
3	02.4	31.8	53	42,3	31.9	03		62.0	53	122.2	91.1	03	162.1		53	202,0	152.
4	03.2	22.4			32.5		83 1	62.6	54	1130		04	162.9		54	202.8	
_5	04.0	-	55		33.1	05	83.9		55	123.8	93.3	05	163.7	_	55	203.6	153.
6		03.6	56		33.7	106		63.8	156		1000	206		124.0	256	204 4	
7	05.6		57	45.5	34-3	07	85.5		57	125 4	1	08	165.3		57	205.2	
8	06.4	35.4		46.3	34-9	08	1000	65.6	-	126.2	95.1	00	166,1	125.2	58	206.6	
9		06.0	60	47-1	35.5 36.1	10	87.8		59	127.8	95.7	10	167.7	-	59	207,6	23
11	3.80		-	48.7	36.7	111	88.6	_	161	128.6	96.9	211	168.5	127.0	261	208,0	-
12	09.6			19,5	37.3	12	89.4			129 4	97.5	12	169.3		62	200,0	
13		07.8	63	50,3		13	90.2			130.2	98.1	1	170.1	0	63	2100	
14	11.2		64	51.1	38.5	14	91.0		64	131.c	98.7	14	170.9	128.8	64	210.8	
15	12.0	09.0	65	51 9	39 1	15	91.8	69 2	65	131.8	99.3	15	171.7	129.4	65	211.6	159.
16	12.8	09.6	66	52.7	39.7	116	92.6	69.8	166	132.6	99.9	216	172.5	130.0	266	212.4	160.
17	13.6	10.2	67		40.3	17	93.4		67	133.4	100.5	17		130.6	67	213,2	100
18	14.4			54.3		18	94.2	71.0		134.2	100	18	174-1	-	68	214.0	the same of the
19	15.2		7.	55.1		19	95.0	71.6		135.0	101.7	19	174.9	Charles and the second	69	214.8	
20	16.0	_	_	55.9		20	95.8		7°	135.8		20	1757		70	215.6	-
21	16.8			56.7		121	96.6		171	136 6		221	176.5		271		163.
22	17.6			57.5		22	97.4			137,4		22	177.3		72	217.2	
23	18.4			58.3		23	98.2			138.2		23	178.1		73	218.C	164.
24	19.2			59,1		24	99.6		74	139 0		24	179.7		74 75	218.8	164.
26	20.8			60.7	_		100.6		176	140.6		226	180.5		276		-
27	21.6			61.5			101.4		77		106.5	27	181.3		77	220,4	
z8	22.4			62.3		0	102.2			142,2		28	182.1		78	222.0	
29	23.2			63.1		7.4	103.0		79	142.9		29	182.9		79	222.8	167
30	24.0			63.9		30	103.8	78.2	80	143.7	108.3	30	183.7	138.4	80	223,6	168.
31	24.8	18.7	81	64,7	48.7	131	104.6	78,8	181	144.5	108.9	231	184.5	139.0	281		169.
	25.6			65.5			105.4		82		109.5	32		139,6	82		169,
33	26.4	19.9		66,3			106.2			146.1			186.1		83	226.0	
34	27.2	-		67.1		34	107.0	80.6	84	146,9		-	186 9		84		170.
35	28.0	_		67.9			197.8		85	147.7	111.3			141.4	85	227.6	
36	28.7			68,7			108.6						188.5		286	228.4	172.
37		22.3		69.5			109.4			149.3			189.3		87	229.2	
		22.9	88	70.3	53,0	38	110.2	83.0	88	150.1	113,1	30	190 1		88	230,0	173
39 40		23.5 24.1	00	71.9	53.6	39 40	111.8	84.2		150.9	114.2	40	190.9		90	230.8 231.6	173
41					-		112.6										
42	32.7 33.5		91	72.7	54.0	141	113.4	85.5	191	152.5	114.9	42	193.3			232.4	
43		25.9	92	74.3	56.0	42	114.2	86.1	92	154.1	116.1		194.1			233.2	176
44	35,1	26,5	94	75.1	56.6	44	115.0	86.7	94	154.9	116.7	44	194.9			234.8	
		27.1		75.9		45	115.8	87,3	95	155.7	117.3	45	195.7			235.6	
45	36.7			76.7		146	116.6	87.0					196,5			236,4	
47 48	37.5	28.3	97	77.5	58.4	47	117.4	88.5	97	157.3	118.6	47	197.3	148.6	97	237.2	
	38.3	28.9	98	78.3	59.0	48	118.2	89.1	98	158.1	119.2	48	198.1	149.2	98	238.0	179.
49	39.1	29.5	99	79.1	59.6	49	119.0	89,7	99	158.9	119.8	49	198.9	149.8	99	238.8	179
50	39.9	30.1	100	79.9	60.2	150	119.8	90.3	200	159.7	120.4	250	199 7	150.4		239.6	180.
Diff	Dep	Lat	Diff	Dep	Lat	Dift	Dep	La	Diff	Der	La	Dift	Dep	Lat	Diff	Dep	Lat

	Last	1)0.1	Dift	[0:	Dep	ID fd	Lat	Denl	D.AI	I at	Dep	n:a:	Lat	Dan I	Diff	Lat	Den
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2	01.6			41.6		02		53,4	- 1	119.8	93.6			124.4	52	198.5	155
3	03.2	- 200	1 7 7	42,5		03		54 0	53	121,3	94.8	-		1266	53 54	200.1	
7	03 9		55	43.3		05		04,6	55	122.1	95.4	05	161.5		55	200.9	
6	_	03 7	56	_	-	106		65 3		122.9	96 0	-	162.8		256	201 7	157.
7	05.5		57			07		65.9		1237	96.7			127 4	57	202,5	
8		04.9			35.7	08		66.5		124.5	97.3			128 1	58	103.3	158
9	07.1	05.5	59	46.5	36.3	09		67.1		125 3	97.9	09	164.7	128.7	59	204.1	159
10	37.9	06 2	60	47-3	36.9	10	86.7	67,7	60	126.1	98.5	10	165.5	129 3	60	204.9	160.
11	08.7	06,8				111	87.5	68.3	163	126.9	99.1	211	166.2	129 0	261	205.6	160.
12		07.4		48 9	38.2	12		690		127.6	99.7	12	167,0	130.5	62		161.
13		08.0			38.8	13		69 6	63		100.4	13		131.1	63	207,2	
14.		08.6		-	39 4	14		70.2	64		101,0			131 8	64	208.0	
15	_	09.2		_	40.0	15		70.8	65	-	101.6	15		132.4	65	208,8	
16		09 9	11 -		40.6	116	91.4		166		102.2	11		133.0	266	209 6	
17		10.5			41.3	17		72.0			103.4	17		133.6	68	210.4	
18		11.1			41,9	19		73.3			104.1	19	1	134.8	69	211.0	
19		12.3			43.1	20		73.9	70		104.7	20		135.5	70	212.7	166
-	-	-		-	_	121		74,5	171	_	105.3	-		136.1	271	-	-00
21	17.	12 9			44.3	22		75.1			105 9			136.7	72	213,5	
23		14.2			44,9			75.7	73		106.5	41		137.3	73	215.1	
24	1 0	14,8			3 45.6		1	76.3	74	137,			1 2	137.9	74	215.9	1-60
25	19.	1	11	1			98	77.0	75	137	107.7	25	177.	138.5	75	216.7	169
26	20.	16.0	76	59.	46.8	126	99	17.6	176	138.	108 4	226	178.	139.1	276	217.5	169
27	21.	1	11 .	60.	7 47-4	27		78.2	77	139.	5 109.0		178	139,8	77	218.2	170
28	22.	17.			5 48.0			78,8	11		109.6	11	179.	140,4	78	219.0	
29					48.6			10 2 .	79		110.2	.11		4 141.0	79	219.8	
30	23	6 18.	-	-	49.1		_	4 80.0	-	-	110.8	-		141 6	80	220,6	
31					8 49.9			2 80.7			6 111.4			142.2	82	221.4	
32		2 19.	11 0	65.	6 50.5					143.	4 1 12.1	11 -		6 143 5	83	222.2	
33		8 20	- 11	100	2 51.7						0 113,	11	1 -	4 144.1	84	223,8	
34	1000	6 21.	-		0 52.		1 .	10			8 113.	1	1 -		85	224.	
36	4	_			8 53,0			-			5 114.	236		9 145,3	286	225.	-
37	4 10 01	2 22.			5 53.	37	107.	9 84.4			3 115.			7 145.9	1 0-	226.	
38		9 23.			3 54.2		108.				1 115			5 146.5			
39	30.	7 24.	0 8	9 70.	1 54.	39	109.	5 85.6	89	148.	9 116.	5 39	188.	3 147.2	89	227.	7 177
40		5 24.	6 9		9 55.4		110.				7 117.			1 147.8		228.	4 178
41		3 25.	2 9	71.	7 56.0	141	111.	1 86.	191	150.	5 117.	6 241	189.	9 148.4	291		3 179
42	33.	1 25	9 9	2 72.	5 56.	6 42	III.	9 87,	1 92	151.	3 118.	2 42	190	7 149.0	92	230,	1 179
43		9 26,	5 9	3 73.	3 57-	3 43	112.	7 88.	93	152	1118.	8 43		5 149.6	93	230.	9 180
44		7 27.	1 9	4 74	1 57.	9 44	113	5 80.	94	152	9 119.	4 44		2 150.2	94	231.	18
45		5 27.			9 58.						6 120.			0 150.8			1 0
46		2 28.	3 9	0 75.	6 59.	1 146	1115	089,	9 196	154	4 120.	7 246	193	8 151.	296	233.	1 181
47	37:	0 28.	9	7 70.	4 59.	7 47	1115	6 90.	97	155	2 121.	3 47	194	6 152.	97	234	9 18
48	37.	8 29. 6 30.	3	77.	061	3 4	110	401	7 0	156	8 122	5 4	105	4 152.	99	234.	6 18
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1 0	0,8	00,6	51	39	9 6	32.1	101		63.6	151	117.3	95,0	201	156.2	126.5	251	195.1	158.0
2 0	1.1	01,3	52	4	0.4	32.7	02		64.2	2	118.1	95.7		157.0		52		158.6
3 0	2.3	21.9	53			33 4	03		64.8	1 23 1	118.0	96.3			127.7	53	196.6	
4 0	3.1	22.5	54			34.0	04		65.4		119.7	96.9		-	128.4	54		159.8
5 0	3.9	33.1	55	4	2.7	34.6	05	81.6	65.1	55	120.5	97-5	05	159.3	129.C	55	198.2	
6 0	4.7	03,2	56	4	3.5	35.2	106	82.4	66.7	156	121.2	.98.2	206	160.1	129.6	256	198.9	161.1
		24,4	57			35.9	07	83,1	67.3	57	123.0	98.8	07	160.9	130.3	.57	199.7	161.7
	-	05.0				36.5	03	83.9	158.0		122.8	99.4	08	161.6	130.9	58	200.5	162.4
	7.0	35.7			5.8	37.1	09	84.7	68.6		123.6	100.1	09	162.4	131.5	59		1630
		26.3		1	6.6	37.8	10	85.5	69.2	60	124 3	100.7	IC	163.0	133.2	60	202.0	163.6
	_	06 9	-	1	7.4	38.4	111	86.	69.0	161	125.1	101,3	211	164.0	132.8	261	202.8	164,2
		07.6			8 2		12		70.5	62		101.9			133.4	62		164.9
		08,2			9,0				71.1	63	116.7				134.0	63		165.5
		08.8			-	40.3	14	85.		11 .		103.2			134-7	64		
	11.7	1		- / -	50.5		15	-	172.4	11		103.8	15	167.1		65		166.8
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- 1		12.	-11			43.4	11		5 74.9	1	131.		11		137.8	70		169.3
20	15 5	12.	0 7	0	54.4	44,1	20	93			132.	107.0	-	-	-		209.6	169.9
21	16.3	13	2 7	1	55.2	44.7	121		76			107.6		171.7	139.1		210.6	170.5
22	17.1	13.	8 7	2	56.c	45.3	22		8 76.8			7 108.2			1	72	1	171.2
23	17 9	14,	5 7	3	56.7	45 9	23	95-	774	73	134.4	108.9	23	173.3	140.3	73	212,1	171,8
24	18.7	1 15.	1 7	4	57-5	46.6	24	96.				109,5						172.4
25	19 4	1 15.	7 7	5	58.3	47.2	25	97.	1 78.	75	136.	110,1	25	174.2	141.6	75	213.7	173,1
26	20,7	16.	4 2	6	59.1	47.8	126	97.	9 79.	176	1 36.	8 110.8	226	175.6	142.2	276	214.	173.7
		17.	- 11		59 8	48.		98.			137,		27	176.4	142.9	77	215.	174,3
		8 17.			60.6		- 0	99.		78		-	28	177-2	143.5	78		174.9
29	22.	10			61.4	1			2 81	79	139.	1 112.6			144,1		216.	175.6
	23.	10			62.2	50.	30	101.	0 81,		139.	9 113,	3 30	178.	144.7	8.	217.	176.2
		-	-11-	_	_	51.0	-	101	8 82	4 181	140.	-		170.	145.4	281	118.	176.8
31	24.	9 20,	211	. 1	63.				6 83.						3 146.0			177.5
32		6 20,	01 6	. 1		5 52.	11		4 83.						1 146.6			1.8.1
33		4 21.	4			3 52.			1 84.		2.2		0 -		0	11 0		178,7
34	1	2 22				1 53.		100 000	985.				11	1 0	6 147.			5 179.4
35	-	_		-			-11		-	-		-					-	
36		0 22	/			8 54.		105	7 85.	9 186		5 117.	• • •		140.	-		3 180.0
37		8 23				6 54.		100	5 86.	2 87		3 117,			2 149.1			0 180,6
38	29.	5 23	9	5.5	60.4	4 55.	4 39	107	2 00		140.	1 118.	3 3	135	7 150.			8 181,2
39		3 24	5	9	69.	2 56.	39		087.	5 09	1140.	9 118	2 3		5 151.			6 181.9
40	31.	1 25	2	90	09.	9 50.	6 40					6 119.			_		_	4 182.5
41	31.	9 25	.8			7 57.		109	.6 38.	7 191		4 120.		1 187.	3 151,	7 29	1 226.	1 183.1
42	32.	6 26	4	92	71.	5 57.	9 42		3 89.			2 120.			1 152.	3 9	2 226	9 183.8
43	33	4 27	, 1			3 58,	- 11				150	0 121.	5 4	3 188.	8 152.	9 9	3 227.	7 184.4
44	34.	2 27	.7	94	73,	0 59.	2 44	111		6 94	150	8 122.	1 4				4 228.	5 185.0
	35.	0 28	.3	95	73.	8 50.	8 4	112	,791.	2 9	151	5 122.	7 4	5 190	4 154.	2 9	5 229	2 185.6
45		7 28		_	-	_	4 14	111	.5 91			.3 123.	3 24	6 191	2 154.	8 29	6 230	0 186.
47	26.	5 20	.6	07	75.	4 60.	0 4	1114	2 92	5 9	153	1 124			9 155.	4 9	7 210	.8 186.
48	27	3 30	.2	08	76	2 61.	7 4	8 115	.002	1 0	153	.9 124	6 4	8 192	7 156.	1 9	8 231	.6 187.
49	13%	1 30	8	90	76	0 62	3 4	1116	.8 93	8 9	9 154	.6 125.	2 4	9 193	.5 156.	7 9	9 232	4 188.
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_	-	00,6	_	-	32.8			64.9	-	115.7	97.1	201	_	129.2	251	192.3	_
		01,3	52		33.4	02		65.6		1164	97.7		C	129.9	52	193.0	1
		01.9	53		34.I	03		66.2	53	117.2	0 4			130.5	53	193.8	10
		02.9	54		34.7	04		66.8	54	118.0	99.0	04		131.1	54	194.6	
_5	03.8	03.2	55	42.1	35.3	05	80,4	67.5	55	118.7	99 6	05	157.0	131.8	55	195.3	
6	04.6	03,9	56	42.9	36.0	106		68.1	156	119.5	100.3	206	20	132.4	256	196.1	164.6
7	-	04,5	57	43.7	1-	07	1 2 1 1	68.8	57	-	100 9			133.1	57	196,9	165.2
8		05.1	58		37.3	08		69.4			101,0			133.7	58	197 6	165,9
9		05.8			37.9	09		70.1	59 60	1	102.2			134.4	59	198.4	
10	07.7	-	-	-	-	10		70.7	-	-	102.8			135.0	-	199.2	_
11		07.1	11 0	1	39.2	111		71.3			103.5			135.6	261	199.9	167.
12		07.7	11		39.9			8 72.0 6 72.6			104.1			136.3	63	200.7	168.
13	1 3 11	09.0		49,0		11		3 73.3	11		105.4			137.6	64	201.4	169.
15	1	09.6	11 0		41.8		88.				106.1			138.2	65	202 2	109.
16	-	10.	-		42.4	11-	-	9 74.6			106.7	216	_	138.8	166	-	-
17		10.0	1 .	1,	43.1	17	-	6 75.2	11 -		107.3	17		139.5	67	203.7	171.
18	1 .	8 11.6			43.7			4 75.9	11 - "		108.0			140.1	68	204.5	171,
19		6 12.2			9 44.4			2 76.			4 108.6		167,7	140.8	69	206.0	172.
20	15	3 12.9	79	53.	45.0	20			11		2 109,3		168 9	141.4	70	206.8	173
21	16.	1 13.	7	1 54.	4 45 6	121	92,	7 77.8	171	131.	0,109 9	121	169.		271	207.6	-
22	16.	9 14.	- 11		46.	11		4 78.4		131.	7 110,6			142.7	72	208.3	
23	17.	6 14,	8 7:		9 46.9	_	94	2 79.1	73	132.	5 111.2			143-3	73	209,1	175
24	18.	4 15.	- 11		7 47.6			0 79.			3 111,9			144,0	74		
25	19.	2 16.		_	4 48.2	25		7 80.4		134.	0 112.5	25	172.	144.6	75	210.6	176
26	19.	9 16.		-	2 48.9	126		5 81.			8 113,1		173.	145.3	276	211.4	177
27		7 17.			0 49.	11 -		3 81,			6 113.8			145.9	1	212,2	178
28		4 18.			7 50.	- 11		C 82			3 114.4			146.6	78	212.9	
29		2 18.	11 0		5 50.1 3 51.			8 82.			1 115,1			147.2	79 83		179
30		0 19.	-		-	-		_	-11-	-	9 115.7				-	-	-
31		7 19	-	7	8 52.			3 84.			4 117.0			9 148.5	181		180
32		3 21,	- 11					985.			2 117,6		1	149.1	83	216.	181
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35	1 .	8 22.	- 11 -		- 1	- 11		4 86			7 118 9	-		151.1	85	1 .	1182
36		6 23.	1 8	6 65.	9 55.			2 87.	4 186	142.	5 119 6	2 3		151,7	286		
37		3 23.	8 8	7 66.	6 55.	9 3	104	9 88,	1 8		2 120.2			5 152.4	87	12	
38	29	1 24	4 8	\$ 67.	4 56.	6 38	105	.7 88.	7 81	8 144.	0 120.0	31	182.	3 153.0	88	220.	185
39			1 8	9 68.	2 57.	2 39	106	,5 89.	4 89	144.	8 121.5	1 3	183.	1 153,6	1 69	221.	1185
40	30.	6 25	7 9	0 08.	9 57.						5 122.		183.	8 154.3	90		1 186
41	31.	4 26.	4 9	1 69.	7 58,	5 141	108	0 90.	6 191	146.	3 122.8	24	184.	6 154 9			9 187
42					5 59.	1 42	108.	8 91.	3 92	147.	1 123.4	4:	185.	4 155.6	92	223.	7 187
43	32.	9 27	9								8 124.1			1 156.2	93	224.	4 188
44		7 28.			0 60.4 8 61,						6 124.7		180,	9 156.9		225.	
45		5 28.	- 10		-	-11		1 93.		-	4 125.4			7 157-5			_
46		2 29.	9	0 73-	5 61.	146	111.	8 93	9 196	150.	1 126.0	24		4 158.1			7 190
48	30.	8 30.	9	7 74.	1 62.4	47	1112,	4 94.	97	150.	9 126.6	1 4		0 159.4			5 190
49		5 31.		75	8 62.6	40	1114	1 05	8 00	1152	4 127.9	4		7/160.1			3 191
50	138.	32.	100	76.	6 64.3	1150	1114	996	1 200	152	2 128,6			5 160,7			8 192
		1		_							La			Lar		i Der	
-			11			1			1		1.0	11-		Lai	1 01	. Del	1

Difference of Latitude and Departure for 41 Deg. 41

		17	12.0		10	173 -	11	10	100	11.00	inen	in:a	T	Dan	Dift	1 1 -4	10-
Dil:	Lat	De,	Dilt	Lat	Dep	שית	Lat	Dep	Un	Lat	Deb	-	-	Dep	Jin	-	Dep
1	00.8	00 7	51	38.5	33.5	IOI	76.2	66.3	151	114.0	99.0	201	151 7	131.8	251	189 4	164
2	01.5	01.3		39.2		02	77.0	66.9	52	114.7	99.7	02	152.5	132.5	52	190,2	165.
,	02.3	02 0		40.0		03	77.7	67,6		115.5	100.4	03	153.2	133 2	53	190 9	166
3	03.0			40.8		04		68 2	54	116.2	101,0	04	154.0	133.8	54	191.7	166.
7	03.8	12 6 1		41.5		05	79.2	68.9	55	117.0	101.7	05	154 7	134 5	55	192.5	167.
-		-		_		106	80,0		156	117.7	102.2	206	155.5		256	193 2	167
6	04.5			42,3		20.00	80,8				103.0	1		135.8	57	194.0	
7	05.3			43.0		07			57			07	157.0		58	194 7	
8	36.0	05.2		+3.8			81.5		58	119.2	· · ·	09	157.7		59	195 5	11.0
9	36.8			44.5		09	-	71.5	59 60	120.0		10	158.5		60	196 2	
10	27.5	-		45.3		10	83.0	-	-	120,8		-		_	-	-	-
11	08.3	07.2		46.0		111	838		161	121.5		211		1 38.4	261	197.0	
12	09.1	07.9		46.8		12	84.5		62	122.3		12	Ibc.c	20.	62	197.7	
13	09.8	08.5	63	47.5	41.3	13	85.3		63	123.0	105.9	13			63		
14	10.6	09.2	64	48.3	42,0	14	86.0	74,8		113.8		14	161.5		64	199.2	
15	11.3	09.8	65	49.1	12.6	15	86.8	75.4	65	124.5	108.2	15	102.3	141.C	65	200.0	173
16	12.1	10.5	66	49,8	41.3	116	87.5	76.1	160	125 3	108 0	215	163.0	141 7	266	200 8	174,
17	12.8		- 1	50,6		17	88.3		67			17	163.8		67	201 5	
8	13.6			51.3		18		77.4		126.8	110.2	18	164.5	143.0	68	202,3	
19	14.3			52 1		19	89 8		69	127.5	2 011	19	165.3	143 6	69	203.0	176.
10	15.1			52.8		20	90.€		70	128.3		20	166.0	144-3	70	203.8	177.
-			_	_	_			-		129.1	112.2	221	165,8	145.0	171	204.5	177
11	15.8			53.6		22	91.3		72	129 8		22	167.5		72	2053	
12	16.6			54.3			92.8	80.0		130.6	2.00	23	168.9		73	2.60	170
3	17.4		73	55.1	47.9	23	93.6			131.3		24	169 1		74	2.68	
4	18.1		74	55.8	40.3	25		32 0		132.1		25	169.8		75	207,5	
15	18.9	_		_	_			_	-	_		_			-	-	-
26	19.6			57.4		126		82.6	176	132.8			170 6		476	208.3	131
7	20.4			58.1		27		83.3		133.6		27	171.3		77	209.1	
.8	21.1			58.9		28		84.0		134.3			172.8		1 2 3 1	210 6	
9	21.9			59,6		29	97.4		79	135.1		30	173.6	- 1	79	211.3	181
10	22.6	19.7		60.4	-	30	98.1		80	135.8		_			-	-	
31	23.4	20.3	81	61.1	53.1	131	98.9		181	136 6	118.7	231	174-3	1	-81	212 1	
32	24.2	21 0		61.9		32	99.6	86,6		137,4		32	175.1		82	212.8	
33	24 9	21.6	83	62.6	54-4	33	100.4	87.2	83			33	175 8		83	213.0	
14	25.7	22.3		63.4	55.1	34	101.1			138.9		34	176.6		84	214 3	186
35	26.4	23.0	85	64.2	55.8	35	101.9	88.6	85	139.6	121.4	35	177.4	154 1	85	215,1	186,
6	27.2	22.6	86	64,9	56.4	136	102.6	89.2	186	140.4	122.0		178.1		286	215.8	187.
	27.9		87	65.7	57.1	37	103 4		87	141.1	133.7	37	178 9	155,5	87	216,6	188.
. 0	28.7		88	66,4	57.7		104.2		88	141.9	123.3	38	179.6	156.1	88	217.4	188.
	29.4		89	67.2	58.4		104.9			142.6	124.0	39	180.4	156.8	89	218.1	189.
ю		26.2			59.0	40	105.7	91.8		143.4		40	181.1	157.4	90	213.9	190.
11				68,7			106.4			144.2				158.1		2196	
2	30.9	27.6	02		60.4		107.2				125.9	42	182.6	158.7		220,4	
3	3-77	28.2	02		61.0	4.	107.9	02 8		145 7	126.6			159.4		221.1	
4	32.3	28.9	04	70.2		44	108.7	94.6	94	146,4	127.2			160.0			
				71.7	62.		109.4		95		127.9		184,9		95	222.6	
15		29.5				45				-	-			161 4	295	_	-
16	34.7	30,2	96	72.5	63.0	146	110.2	95.8	196	147.9	128.0	140	186	162.0		223.4	
17	35,5	30.8	97	73.2	63.6	47	110.9	90,4		148.7	129.2					224.2	
48	36.2	31.5	98	74.0	64.3		111.7				129.9			162.7		224.9	
49	37.0	32.1	99	74.7	64.9	49	112.5	97.7			130.5		188 -	163.3	99		
50	37.7	32.8	100	75,5	65.6	150	113.2	98.4		16	131,2			164.0		1	
	10	Lat	D:a	0	10	1 0:4	Dep	11 24	IID:0	Den	La	IID if	Dep	Lat	Dift	Dep	1 La

for 49 Deg.

42 Difference of Latitude and Departure for 42 Deg.

1 00.7 00 7 51 37.9 34.1 101 75.0 67.6 151 112.2 101.0 201 149.3 134.5 251 186.5 167.9 201.5 01.3 52 38.6 34.8 02 75.8 68.2 52 112.9 101.7 02 150.1 135.1 52 187.2 168.6 30.2 20.2 0.2 0.5 339.4 35.5 03 76.5 68.9 53 113.7 102.4 03 150.8 135.8 53 187.9 169.3 4 03.0 0.2 7 54 40.1 36.1 04 77.3 69.6 54 114.4 103.0 04 151.5 136.5 54 188.7 169.9 55 03.7 03.3 55 40.9 36.8 05 78.0 70.2 55 115.1 103.7 05 152.3 137.1 55 189.4 170.6 6 04.5 04.0 56 41.6 37.5 106 78.7 70.9 156 115.9 104.4 206 153.0 137.8 256 190.2 171.3 8 05.9 05.4 58 43.1 38.8 08 80.2 72.3 58 117.4 105.7 08 154.5 139.1 58 191.7 172.6 9 06.7 06.0 59 43.8 39.5 09 81.0 72.9 59 118.1 106.4 09 155.3 139.8 59 192.4 173.3 10 07.4 06.7 60 44 6 40.1 10 81.7 73.6 60 118.9 107.0 10 156.0 140.5 60 193.1 173.9 104.6 104.0 10 156.0 140.5 60 193.1 173.9 104.6 104.0 10 156.0 140.5 60 193.1 173.9 104.6 104.0 10 156.0 140.5 60 193.1 173.9 104.6 104.0 10 10 10 10 10 10 10 10 10 10 10 10 10	D. 161	Last	David	kD:	air		Der	D.61	I at 1	Dep	D AI	Lac	Dan	D:A	Lat	Den	Dift	LTati	Don
3 0 1.5 0.1 3.2 3.6 3.4 8 0.2 75.8 68.2 35 11.9 10.1.7 0.2 150.1 135.1 52 187.2 168.5 0.3 0.2 0.3	DIN !	Lat	Deb	-	-1-	Jac	Dep	-	_		-			_		-	Dik.		-
3 0 a. 0 a. 0 5 3 3 3 9.4 3 5.5 0 3 76.5 68.9 63 1 13.7 10.4 0 3 1 50.8 1 35.8 53 1 88.7 1 69.9 6	1	00.7	00 7					12.10			- 1	1	4.50	201	149.3	134.5		186,5	167.9
4 03.0 22.7 544.0.3 16.1 04 77.3 69.6 54 13.4.4 103.0 04 131.5 136.5 54 188.7 169.9 6 03.7 03.3 55 40.9 36.8 05 78.0 70.2 55 115.1 103.7 05 133.1 137.1 55 40.9 36.0 137.5 106 78.7 70.9 156 115.9 103.4 105 133.1 137.1 55 40.9 36.0 137.5 106 78.7 70.9 156 115.9 103.4 105 133.1 137.1 55 40.9 17.1 172.6 10.0 17.0 173.6 173.6 1	2	01.5	01.3	M -							- 1		101.7		-				
\$\frac{5}{6} \frac{0.4}{0.5} \frac{0.5}{0.5} \	2			11				- 1		!		-					71.		
6 04-504-0 56 31.6 37.5 106 78.7 70.9 156 115.0 104.4 206 133.0 137.8 256 190.2 171.3 271.0				11 -															0.0
7 0 5.2 0 4 - 7	5	03.7	03.3	11-	_	10.9	30.8	05		70.2		115.1	103.7	05		_	_	-	-
8 05-9 05-4 58 45-1 38-8 08 80,2 72-3 58 118-1 105-7 08 154-5 139-1 58 191-7 172-6 10 07-4 060-7	6	04.5	04.0					106	78.7		156	115.9	104.4	206	153.0	137.8	256	190,2	171.3
g 06,706. 59,43,8 jg,5 90 81.6 72.9 69 18.1 72.9 69 118.3 106.4 90 15.5,3 jg,8 59 119.4 173.9 11 103.2 07.4 60 14.5 12.2 89.9 86.0 62.46 14.5 12 83.2 74.9 62 120.3 109.7 11 156.7 141.2 83.2 74.9 62 120.3 108.4 11 86.2 77.6 63 14.5,19.3 13 13 158.2 14.6 14.5,19.2 13 83.9 17.5 64 12.3 14.1 159.0 14.1 159.0 14.2 159.0 14.1 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 14.2 159.0 159.0 <td< td=""><td>7</td><td>05.2</td><td>04.7</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td>71.6</td><td></td><td>116.6</td><td>105.0</td><td></td><td></td><td></td><td>57</td><td></td><td></td></td<>	7	05.2	04.7					-		71.6		116.6	105.0				57		
10 07 06 04 06 07 06 04 06 07 07 08 08 08 08 08 08	8	05.9	05.4					08		72.3	58	117.4	105.7	08			58	191.7	172.6
1	9							09		72.9	59	118.1	106.4	09	155.3	139,8	59	192.4	173.3
2	10	07.4	06,7	0	0	14 6	10.1	10	81.7	73.6	60	118.9	107.0	10	156,0	140,5	60	193.1	173.9
12 0.8 0.8 0.8 0.6 0.6 0.6 0.6 0.6 0.7	11	03.2	07.4	6	1	15.3	40.8	111	82.5	74.3	161	119.6	107.7	211	156.7	141.2	261	193.9	174,6
13 09 7 08 7 63 46 49 13 83 9 75 66 40 14 104 09 44 64 47 76 34 84 77 76 36 47 76 14 104	12	2.7		100	2	16.1	41.5	12			62	120.3	108.4	12	157.5	141.8	62		
14 10 10 10 10 10 10 10	13	09.7	08.7	6	3 4	16.8	42,1	13		75.6	63	121,1	109.0	13			63	195.4	
16	14			11 6	4 3	17.5	42.8	14	84.7	76.3	64	121.8	109.7	14	159.0	143.2	64	196.1	176.6
16	15	11.1	10,0	1	15	18.3	43.5	15	85.4	76 9	65	122.6	1104	15	159 7	143 8	65	196.9	177.3
17	16	11.0	10.	1 6	E	19.0	44.2	116	86.2	77.6	166	123.3	111.0	216			266	197.6	
18	17			81									15.7	100					
14 12.7 65 51.3 66.2 19 88.4 79.6 69 125.5 13.1 19 162.7 146.5 70 200.6 180.6 180.6 160.6 180.	18		1								100	124.8	112.4	11 -	1.112				
10	19	-	1					19	88.4		69	125.5	113.1	19	162.7	146.5	69		
11	20	14 9	13.4		- 1												70		
12 16.3 14.7 7 72 53.5 48.2 22 90.6 81.6 72 127.8 115.1 22 164.9 148.5 72 202.8 182.6 13.1 15.1 15.4 73 54.2 48.8 23 91.4 82.3 73 128.5 115.7 23 165.7 149.2 73 202.8 182.6 165.7 75 55.7 50.2 25 92.9 83.6 75 130.0 117.1 25 167.1 150.5 75 204.3 183.6 19.3 17.4 76 56.5 50.8 126 93.6 84.3 176 130.7 117.7 226 167.9 151.2 276 205.0 184.6 17.8 18.1 77 57.2 51.5 27 94.3 85.0 75 130.0 117.1 25 167.1 150.5 75 204.3 183.6 17.5 19.4 79 58.7 52.2 28 95.1 85.6 78 133.2 119.1 28 169.4 152.5 78 206.5 186.3 12.3 10.1 8c 59.4 53.5 30 96.6 87.0 80 133.7 120.4 30 170.9 153.2 99 95.8 86.3 30 12.3 10.1 8c 59.4 53.5 30 96.6 87.0 80 133.7 120.4 30 170.9 153.2 80 207.3 185.4 22.1 83 66.2 34. 85 66.1 55.5 3 35 96.8 89.6 83 133.5 123.1 31.5 12	-	_		-11-	7,	52.7	47.5	121	_		-	127.0	114.4	221		_		201.2	181.0
13 17.1 15.4 73 54.2 48.8 23 91.4 82.3 73 118.5 115.7 23 165.7 149.2 73 202.8 182.6 25 186 16.7 75 55.7 50.2 25 92.9 83.6 75 130.0 117.1 25 167.9 150.5 75 204.3 183.0 193 17.4 76 56.5 50.8 126 93.6 84.3 176 130.7 117.7 226 167.9 151.2 276 205.0 184.6 181 77 57.5 52.2 28 95.1 85.6 77 131.5 118.4 27 168.6 151.9 77 205.8 185.6 78 132.2 119.1 28 169.4 152.9 78 205.0 184.2 208.8 185.6 79 133.5 119.7 226 168.6 151.9 77 205.8 185.2 77 131.5 28 169.4 152.9 78 206.5 184.2 20.7 186.3																	2030	1000	1 - 3
24 17.8 16.1 74 55 0 49.5 24 92.1 83.0 74 129 3 116.4 24 166.4 149.9 74 203.5 183.2 26 19.3 17.4 76 56.5 50.8 126 93.6 84.3 176 130.7 117.1 226 167.1 150.5 75 205.8 184.0 28 20.8 18.7.7 75 57.2 21.5 27 94.3 85.0 77 131.5 118.4 27 168.6 151.9 72 205.8 185.6 77 131.5 118.4 27 168.6 151.9 72 205.8 185.6 77 131.5 118.4 23 169.4 152.5 78 205.8 185.6 77 131.5 118.4 23 169.4 152.5 78 205.8 185.6 77 131.5 118.4 23 169.4 152.5 78 205.8 185.6 77 131.5 118.4 23.1 170.1 153.2 207.3 186.6 208.7 207.3 186.7	17.75				- 3	54.2	48.8				11								
25 18 6 16.7 75 55.7 50.2 25 92.9 83.6 75 130.0 117.1 25 167.1 150.5 75 204.3 184.6 26 19.3 17.4 76 56.5 50.8 126 93.6 84.3 176 130.7 117.7 226 167.9 151.2 276 205.0 184.6 28 20.8 18.7 78 57.9 52.2 28 95.1 85.6 78 132.2 119.7 29 168.6 151.9 77 205.8 185.7 29 95.8 86.3 79 133.0 119.7 29 170.1 153.2 79 207.3 186.7 79 207.3 186.7 79 207.3 186.7 79 207.3 186.7 79 207.3 186.7 79 207.3 186.7 79 207.3 186.7 207.3 186.7 207.3 186.7 207.3 186.7 207.3	-	1 .		- 11	-										1 -2 "				
26				71 3															
27 20.1 18.1 77 57.2 51.5 27 94.3 85.0 77 131.5 118.4 27 168.6 151.9 77 205.8 185.2 28 20.8 18.7 78 57.9 52.2 28 95.1 85.6 78 132.2 119.1 28 169.4 152.5 78 206.5 186.6 29 21.5 19.4; 79 58.7 52.9 2 95.8 86.3 79 133.0 119.7 29 170.1 153.2 79 20.73 186.6 21.3 10.1 8c 59.4 53.5 30 96.6 87.0 80 133.7 120.4 30 170.9 153.9 80 187.3 121.4 82 60.9 54.9 32 98.1 88.3 24.5 22.1 83 61.7 55.5 33 98.8 89.0 83 135.9 122.4 33 173.1 155.9 83 210.2 189.3 125.3 22.7 84 62.4 56.2 34 99.5 89.6 84 136.7 123.1 34 173.8 156.5 84 211.0 190.3 153.9 122.4 153.2 123.1 34 173.8 156.5 84 111.0 190.3 153.9 122.4 153.2 123.1 34 173.8 156.5 84 111.0 190.3 153.9 122.4 153.2 123.1 34 173.8 156.5 84 111.0 190.3 153.9 122.4 153.2 123.1 34 173.8 156.5 84 111.0 190.3 153.9 122.4 153.2 123.1 34 173.8 156.5 84 111.0 190.3 153.9 122.4 153.2 123.1 34 173.8 156.5 84 111.0 190.3 153.9 122.4 153.1 153.9 122.4 155.2		_	-	-11-	-	_	_	-						-					
28 20.8 18.7 78 57.9 52.2 28 95.1 85.6 78 132.2 119.1 28 169.4 152.5 78 206.5 186.6 30 123.3 10.1 8c 59.4 53.5 30 96.6 87.0 80 133.7 120.4 30 170.9 153.9 80 208.0 187.3 123.8 11.4 82 60.9 54.9 32 98.1 88.3 82 135.2 121.8 32 172.3 155.9 281 209.5 188.3 124.5 22.1 33 125.2 22.1 34.5 22.1 34.5 22.1 35.3 22.7 35 26.0 23.4 85 63.1 56.9 35 100.3 90.3 85 137.4 123.8 35 174.6 157.5 85 211.7 190.3 36.4 32.5 24.8 88.6 58.2 37 101.8 91.7 37 27.5 24.8 88 65.4 58.2 37 101.8 91.7 37 125.8 38 174.6 157.2 85 211.7 190.3 38 22.7 23.8 23.2 23.4 23.8 23.2 23.4 23.8 23.2 23.4 23.8 23.2 23.3 23.2 23.8 23.2 23.3 23.2 23.3 23.2 23.3 23.3 23.3 23.2 23.3 2	1			. 11			1-												
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Din.	_	-	-			-	-		-			-			_		
1	00,7	100		36.7		101	72,6		-	108.6		201	144.6			180.5	174,3
2		01,4	- 4	37.4		02	73.4	70.8	-	, ,	105.0	02	145.3		52		175.0
3	02.2			38.1	36.8	03	74.1	71.5	33		106.3			141.0		182.0	
4	02.9					04	74.8	72.3	2.1	111.5		04	147.5			182.7	
5	-	03.5	55				75.5	_					_				177.1
6		04,2	56			106	76.2	73.6	-	112.2			148.2			1841	
1 7		05.6	57	41,0		03	77.0	74-3	-	112.9	109,7	08	148.9			184.9 185.6	
9		66.3	59	1000	41.0	09	77-7	75.0	59		110,4	09				186.3	
10	4 -	06.9	60	43.2	41.7	10	79.1	76.4	60		111.1	10	151.1		60		180,6
111	07.0	07.6	61	-	42.4	111	79,8	77.3	161	_	111,8	211	151.8			_	181,3
112		08,3	62	1	43.1	12	80,6	77 8	62	116.5		12		147.3			182.0
13	09.4	-	63	45.3	0	13	81.3	78.5	63	ATA IN	113.2	13		147.9		189.2	
14		09.7		46.0		14	82.0	79.2	64	118.0	113,9	14		148.6		189 9	
15	10.8	10.4	65	46.8	45.1	15	82,7	79.9	65	118.7	114.6	15	154.6	149.3	65		184.1
16	11.0	11.1	66	47.5	45.8	116	83.4	80.6	166	119.4	115,3	216	155.4	150,0		191.3	184.8
17		8.11	67	1		17	84.2	813	67		116,0	17	156.1	150.7	67	192.1	185.5
18	12.9	12.5	68		47.2	18	84.9	82,0	68	120.8	116.7	18	156.8	151.4	68	192.8	
19		13.2	11	1	47.9	19	85.6	82.7	69		117,4		157-5	1 -	69		186.8
20	14.4	139	70	50.4	43.6	20	86.3	83.4			118.1	26	158.2	152.8	70	_	187.5
21	1 -	1 14,6	71	51.1	49.3	121	87.0				118.8		1	153,5	271		188.2
22	1 3			10	1-	2.8	87.8	84.7			119.5	11		154.2	2 6		188.9
23		5 16.0	11		10	23	88.5		11		120.2	11	10	154.9			189.6
24	17.	3 16.7	11	1	1		89.2	86.8		1	120.9			155.6	6.6		190.3
25	_				-			-		-		11-	-	-			_
26		7 18.1				23	90 6			126.6				31	77		191,7
27		1 19.4			53.5	11 -	92,1	88.9	11 - 2		123.0		1	157,7	78		192,4
29	-	9 20,1	1		54.9	11	92.8	89.6	11		8 124.	11		159.1	79		193.8
30		6 20,8	. 11 0				93 5		11 0	115 115			1 - 6				194.5
31		3 21.	0		56.	-	94.2	-		130.	135.7	231	166,2	160.4	281	-	195.2
32		0 22.5				11			0 -		1	11 -	100	161.1	82		195.9
33		7 22.0			1	11			11 0 -	131.	6 127.	33		161.8	11 -		196.6
34		5 23.6	84		4 58,	34					4 127.			162.5	84		197.3
35	25.	2 24.	85	61.	1 59.0		97-1	93.8	85				169.0	163.2	85	205.0	198.0
36		9 25.0			1 20 1	11					8 129.			163.9		205.7	198.7
- 37	26.	6 25.	87	62.	6 60.4	37	98.5	95.2	87		5 129.	37		164.6		206.4	199,3
38		3 26.4			61.	38	99.3	95.9	88	135.	2 130.	38	171.2	165.3	88		200.0
39		1 27,			61.8		100.7	1	00	135.	9 131.	39	171.9	166.0	1 00	207,9	200.7
40	-	8 27.1		-	62.			-			7 132,0					-	201.4
41		5 28.			63.2	141	101.4	97.5	191	137,	4 132.	41	173.4	167.4	291		202.1
42		2 29.2			63.9		102.9		92	128	8 134.	1 4	174.5	168.8	93		202.8
43		9 29.6			6 65.3			100.0	94	120.	5 134.	8 44	175.	169.9	94		204,2
45		4 31.	18		66.0			100.7			3 135,4			170.2	95		204.9
46					66.7				. 1/					170.9			205.6
47	,	32.6		60.8	67.4	47	105.7	102.1	97	141.	136.	47	177.	171.6	97		206.9
48	34.	5 33.3	1 98	70.5	68.1	48	106,5	102.8	98	142.4	1 37.	48	178.4	172.3	98	214.4	1207.0
49	35.	2 34.0	99	71.2	68.8	49	107.2	103.5	99	143.1	138.2	49	179.1	173.0	99	215.	1 207.7
50	36.0	33.7	100	71.9	69.5	150	107.9	104.2	200	143.9	138.0	250	179.	173.6	300	215.8	208.4
Die	Le										Lat				Diff		
-			11					1			11. 12.14			100			-

) (1	Lat	De	Illo	Diffe	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Ditt	Lat.	Dep	Dift	Lat	Dep
-	_	-	-11-	_	36.1		101	71.4	71.4	151	106 8	106.2		142.1	142.1	251	177.5	-
1	00.7	1		51	36.8		02	72.1	72.1		107,5	107.0	02		142 8	52	178.2	
2	01.4		-11	_		200	03	72.8	72.8	53	108.2		03		143.5	53	178.9	
3	02.1	1	~!!		37·5 38.2		04	73.5	73 5		108.9		04		144.2	54	179.6	
4	02.8	0.1	-11		38.9		05	74.2	74.2	55		109.6	05	144.9		55	180.3	188.
_5	03.5	03.	- 11	1	_	30.9			_	-			_	-				
6	04.2			- 1	39.6	39.0	100	74.9	74.9	-	110.3	THE STATE OF	206		145.7		181 0	
7	04.9			21	40.3		07	75.7	75.7	57	111.0		07	2. 20. 2	146.4	57	181.7	
8	05.7	1 0	- 11	- 1		41.0	08	70.4	76.4		111.7	San Branch B.	08		147.1		182.4	
9	00.4	06.	4	2-1	41,7	41.7	09	77.3	77.1	2 1	112.4	112.4	09		147.8		183.1	
10	07.1	07.	2	00	42.4	42.4	10	77.8	77.8	-	113.1	-	10	148.5	148.5	- 00	183.8	
11	07.8			61	43.1	43.1	11:	78.5	78.5	161	113.8	113.8	211	149 2	149.2	261		
12	08 5	80	5	62	43.8	43.8	12	79.2	79.2		114.5	1145	12		149.9	62	185.3	185.
13	09.2	09,	2	63	44.5	44.5	13	79 9	79.9		115.3				150.6		185,0	
14	09.9	09,	9		45.3		14	80.6	80.6		116,0				151.3		186.7	
15	10,6	10,	c	65	40.0	45.0	15	81.3	81.3	05	116.7	110.7	15	152.0	152.0	05	187.4	187.
16	11.3	II.	5	66	46.7	46.7	116	82.0	82.0	166	117.4	117,4	216	152.7	152.7		1.88.1	
17	12.0	12.	all	67	47.4	47.4	17	82.7	82.7	67	118.1	118.1	17	153.4	153.4	67	188.8	188.
18	12.7	12.	7		48.1		18	834	83.4	65	118.8	118.8	18		154.1		189.5	189.
19	13.4	1 13.	411	69	48,8	48.8	19	84.1	84.1	69	119.5	119.5	19		154.8		190.2	190
20	14.1	14	1	70	49,5	49.5	20	848	84,8	70	120.2	120.2	20	155.6	155.6	70	190.9	190
21	14.5	14	8	71		50.2	121	85.6	85.6	171	120.0	120.6	221	156.3	156.3	271	191.6	LOI
22		6 15	- 11	72		509	22	86.3	86 3	72	121,6	1 2	11		157.0	M	192.3	
23	1 2	3 16	- 11	73		51.6	23	87.0	87.c	73	122.3	1			157 7	11	1930	
24	17		~11	74	-	52.3	24	87.7	87.7	74		123 0	11	0	158.4	11	193.7	193
25	1	1 .	- 11	75	53 0		25	83,4	88.4	75		123.7	11		159.1	41	194 4	
-	-	-	-11	76	-	-	126	89,1	-			100	1	_	159.8	-		-
26	The Cart		- 11		53-7		11	89.8	89.1	176		124.4	11		160.5			
27		-	-11	77		55.2	27	90.5	89,8	77 78	-	125.9			161,2		195.9	
	1-	8 19		78		55.9		91.2	99.5	11	16 6	126.6			161.9	11	1	
29		5 20 2 2 I	-11	80	56.6			91.9	91.9	11 6		127.3	11	1 .	162.6	11 0	1980	
30	-	-	-1	-	-	-		_	-	-	-			_	-	-		-
31		-	311	81	57.3			92.6	92.6	11 0		128,0			163 3		198.7	
32				82	58.0	1 -		93.3	93,3		128.7	1		1	164.0	0.2	199.4	
33	1	3 23		83	1-	-	11	94 0		11 -	1	129 4	.11		104.7	11 0	1	1
34		0 24		84	59.4	10	11	94.7	94.7	11 -	130.1			1	105.5	11 -		1 - 4 - 1
35		7 24	,7	85	-	1 00.1	35	95.5	95.5		-	130.	-		166.2	-		_
36	25.	5 25	.5	86	1000	8 60.8		96.2	96.2		131.5		- 11				202.2	
37		2 26		87	61.	61.5	37	96.9			1 32.2				167.6	87	202.9	202
38	26.	9 26	.9	88	62.2	62.	38	97,6	97.9	88	132.9	132.	38	168.	168.	88	203.6	203
39		6 27		189	62.0	62.9	39	98.3			133.6		39	169.0	169.0	89	204.3	204
40	23.	3 28	.3	90	63.6	6 63 6	40	99.0	99.0	90	134.	134.	3 40	169.	169,7	90	205.1	205
41	29.	0 29	0.0	91	64.	3 64,	141	99.7	99.7	191	135.1	135.	1 241	170.	4 170.4	291	205.8	205
42		7 29		92	65.1	1 65.1	42	100.4	100.4	92	135.8	135.	8 42	171.	171.	1 92	206.5	206
4:		4 30		93	65,	8 65.8	43	IOL.	101.1	93	136.	1 36.	5 43	171	8 171.	93	207.2	207
44		1 31		94	66.	5 66.	44	101.8	101.8	94	137.2	137.	2 44	172.	5 172.	5 94	207.9	207
		8 31	.8		67.	2 67.					137.						203.6	
45	5 22	5 32		-		9 67,	- 11										209.	
41		2 33				6 68	6 47	102.6	102.0	07	139.	3 130.	3 4	174	6 174	6 07	210.0	210
4		9 3		08	60	2 60	3 49	I DA	104	6 08	140	0 140.	0 48				210.7	
4						3 70.	A	105	105.	1 00	140.	7 140.	7 40	176.	1 176	1 00	211.4	211
5		4 3		100	70.	7 70	7 1 50	106	106.	1 200	141	4 141.	4 250	176.	8 176	8 200	212.	21:
		- 3		5	مرام			a D	La	1	n) D	To	- 5	Dan	La	-	t Dep	
																10 (7 1		

Number for the Readier finding the Courses in the foregoing Tables of Difference of Latitude and Departure.

Dift. :	and I	Diff. of	Lat.		Dift	and	Depar	ture	Diff.	of La	t. and	Dep
Num	Deg.	Num	Deg.		Num	Deg.	Num	Deg.			Num	
1000	1	17	89		17	• 1	1000	89	2	1	5882	89
909	2	35	88		35	2	999	88	3	2	2855	88
908	3	52	87	- 1	52	3	998	87	5	3	1908	87
997	4	70	86		70	4	997	86	7	4	1432	86
996		87	85		87	5	996	85	9		1145	85
995	5	105	84		105	6	995	84	10	5	950	84
993	7	122	83		122	7	993	83	12	7	816	83
990	8	139	82		139	8	990	82	14	8	711	82
988	9	156	81		156	9	988	81	16	9	632	81
985	10	173	80		173	10	985	80	18	0	568	80
982	11	191	79		191	11	982	79	19	11	515	79
978	12	208	78		208	12	978	78	21	12	470	78
974	13	225	77		225	13	974	77	23	13	433	77
970	14	242	76		242	14.	970	76	25	14	401	76
966	15	259	75		259	15	966	75	. 27	15	373	7.5
961	16	276	74		276	16	961	74	29	16	349	74
956	17	292	73		292	17	956	73	30	17	328	73
951	18	309	72		309	18	951	72	32	18	308	72
945	19	326	71		326	19	945	71	34	19	290	71
940	20	342	70		342	20	940	70	36	20	275	70
934	21	358	69		358	21	934	69	38	21	260	69
927	22	375	68	100	375	22	927	63	40	22	248	68
921	23	391	67		391	23	921	67	42	23	230	67
914	24	407	66	1	407	24	914	66	45	24	225	66
906	25	423	65		423	25	906		47	25	214	65
899	26	438	04		438	26	899	64	49	26	205	64
891	27	454	63		454	27	891	63	51	27	196	63
883	28	470	62		470	28	883	62	53	28	188	62
875	29	485	61		485	29	875	61	55	29	180	61
866	30	500	60	101	500	30	866	60	58	30	173	60
857	31	515	59		515	31	857	59	60	31	166	59
848	32	530	59		530	32	848	8	62	32	160	58
839 829 819	33	545			545	33	839 825	57 56 55	65 67	33	154	57
829	34	559	57 56		559	34	825	55	67	34	154	56
819	35	574	55		574	35	819	55	70	35	143	55
809	36	588	54	777	588	36	800	54	73	36	138	54
799	37	602	53		602	37	79	53	75	37	133	53
788	38	616	52		616	38	79 788	52	78	38	128	52
777	39	629	51		629	39	777 766	51	18	39	123	51
766	40	643	50		643	40	76t	50	84	40	119	50
755	41	656 669	49		6;6	41	755	49	87	41	115	-
743	42	669	48		656 669	42	743	49 48	90	42	III	48
731	43	682	47		68z	43	731	47	93	43	107	47
719	44	695	46	1	695	44	719	46	93 96	44	103	46
719	45	707	45		707	45	707		1100	45	100	45

The Use of the Tables of Difference of LATITUDE and DEPARTURE, in Working any of the Cases of PLAIN-SAILING.

N these Tables the Course if less than 4 Points, or 45 Degrees, will be found at the Top of the Tables; but if it is more than 4 Points, or 45 Degrees, it will be found at the Bottom of the Tables; and on every Side there are Six Columns for the Distances, mark'd Dist. which contain 50 Miles in each Column, the First beginning at 1, and ending at 50; the Second beginning at 51, and ending at 100, and so on to 300 Miles Distance; and to each of these Columns of Distance there belongs two other Columns, shewing the Difference of Latitude and Departure to any of them Distances, mark'd Lat. and Dep. in which you are to observe, that if your Course be found at the Top of the Tables, then you are to take the Difference of Latitude and Departure as they are mark'd at Top; but if your Course be found at Bottom, then you must take them as they are mark'd at Bottom.

Note, In any Case where the Course is given in Points, half Points, or Quarters, you must make use of the following Tables of Difference of Latitude and Departure, which are calculated for Points, &c. but where the Course is given in Degrees, or where it is not given at all, you must make use of the foregoing Tables of Difference of Latitude

and Departure.

Plain Sailing, Case the First.

Course and Distance being given, to find the Difference of Latitude and Departure.

R U L E.

Find your Course as before directed, and look in some of the Distance Columns belonging to that Course, for your Distance, the Difference of Latitude and Departure answering to that Distance, will be the Difference of Latitude and Departure required.

Example

EXAMPLE I.

A Ship sails NNE. 136 Miles, I demand her Difference of Latitude and Departure.

Having found my Course, which is 2 Points in the Table for Points, I find my Distance 136 in the third Column for Distances, and right against that, I find 125.7 Tenths for my Difference of

Latitude, and 52.0 Tenths for my Departure.

Note, In all Cases whatsoever, if the given Side or Sides be in Miles, then the Sides found by the Table, will also be in Miles; but if the given Side or Sides be Leagues, then the Sides found will also be Leagues.

Plain-Sailing, Case the Second.

Course and Difference of Latitude being given, to find the Distance and Departure.

RULE.

Find your Course as before, then look in some of the Difference of Latitude Columns belonging to that Course, for your Difference of Latitude, the Distance and Departure answering to that Difference of Latitude, will be the Distance and Departure required.

EXAMPLE.

A Ship sails S. 48 Degrees 00 Minutes E. till her Difference of Latitude he 164 Leagues, I demand her Distance and Departure?

Having found my Course 48 Degrees at the Bottom of the Tables, I look in some of the Columns mark'd Latitude at Bottom, for the nearest I can find to my Difference of Latitude, which is 163.9, and answering to that, I find for my Distance 245 Leagues, and for my Departure 182.0 Leagues.

Plain-Sailing, Case the Third.

Course and Departure being given, to find the Distance and Difference of Latitude.

RULE.

Find your Course as before, then look in some of the Departure Columns belonging to that Course, for your Departure, the Distance and Difference of Latitude answering to that Departure, will be the Distance and Difference of Latitude required.

EXAMPLE.

A Ship sails SW. by S. till ber Departure be 165 Miles: I demand ber Distance and Difference of Latitude.

Having found the Course, which is 2 Points at the Top of the Table for Points, I look in some of the Columns mark'd Dep. at Top, for the nearest I can find to my Departure, which is 165.0, and answering to that I find my Distance 297 Miles, and for my Difference of Latitude 246.9 Miles.

Note, In any Case where the given Side is too big to be found in the Tables, then divide it by 2, 3, 4, or any other Number that will make it small enough to be found, and then the required Sides, when found, must be multiplied by the same Number; but the Course must never be multiplied nor divided.

Plain Sailing, Case the Fourth.

Distance and Difference of Latitude being given, to find the Course and Departure.

RULE.

Put two Cyphers to the Difference of Latitude, and divide it by the Distance (without taking any Notice of the Comma that stands between the Miles and Tenths) and note the Quotient: Then look in the Table of Numbers (at the end of the Tables of Difference of Latitude and Departure) in the Columns belonging to Distance and Difference of Latitude, for the nearest Number to that Quotient, the Degrees answering to that Number will be the Course. Then to find the Departure, proceed as in Case the first. But here you are to obferve, that in all Cases where the Course is to be found by the Table of Numbers, the Difference of Latitude and Departure are supposed always to be in Miles and Tenths, as for Example, 112,4 Tenths, 907,2 Tenths, &c. so that if at any Time either of them should be given in Miles without Tenths, as 117, 124, &c. You are then to put a Cypher to them to supply the Place of Tenths, and call them 117,0 Tenths, 124,0 Tenths, &c. and then put two Cyphers more according to your other Rules, to find the Number for the Course.

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EXAMPLE.

A Ship sails between the North and West, till her Distance is 276 Miles, and her Difference of Latitude 211.4 Miles, I demand her Course and Departure.

Having put two Cyphers to the Difference of Latitude, which makes it 211400, I divide it by the Diffance 276, and find the Quotient be 766 nearly, then I look in the Table of Numbers (under Diff. and Diff. of Lat.) for the nearest to it which is 766, against which I find 40 Degrees for my Course, and with that Course and my given Distance, I find my Departure to be 177.4 Miles, (by Case the first.)

Plain Sailing, Case the Fifth.

Distance and Departure being given, to find the Course and Difference of Latitude.

RULE.

Put two Cyphers to the Departure, then divide it by Distance, and look in the Table of Numbers, in the Columns belonging to Distance and Departure, for the nearest Number to the Quotient; the Degrees answering to that Number will be the Course, and then the Difference of Latitude may be found, (by Case the First.)

EXAMPLE.

A Ship sails between the South and East, till her Distance is 546 Miles, and her Departure 412 Miles, I demand her Course and the Difference of Latitude.

Having put a Cypher to my Departure to supply the Place of Tenths, which makes it 412,0 and then two more Cyphers according to the Rule for this Case, which makes it 412000, I divide it by the Distance 546, and find the Quotient to be 754, against the nearest to which, viz. 755 in the Table of Numbers under Dist. and Dep. I find 49 Degrees for my Course; and with that Course and my Distance (divided by 2, because it is too big to be found in the Tables) I find a Difference of Latitude 179,1 (by Case the First) which multiplied by 2, because the Distance was divided by 2, gives 358,2 for my whole Difference of Latitude.

Plain

Plain Sailing, Case the Sixth.

Difference of Latitude and Departure being given, to find the Course and Distance.

R U L E.

Put two Cyphers to the Departure, and divide it by the Difference of Latitude, then look in the Table of Numbers, in the Columns belonging to Difference of Latitude and Departure, for the nearest Number to the Quotient, the Degrees answering to that Number will be the Course. Then to find the Distance proceed as in Case the 2d, or 3d.

EXAMPLE.

A Ship sails between the North and West, till her Difference of Latitude is 184 Miles, and her Departure 115 Miles, I demand her Course and Distance.

Having supplied the Place of Tenths in both these Sides, which makes them 184.0, and 115.0, I then put two Cyphers to the Departure which makes it 115000, and divide it by the Difference of Latitude 1840, and find the Quotient to be 62; against which in the Table of Numbers, under Difference of Latitude and Departure, I find 32 Degrees for my Course, and with that Course, and my Difference of Latitude, (by Case the Second) or with that Course, and my Departure (by Case the Third) I find my Distance to be 217 Miles.

Note, By these foregoing Rules for Plain Sailing, you may work any Case in Traverse, Mercator, Parallel and Middle Latitude, only by supposing the Names of the Sides and Angles in Mercator, Parallel and Middle Latitude, to be changed into the Sides and Angles they represent in Plain Sailing.

TRAVERSE.

The several Courses and Distances a Ship sails being given, to find what direct Course and Distance she has made good, and her Difference of Latude and Departure.

RULE.

Make a Table as on the following Side, and set down in it your several Courses and Distances, then by the Rule, for Case the First of Plain Sailing, find the Difference of Latitude and Departure to each

of the Courses and Distances, and set them down in the Table, opposite to the Courses they belong to, taking Notice that the Disserence of Latitude must always be set in the North Column, if the Course be Northerly, and in the South Column if the Course be Southerly; and the Departure must always be put in the East Column, if the Course be Easterly, and in the West Column, if it be Westerly.

Then add up all your Columns of North, South, East and West separately, and set down their respective Sums at the Bottom of each Column, and if you have but one Column of Northing or Southing, and but one of Easting or Westing, then their Sums will be the Difference of Latitude and Departure of the same Name with the Column they stand under; that is, the Difference of Latitude will be Northerly, if it stands under the North Column; and the Departure

Easterly, if it stands under the East Column, &c.

But if you have Numbers in all the Columns of North, South, East, and West, then take the Sums of the North and South Columns, and subtract the lesser from the greater, the Remainder will be the Disserence of Latitude, of the same Name with the greater of them: Also do the same with the Sums of the East and West Columns for the Departure; then with that Disserence of Latitude and Departure, find the Course and Distance, as in Case the Sixth, of Plain Sailing.

EXAMPLE.

A Ship sails the following Courses, viz. SSW. 54 Miles, W. by S. 39, NW. by N. 40, NE. by E 69, and NNW. 60 Miles; I demand her direct Course, Distance, Difference of Latitude and Departure.

h .		Diff. o	f Lat.	Dep	arture
Courie:	Dift.	North	South	Eaft	Wett.
SSW	-54		49.0		20.7
W by S	39		7.6		38.2
NW by N	40	33.3			22.2
NE by E	69	38.3		57-4	
NNW	60	C\$.4			23.0
		127 0	57 5	57.4	104.1
		57-5			57-4
diff. Lat	N.h	69.5	DepW	erly.	46.7

Note, 'Tis by this Method that the Difference of Latitude and Departure are found in working any Days Work at Sea; and from the Difference of Latitude and Departure so found, we find the Course, Distance and Latitude by Dead - Reckoning, Meridian Distance and Longitude made; all which will be further explained in the Rules for keeping a Journal.

Course N. 34 00 W. Distance 84 Miles.

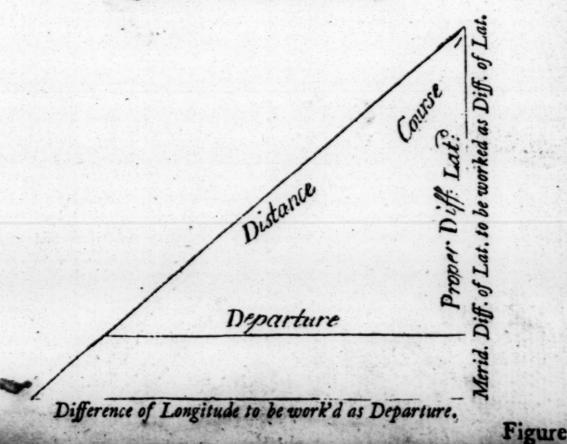
To Work any Right-angled Triangle, by the foregoing Rules for PLAIN SAILING.

In all Right-angled Triangles that are to be worked by the Tables, you are to suppose four Things, viz. Course, Distance, Difference of Latitude and Departure, two of which must always be given to find the other two: Then as these Rules are wrote for working of Plain Sailing, if you would work any other Sailing by them, as Mercator, Parallel, Middle Latitude, or any other Right-angled Triangle, you must suppose the Sides and Angles of that Triangle to be called by the same Name that the Sides and Angles they represent in Plain Sailing are called by, and then work them as if it was a Case in Plain Sailing.

As for Example. The North and South Line, is any Right-angled Triangle (but whatever Name it is called in the Sailing it belongs to) must be work'd as if it was Difference of La itude in *Plain Sailing*: The East and West Line as Departure; the long Side as Distance, and the Angle opposite to the East and West Line as Course. For

Example see the following Figures.

Figure for Mercator's Sailing.



Mercator's Sailing, Case the First.

The Latitudes and Longitudes of any two Places being given, to find what Course and Distance a Ship must Sail from one Place to the other.

RULE.

Having the two Latitudes and two Longitudes given; find the proper Difference of Latitude, the Meridional Difference of Latitude, and the Difference of Longitude, (as by the Rules for that Purpose) then with the Meridional Difference of Latitude, and the Difference of Longitude (taken as Difference of Latitude and Departure) find the Course by the Sixth Case of Plain Sailing, and with that Course, and the proper Difference of Latitude, find the Distance by Case the Second of Plain Sailing.

EXAMPLE.

What Course and Distance must a Ship sail from a Place in Latitude 50.00 North, and Longitude, 03.10 West, to a Place in Latitude of 17.10 North, and Longitude 59.11 West?

Having put two Cyphers to the Difference of Longitude, and divided it by the Meridional Difference of Latitude, I find the Quotient to be 138, against which in the Table of Numbers (under Difference of Latitude and Departure) I find 54 Degrees for my Course; and with that Course, and my proper Difference of Latitude, I find my Distance to be 3348 Miles.

The Course being thus found in Degrees, I want in the next Place to know what Quarter of the Compass it is in, that is, whether it be so many Degrees from the North towards the East, or from the North towards the West, &c. to do which take the following Rule.

If you are to sail from a greater North Latitude to a less, or from North Latitude into South; or from a lesser South Latitude to a greater, then you must sail to the Southward.

But if you are to fail from a greater South Latitude to a leffer, or from South Latitude into North; or from a lefs North Latitude to a greater, you must fail to the Northward.

If you are to sail from a Greater East Longitude to a Lesser, or from a Lesser West Longitude to a Greater; or from East I ongitude into West, you must sail to the Westward, except the Difference of Longitude be more than 180 Degrees, and then you must sail to the Eastward.

But if you are to go from a Greater West Longitude to a Lesser, or from a lesser East Longitude to a greater, or from West Longitude into East, you must sail to the Eastward, except your Difference of Longitude be more than 180 Degrees, and then you must sail to the Westward.

EXAMPLE.

In the foregoing Case of Mercator's Sailing, I find by the two Latit. that I am bound from a Greater North Latitude to a Lesser, viz. from 50.00 N. to 17.10 N. then by the Rule I must sail to the Southward; and I find by the two Longitudes, that I am bound from a Lesser West Longitude to a Greater, viz. from 3.10 West to 59.11 West, then by that Rule I am to go to the Westward, therefore my Course will be South 54.00 West, or SW. 3 West nearest.

This first Case of Mercator, being the Case that is always made use of, to find the Course and Distance from Place to Place, or to find the Bearing and Distance of any Place, from the Ship at any Time, I have set down the Work of it at large, and shall leave the other Case for the Reader to exercise himself with, by working them by the Rules

already given him.

A Table of the Angles which every Point and Quarter Point of the Compass makes with the Meridian.

1	D M	D M	D M	D M
1 4	2 49	2 2 25 19	4 47 49 64	70 19
1 2	5 37	2 2 28 07	41 50 38 61	
34	8 26	23/4 30 56	44 53 26 63	75 56
1	11 15	3 38 45	5 56 15 7	78 45
14	14 04	3 4 36 34	5 5 59 04 7 4	
11	16 52	3 39 22	51 61 53 71	
134	19 41	3 4 42 11	53 6441 73	87 11
2.	22 30	4 45 00	6 6 730 8	90 00

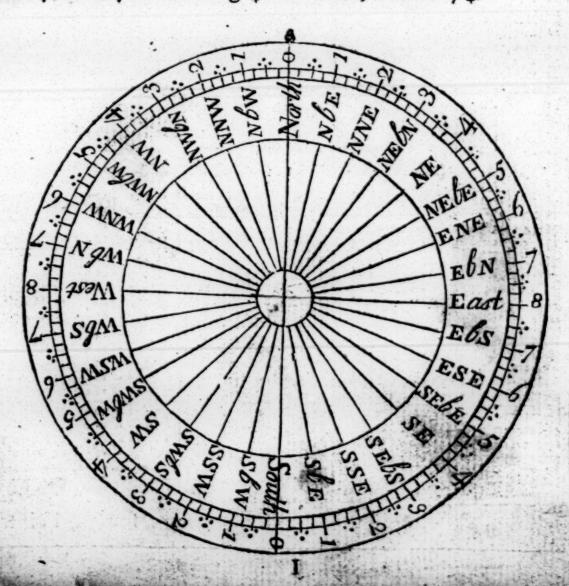
The Use of this Table is to turn Points into Degrees, or Degrees into Points, as follows; Suppose I would know how many Degrees 5 Points are, then I look for 5 Points, and against it I find 56 Deg. 15 Min. or if I would know how many Points 42 Deg. 17 Min. are, I look for the nearest to it, which is 42 Deg. 11 Min. and against that stands 33 Points.

The Courses and Distances being set down in a Traverse Table, as in Page (52) it will be found necessary for the ready-looking them out in the Table of Disserence of Latitude and Departure, to know what Angles they make with the Meridian, (or as we commonly say) to know how many Points there are, for which Reason I have here given the Figure of the Mariner's Compass, which is to be used as follows.

Example 1st. Suppose I would know how many Points I must look out for in the Table of Difference of Latitude and Departure, for a SW. by W. Course.

Look in the Figure below, and against the Point mark'd with SW. by W. you will see the Figure 5, which shews that you must look out for 5 Points.

Example 2d. How many Points is E. by N. \(\frac{3}{4}\) E. against E. by N. I find 7, and my Course being \(\frac{3}{4}\) Point more, it makes 7\(\frac{3}{4}\).



58 Difference of Latitude and Departure for ‡ Point.

1		-	·D:		-	0.0		-	-50		. =						
חעו	Lat	Dep	Dir	Lat	Del	Dift	Lat	Dep	Dift	La	Dep	Dift	Lat.	Dej.	Ditt	Lat	Dep
1	01.0	00.0	51	50.0	02.5	101	100.9	05.0	151	1 50.8	07.4	201	200.8	09 9	7.51	200	-
2	02.0	00.1	52		02.6	02	101.0	05.0	52	151.8			201 8	09,9		250.7	
3	01.0	00.1	53		02.6	03	102.9	05.1	53	152.8		03	202.8	10 0	52	251.7	
1 4		00.2	54		02.7	04	103.9	05.1	54	153.8			203.8	10.0	53	252.7	
1	05.0	1	55	54 9		05	104.9	05.2	55	- 0			204.8		54	253.7	
1 -3	_			-	-			_					_	10.1	55	254 7	12.5
6		00,3	56	55,9		106	105.9	05.2	156	155.8	07.7	206	205.8	10,1	256	255-7	12.6
7		00.3	57		02.8	07	106.9	05.3	57	156.8	07.7	07	206.8	10.2	57	256.7	
8		00.4	58		02.8	08	107,9	05.3	58	157.8	07.8	08	207.8	10.2	58	257.7	12.7
9		00,4	59		02.9	09	108.9	05.4	59	158.8	07.8	09	208.7	10.3	59	258.7	12.7
10	10,0	00.5	60	59 9	02.9	10	109.9	05.4	60	159.8	07.9	10	209,7	10.3	60	259.7	12,8
11	11.0	00.5	61	60.0	03 0	111	110.9	05.5	161	160.8	07.9	211	210,7	10.4	261	260.7	_
12	1. "	00.6	62		03.0	12	111.9	05.5	62	161.8	08.0		211.7	10.4			12.8
13		00.6	63		03,1	13	112.0	05.5	63	162.8	08.0		212.7	10.5			12.9
14		00.7	64		03.1	14	113.9	05.6	64	163.8	08.1					262.7	
	2.70	00.7	65	64.9		15	114.9	05.6	65	164.8		14	213.7	10.5			13.0
15	-	-	ren e	-	_	-						15	214.7	10.6	05	264.7	13.0
16		00.8	66	65.9		116	115.9	05.7	166	165.8	08.2	216	215.7	10.6	266	265.7	13.1
17		00.8	67	66.9		17	116,9	05.7	67	166.8	08 2	17	216.7	10.7	67		13.1
18		00.9	68		03.3	18	117.9	05.8	68	1678	08.3	18	217.7	10.7	68	267.7	13.2
19	19.0	00,9	69	68 9	03.4	19	118.9	05.8	69	168 8	08.3	19	218.7	10.8	69	268.7	13.2
20	20.0	01.0	70	69.9	03.4	20	119.9	05.9	70	169.8	08.4		219.7	10.8	70	269.7	12.2
21	21.0	01.0	71	70.0	03.5	121	120.0	05.9	171	170.8	08.4	221		_	-	_	- 3.3
22		01.1	72		03.5	22	121,0	06.0	72	171.8	08.5	1 1 1	220.7	10.9	271	270.7	13.3
23		01.1	73		03.6	23	122.0	06.0				22	221.7	10.9		271,7	
24		01.2	74		-	24		06.1	73	172.8			222.7	11.0	73	272.7	
		01.2	75	1	03.6	25	123.9	06.1	74	173.8		11	223.7	11.0	74	273.7	13.5
25	1-	-		74 9			124.9		75	174.8	08.6	25	224.7	11.1	75	274.7	13.5
26		01.3	76	75.9		126	125.8	06.2	176	175.8	08.6		225.7	11.1	276	275.7	13.6
27	1.	01.3	77		03.8	27	126.8	06.2	77	176.8	08.7	27	226,7	11,2	77	2	13.6
23	28.0	01.4	78		03.8	28	127.8	06.3	78	177.8	08.7	28	227.7	11.2	78		13.7
29		01,4	79	78.9	03.9	29	128.8	06.3	79	178.8	08.8	29	228.7	11.3	79	278.7	13.7
30	300	01,5	80	79 9	03.9	30	129 8	06.4	80	179.8	08.8	30	229.7	11.3	80	279 7	13.8
31	21.0	01.5	81	_	04.0	131	130.8	06.4	181	180.8	_	-			281		
32		01.6	82		04.0	11 -	131.8	06,		181.8		231	230.7	11.4		280.7	13.8
33		01.6	83	82.0	04.1			06.5	83	182.8			231.7	11.4		281.7	13.9
34		01.7	84	83.9		33	132.8	06.6	84				232.7	11.5		282.7	13.9
35			85			34	133.8			183.8	09.0		233-7	11.5		283.7	14 0
110		01.7	_	84.9	04.2	35	134.8	06.6	85	184.8	09.1	35	234.7	11.5	85	284.7	14.0
36	36.0	01.8	86	85.9		136	135.8	06.7	186	185.8	09,1	236	235.7	11.6	286	285.7	14,1
37	37.0	8.10	87	86.9	04.3	37	1 36.8	06.7	87	186.8	00.2	37	236.7	11.6	87	286.7	14.1
38	38.0	01.9	88	87.9	04.3	38	137.8	06.8	88	187.8	09.2	38	237.7	11.7		287.7	14.2
39	39.0	01.9	1 99	88,9	04.4	39	138.8	06.8	89	188.8	09.3	39	238.7	11.7	80	288.7	14.2
40		02.0	90	89.9	04.4	40	139.8	06.0	90	189.8	00.3	40	239.7	11.8	90	289.7	14.3
41	-	02.0		90.9			140.8						33.1		-	-3.1	4.3
42		02,1				42	141.8	30.9	191	190.8	09.4		240.7	11.8	291	290.7	14.3
	42.9	02.1			04.5				91	191.8	09.4	42	241.7	11.9	92	291.6	14.4
73	42.9	02.1			04.6		142.8	07.0	93	192.8	09.5		242.7		93	292.6	14.4
44		02.2	94	93.9		44	143.8	07.1		193.8			243,7	12.0		293.6	
45	44.9	02.2	95	94.9	04.7	45	144.8		95	194.8			244.7	12.0		294.6	
	45.9	02.3	96	95.9	04.7	146	145.8	07.2	196	195.8	00.6	246	245.7	12.1		295.6	
47	46.9	02.3	97	96.9	04.8	47	146.8	07.2	97	196.8	00.7	47	246.7	12.1		296.6	14.6
48	47.9	02.4	98	97.9	04.8	48	147.8	07.2	98	197.8	00.7	48	247.7		08	297.6	14.6
	48.9			08.0	04.0	49	148.8	07.2	99	108.8	00.8	40	248 7	12.2	00	208 6	14.0
	49.0		100	99.0	04.0	150	149.8	07.4	100	100.8	00.8	250	240.7	12.3	100	298.6	4.7
	Dep			<u>D</u>	1.00	D.0	D.		7	23.0	3,0	5	249.7		3	299.6	
~	Deb.	1.4	OIL	Dei	il at	DIM	Dep	Lat	אוען	Dep '	Lat	יווים	Dep	Lat	Ditt	Dep	Lat
	35 W. T.	100		11.	10.12	1.17			H 1	100	17 9 95			4. 44			

for 73 Points.

_		-	-		153	1112 -				-	-	15.0		A STATE OF THE	-510		
Ditt	Lat	Del	Dil	Lat	Dei	DV	Lat	Dep	Diff	Lat	Dep	Diff	Lat	Dep	Dift	Lat	De,
1	01.0	00,1	51	50,8	05.0	101	100.5	09.9	151	1 50.3	14.8	104	200.0	19.7	151	249.8	24 6
2	02.0	00,2	52	51.8	05.1	02	101.5	10.0	52	151.3	14.9	02	201,0	19.8	52	250.8	24.7
3	03.0	00.3	53	52.7	05.2	03	102.5	10.1	53	152.3	15.0	03	202.0	19.9	53	251 8	24.8
4	04.0				05,3	04	103.5		54	I 53.3	15.1		203.0		54	252,8	
5	05.0	00.5	55	54.7	05.4	05	104.5	10.3	55	154.3	15,2	05	204.0	20.1	55	253.8	25 0
6	06.c	00.6	56	55.7	05.5	106	105.5	10.4	156	155.3	19.3	206	205,0	20.2	256	254.8	25.1
7	07.6	00.7		56.7	1	07	106.5		57	156.2		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	206.0	100000000000000000000000000000000000000	57	255.8	
	08.0	00.8	58	57.7	05,7	08	107.5			157 2		08	207.0	20,3		256.8	
9	09.0	00 9	59	58.7	05.8	09	108.5	10.7	59	158.2			208.0		59	257.8	
10	10.0	01.0	60	59,7	05.9	10	109.5	10,8	60	159.2		10	209.0	20.5	60	258.8	25.5
11	10.9	01.1	61	60.7	06.0	111	110.5	10.0	161	160 2		211	2100	20.6	261	259.7	25 6
12	119	200		61.7		12	111.5		62	161.2		P. Sec. 217	211.0	2.1		360.7	
13		01.3		62.7		13	112.5		63	162.2			212.0		63	261.7	
14	7 3	01,4	1 -1	63.7		14	113.5		64	163.2		1	213.0	9 32 6	64	262.7	
15	14.9	01.5		64.7		15	114.4		65	164 2		1 15	214.0		65	163.7	
16		01.6	66	65.7	06.5	116	115.4	11.3	166	165.2	_	216	215.0	-	266	364.7	
17	16.9	1000		66,7		17	1164	11.4	67	166.2		17	216,0		67	265,7	
18		01.8		67.7		18	117.4			167.2			217.0	21 1		266.7	
19	1	01.9		68.7		19		1 21	69	168.2			217.9			267.7	
20		32.0		69.7		20	119.4	11.7	70	169,2	3		218.9		70	268.7	10 20 0
21				_	06.9	-		11.8	_	_				_		-	-
22	20.9	10000				121	120.4		171	170.2			219.9		271	269.7	
23	22.0			72.6	07.0	22	121.4	11.9	1000	171.2			220.9		72	270,7	
24	23.9			73.6		23	122.4		73	172.2		23	221.9		73	271.7	
25	24 0				07,3	25	124.4		74	173.2		25	223.9		74	272.7	T. Carlotte
		-						_			-	-	-		75	273.7	1
26	25.9				07.4	126	125.4		176	175.2	100	220	224.9		276	274.7	1.2.4
27	26.9	100			07.5	27	126.4		77	176.2		27	225.9		77	275,7	
	27.9	A 200			07,6	28	127-4			177.3		28	226.9		78	276.7	
		3.4			07.8	29	128 4		79 80	178.1			227,9		80	277.7	
30	29.9					30	129 4		_	179.1	_	30	228.9	22.5	-	278.7	
31		03.0			07.9	131	130.4		181	180.1		231	229.9		281	279.6	
32		03.1		0.77	08.0	32	131.4			181.1			230.9			280.6	
33		03.2		in .	08.1	33	132.4	100	83	182.1		700	231.9		83	281.6	
34		03.3			08.2	34	I 33.4		84	183.1			232.9		84	282.6	
35		03.4			08.3	35	I 34-4	3.2	85	134.1	18.1	35	233.9	23.0	85	283.6	-
36		03.5			08.4	136	135.3	13,3	186	185.1		236	234.9	23.1	286	284.6	100 200
37	36.8		0.0		08.5	37			87	186.1		37			87	285.6	
38	37.8	03.7	88		08.6		1 37-3	13.5	88	187.1	18,4		236,9	23,3		286.6	
		03.8			08.7	39	138.3	13.0		1.88.1			237.9	23.4		287.6	
_	39.8			_	08.8		1 39.3		90	189.1	_		238.8		90	288.6	
41		04.0			08.9		140,3		191	190.1		241	239.8	23.6	291	289.6	
	41.8				09.0		141.3		92	191.1			240,8			290.6	
	42.8				09.1		142.3			192.1			241.8			291.6	
		04.3			09.2	44	143.3		94	193.1	19.0	44	242.8			292.6	
45		04.4	95	94.5	09.3	45	144.3	14.2	95	194.1	19.1		243.8		95	293.6	
46	45.8	04.5	96	95.5	09.4	146	145.3	14.3	196	195.1	19.2	246	244.8	24.1	296	294.6	29.
		04,6	97	96.5	09.5	47	146.		97.	196.1		47	245.8	24.2	97	295.6	29.
	47.8		98	97.5	09.6	48	147.3	14.5	98	197,0	19.4	48	246.8	24,3	98	296.6	29
			99	98.5	09.7	49		14.6	99	198.0	19.5	49	247.8	24.4	.99	297.6	29.
5 e	149.8	04.9	100	99.	09.8	150			200	199.0	19.6		248.8			298.6	
	Dep																

60 Difference of Latitude and Departure for 3 Points.

DA	Lat	Derl	Die	Lat	Depl	Dift	Lat	Depl	1Diff	Lat	Der	Dia	II.at.	Deul	(Dift)	Tat	Dep
_	_		-	-					-			_		Dep	_		-
1	01.0		51		07.5	02	99.9	14.8		149.4				29.5		248.3	
3	01.0	00.3	53	51.4	07.8	03	101.9	15.1	52	150.3	22.3	03		29,6		249.3	
4		00.6	54	53.4		04	102.9	15.3	54	152.3			201.8	29 9		250.2 251.2	
5	04.9		55	54 4	68.1	05	103.9	15.4	55	153.3	22.7	05	202.8	30.1		252.2	
6	-	00,9	56	55,4	08.2	106	104.8	15.5	156	154.3	22.0	206	203.8	30.2			-
7		01.0	57		08.4		105.8			155.3	23.0		204.7	30.4	100	253.2 254.2	
8		01.2	58	57.4	08.5	08		15.8	58	156.3		2	205.7	30.5	58	255.2	
9	08.9	01.3	59	58.4	08.6	09	107,8	16,0	59	157-3	23.3	09	206.7	30.6		256.2	100
10	09.9	01.5	60		08.8	10	108.8	16.1	60	158.3	23.5	10	207.7	30.8	60	257.2	38.1
11	10,9		61		08.9	111	109.8	16.3	161	159.2		211	208.7	30.9	261	258.2	38.3
12	11.9		62		09.1	A 17	110.8	16.4	62	160.2	23.8	12	209,7	31.1		259.1	13
13	12.5		64		09,2		111.8	16.6		161.2			210,7	31.2		260.1	13
15		02.1	65		09.4	15		16.7	65				211.7	31.4	65	261.1	13-1
-	-	_	-	-	-	-	113.7	-	-	163.2	_	-	212.7	31.5	-	262.1	1 2 2
16		02,3	66	1-2.3	09.7		114.7	17.0				216	213.7	31.7		263.1	100
18		02.6			10.0	-0	116,7	17.2	68	1	24.5		214.6	31.8	68	264.1	1
19	1	02.8	11 .	1	10.1	19	117.7	17,5	69	167 2	24.8	19	216.6	32.1	1	266.1	33.3
10	19.8	02.9				20	118.7	17.6	70	168.1	24 9		217.6	32.3			132.3
21	20.8	03.1	71	-	10.4	121	119.7	17.7	171	169.1		-	218.6	32,4	271	268.1	39
22		03.2			10.6	22	120.7	17.9	72	170.1	25.2			32.6		269.0	132.1
23		03.4	73	72.2	10.7	23	121,7	18.0		171.1	25.4		220.6	32.7	73	270.6	
24		03.5			10.8			18.2	74	172.1	25.5		221.6	32.8	74		40.2
25	24.7	03.7	_		11.0	25	123.6	18.3	75	173.1	25.7	25	222.6	33.0	75	272.0	40.3
16	25.7	03,8	76	75.2	11.1	126	124.6	18.5	176	174.1	25.8	226	223.5	33.1	276	273 0	40.5
27		04,0			11.2		125.6		77	175.1			224.5	33.3	77	274.0	40.6
28		04.1	78		111.4	11			78	176.1			225.5	33.4		275.0	
29		04.3	80		111.6	-			79 80	177.1			226,5	1 To 1 To 1	0	276,0	1
30	-	04.4	11 -	13	-			-	_	-			227.5	33.7		277.0	41.1
31		04.5	110		111.9				181				228.5			277.9	
33	1 -	04.8	110		3	11 -	130.6		83				229.5	1-	82	278.9	
34	1-	05.0	110			34	132.5	1	11 6	182.0			231.5	34.3	84	-13.	41.6
35	34.6	6 05.1	85				133.5	19.8	85				232.4	34.5	85	281	
36	35.6	05,3	86	85.7	12.6	136	134.5	19.9	186	184.0		_	233.4	24.6	-06	282.0	
37	36.6	05 4	87	86.1	12.8	37	135.5	20.1	87	185.0	27.4	37	224.4	34.8	11 -	283.	
38	37.5	05.6	88	87.0	12.9	38	136.5	20.2	88	186.0	27.6	38	235-4	34.9	11 00	284.	
39	38.€	05,7	1 89	88,0	13.0	1 39	137.5	20.4	09	10 .9	27.7	1 39	236.4	35.0	89	285.	42.4
40		05.9		89.0	13.2	40	138.5	20.5	90	187.9	27.9	40	237.4	35.2	90	286.1	8 42.5
41		06.0		90.0	13.3		139.5	20.7	191	188.9	28.0	241	238.4	35,3	291	287.8	42.7
42	41.5	06.2	92		13.5	42	140.5	20.8	92	189.9	28.2	42	239.4	35-5	92	288.8	8 42.8
43	42.5	06.3			13.6		141.4		93	190.9	28.3	43	240.4	35.6	93	289.	43.0
44	43.5	06.5	94		13.8	44	142.4	21.1		191.9			241.3		94	290.	43.1
45					13.9		143.4		95				242.3	35.9		291.8	-
	45.5	06.7	96	95.0	14.1	146	144.4	21.4	196	193.9	28.7	240	243,3	36.1	296	292.	43.4
48	47.5	07.0	108	95.9	14.2	47	145.4	21.0	08	194.9	20.9	47	244 3	36.2	97	293.8	43.6
.49	48.5	07.2			14.5		147.4		90	196.8		40	245.3 246.3	36.5		294.8	43-7
50	49.5	07.3	toc	68.0	14.7	150	148,4	22.0	200	197.8	20.2	250	247.2	36.7	100	206	43.2
	Dep						Dep	Lar	Diff	Den	La	Dift	Den	Lat			
-		- (1	Р	24,1						,		Эср		I I	Del	l La

1	1	David	10:4	Las	D	D:A	1	De I	ID:A	Tat	De l	D:4	Lat	Denl	D:4	Tas	Da
	_				_				-	Lat				-			-
1	0.10		51		10.0	101	99.1	1.5	151	148.1	29.5	201	197.1	39 2		246.1 247.1	
:	02.0		_	51.0		02	100.0		52		29,7	03	199.1	39,4		248.1	
	039	-		53.0		04	102.0			151.0	30.C	04	200.1	39.8		249.1	
	04.9		55	53.9		05	103.0	1	55	152.0	30.2	05	201.0	40.0		250.1	
			56	_	_	106				_	30.4	-	202.0	40.2		251.1	
		01.2		54 9 55,9		07	104.0		. 750	153.0	30.6	07	203,0	40.4		252.0	
		01.6		56.9	11.3	08	105.9	-		154.9	30.8		204.0	40.6	58	253.0	50.
		8.10		57.9	11.5	09	106.9			155.9	31.0	1	205.0	40.8		254,0	
		02.0		58.8		10	107,9			156.9	31,2	10	205.9	41.0		255.0	
11	10,8	02.1	61	59.8	11.0	111	108.9	21.7	161	157.9	31.4	211	206.9	41.2		256.0	
12	11.8			60.8			100.8			158.9	31.6		207.9	41.4		256,9	
13		02.5	63	61.8	12.3	13	110.8	-		159.8	31.8		208.9	41.6		257.9	
14		02.7		62.8		14	111.8	22.2		160.8	32.0	14	209.9	41.8		258.9	
15	14.7	02.9	65	63.7	12.7	15	112.8	22.4	65	161.8	32.2	15	210.8	42.0	65	259.9	51.
16	15.7	03.1	-	64.7	12.9	116	113.8	22,6	166	162.8	32.4	216	211.8	42.1		260.9	
17		03.3	67	65.7	13.1	17	114 7		67	163.8	32.6	17	212.8	42.3	67	261.8	52,
18	17.7	03.5		66.7		18	115.7		68	164.7	32.8		213.8	42.5		262.8	
19		03.7		67.7	13.5	19	116.7	23.2	69	165.7	33.0		214.8	42.7		263.8	
20	19.6	03.9	70	68.6	13.7	20	117.7		70	156.7	33.2	20	215.7	42.9	70	264.8	52.
21	20.6	04.1	71	69.6	13.9	121	118.7		171	167.7	33.4	221	216.7	43.1		265.3	
22	21.6				14.0	22	1196		72	168.7	33.6		217.7	43.3		266.7	
23	10.10.12	04.5		71.6			120.6			169.7	33.8		218.7	43.5	73	267.7	53.
24		04.7				24	121.6			170.6	34.0	24		43.7		268.7	
25	24.5	04.9	75	73.6		25	122.6		75		34.1		220.6	43.9		269.7	
26		05.1	76	74.5		126	123.6				34.3		221.6	44.1	276	270.7	153.
27		05.3	77		15.0	27	124.5		77	173.6	34.5		222.6	44-3		271.6	
28		05.5	78		15.2	28	125.5		78	174.6	34.7	28	223.6	44,5		272,6	
29		05.7	79	77.5	15.4	30	126.5		79	175.5	34.9		224.6	44.7	80	273.6	154
30		05.9	-							-	-		_	44.9			-
31		06.0	81	79.4	15.8	131	128.5		181	177.5		231	126.5	45.1	82	1-13.	
32		06.2	83		16.0	32	129.5			178.5		32	227.5	45.5		276.9	55
33		06.6	84	82.4	16 4	34	131.4		84				229.5	45.7	84	278.	55:
35	34.1	06.8	85		16.6		132.4		85				230.5	45,9		279.	
36			86		16.8	136		_	186		1		231.4	46.0		280.	
37		07.0	87		17.0					183.4			232.4	46.2		281.	
-		07.4			17.2		135.			184.4			2334			282,	
39	38.	07.6	89	87.3	17.4		136,		89	185.3	36.9	39	234.4	46.6	89	283.4	56
40		07.8			17.6		137.				37.1		235.4	46.8	90	284.4	1 56
41	40.	08,0	91		17.8		138.			187.3	57.3	241			291	285.	1 56
42		08.2	62	90.	18.0	42	139.		92	188.3	37-5	42	237.3	47.2	92	286.4	1 57
43		2 08.4	93	91.2	18.1	1 43	140.1	27.9	93	189.3	37.7	43	238.3	47.4	93	287.	3 57
44	43.	08.6	94		18.3	44	141.	2 28.1	94	190.2				47.6	94	288.	3 57
45	44.	08.8	95		18.5		142,			191.2						289.	
46		1 09.0		94.	1 18,7	146	143.	28.5	196		38.2		241.2	48.0		290.	
47	46.	1 09.2	97	95.	1 18.9	47	144,	2 28.7	97	193.2	38.4	47	242.2	48.2	9	7 291.	3 58
48		1 09.4			1 19.1	48	145,	1 28.9	98	194.2	38.6	48	243.2	48.4	9	8 292.	
49		1 09.6			1 19.3			1 29.1	99	195.2	38.8		244.2	48.6	9	9 293.	
50		0 09.8			1 19.			1 29.3	200	196.1						294.	_
Dil	1 De	plLat	II Dit	De	La	Dit	t IDep	1 La	IIDil	Dep	Lat	Dif	Dep	La	Di	"Dep	11

62 Difference of Latitude and Departure for 14 Point.

Did	Lat.	Denl	Dift	Lat	Devil	Ditt.	Lar	Devil	Dim	Lat	De.I	Ditt	Lat	Det	Dist	Lat	Dep
_			-	_		-					- 8	201	195,0				-
	01,0			49.5		101	98.0			146.5		1.4	195.9		52	243.5	
	01.9				12.9	02	98.9	15.0		148.4			196.9			245-4	
	03.9				13.1		100.9			149.4		04	197.9		11	246.4	
	04.9		55		13.4		101 9		55		37.7	05	198.9		55	247.4	
-	05.8		56			_	102.8				-	_	199.8		256	248.3	_
	06.8				13.6		103.8			151.3		07	200,8	50.2	57	249.3	
8		31.9			14.1		104.8		58	153.3	28.4	08	1 ~		58	250 3	
9		02.2	59		14.3	09	105.7			154.2	38.6	09	202.7		59	251.2	
10	09.7		60		14.6	10	106,7		60	155.2	38.9	0.00	203,7	-	60	252.2	
11		02.7	61	-	14.8	111	107.7	27.0	161	156.2	-	211	204.7	51.3	261	253.2	62.4
12		02 9	62		15.1	12	108.6		62	157,1	1	12	205.6		62	254.1	
113		03.2	63		15.3	13		27.5	63		39.¢		206 6		63	255.1	10
14	1-3.6	03.4		1	1 5.6	14	110.6	27.7	64	-	39,9	14	207.6	52.C	64	256.:	64.2
15	14.6	03.6	65	63.1	1 5.8	15	111.6	17.9	65	160 1	40,1	15	208.6	52.2	05	257.1	64.4
16	15.5	03.9	66	64.0	16.0	116	112.	28.2	166	161.0	40.3	216	209.9	52.5	266	258.0	64,6
17		04.1	11 0	65.0	16.3	17	113.	28,4	67	162.0	40.6	17	210.	52,7	67	259.0	64,9
18		04.4		1000	16.5	18		28.7	68	163.0	40.8	1 28			68	1 /	65.1
19		04,6	69		9 16.8	11		4 28.9	69		9 41.1		212.4		69		65.4
20	19.4	04,9	70	67.	9 17.0	20	116.	4 29.2	70	164.	9 41.3	1 20	213.4	53.5	70	-	65.6
21	20.4	105.1	71		9 17.3		117.	4 29-4	171		9 41.6		214.4	153.7	271		65.9
22		3 05.			8 17.5		118.	3 29.6			8 41.8			3 53.9	72	1 .	66.1
23		3 05.			8 17.7			3 29.9			8 42.0		216.				66.3
24		3 05,			8 18,0			3 30.1			8 42,3	1 3	217.		74	205.	66.6
25		3 06.	_		8 18.2		_	3 30.4		_	8 42 5	-	218.	-	75		_
26		2 06.			7 18.5			2 30.6	11		7 42,8		219.		276		67.1
27		2 06.			7 18.7			2 30.9			7 43.9	11 -	7 220. 8 221.				67.3
29		1 07.			7 19.0	11		2 31 1			7 43						6 67.8
30		107.	11 2		6 19.4			1 31.6			6 43.			1 55.9	11 0		6 68.0
		_		-	6 19.		_	1 31.8	-		6 44.0	-		1 56.1			6 68.3
31		0 07,	-11		5 19.0			c 22,			5 44-		2 225	0 56.4	82		5 68.5
33		0 08,			5 20.			0 32.		1./-	5 44-	-11 -	3 226.	0 56 6		1 2	5 68.8
34	122.	0 08.	3 8		.5 20.			0 32.	41 6	1 / 1	5 44		4 227.		84	275,	
33		0 28.	5 8		.5 20.			0 32.1			5 45.		5 228:	0 57.1	8	276.	5 69.3
30		9 08.		6 82	4 20.	136	121	9 33.0	186	180.	4 45	2 23	6 228.	9 57-3	286	277.	4 69,5
37		909	0 8	7 84	4 21.	1 37		9 33-			4 45,	4 3	7 229.	9 57.6	87	278.	4 69.7
31	100	909.	2 8	8 85	4 21.	4 38	133	9 33.	5 88	182.	4 45	7 3	8 230.	9 57.8	81		4 70.0
39		8 09	5 8	9 86	.3 21,	6 39	134	8 23.	8 89	183	3 45.	9 3	9 231.	8 58.1	1 89	280.	3 70.2
40	38	8 09.	7 3	0 87	.3 21.	9 40	135	8 34.	90	184	3 40.	2 4	0 232.				3 70.5
4	1 39	8 10	0 9	1 88	.3 22.	1 41	136	8 34.	3 191	185	3 46.	4 24	1 233.	8 58.	29	282.	3 70,7
4	40	7 10	2 9	2 89	. 2 32.	4 42	137	7 34.	5 92	186	2 46,	7 4	2 234.	7 58.	8 9:	283,	2 71.0
4	41.	7 10	4 9		.2 22.	6 4	138	7 34.	7 93	187	2 46.		3 235			284.	2 71.2
4	42	7 10	7 9		.2 22.		139	7 35	94		.2 47.		4 236	7 59.			2 71,4
4		710	_	_	2 23.		140	7 35	2 99		,2 47.			7 59.			2 71.7
4		6 11		6 93	.1 23.	3 140	141	6 35.	5 196	190	.1 47.	6 24	6 238	6 59.	8 29		1 71.9
1 4		6 11	4 9	7 94	.1 23.	6 47	142	6 35.	7 97		1 47,		7 239				1 72.2
1 #		6 11		8 95	.1 23.				98	1192	1 48.		8 240				1 72.4
1 4		5 11			.0 24.			.5 36.	5 200	193	0 48	6 2	9 241 C 242	5 60	7 20	290	0 72.7
150			2 10		.0 24.	3	145	.5 36.	2	194	0 48.			_	_		
U	A L'e	plLa	tilla	m D	ep Lat	ויעון	ig De	PILA	Di	line	'La	JID	tt e	, 'L.a	111.71	ft Der	, .L.
200		11111	1 12	121	2 12 1	2 1 1		The same				1- 41		_ 14 (3)	-	100	

for 6 3 Points.

					-			D:A			Dayl	ın:	Ai T	at I	Dei	ID	iti	Lat	De	1 11	Dift	Lat	D	ep
_	_		-11	Dift	Lat	שו	15	Dift				-	-	4 5	42.8	8 2	1	192.	1 58	-3	251	240.	2 72	8
		00			48.			101			19.3 19,6	5		5.5	44.	1		193.	3 58	.6		241.		
		00.		1.0	49.	7 15		02			29.9			2 -	44.	11	03	194.	-	- 11	-	242.		
10	2.9	00.	9	53 54	51			04			30.2		4 14	7.4	44,	. 1 1		195.	11.1			243.		
		01		55	52.	6 16).c	05			30.5	5		8.3	45.			196.	_	1.5		244.	_	
1-	-	1-	-11	56		6 16		106			30.7	15	6 14	19-3	45		06	197.	1 59		256			
. 1	5.7	01	6	57	54	5 16	5 5	07			31.0	11 5	7 1		45.	-		198.		0.3		245		
		02		58		5 16	5.8	08	10		31.3		8 1	51.2	45.		00	199.	0 60			247		
	-	02		59	56.	5 17	7.1	09			31.6	11 6		52.2	46.			201.		0.9		248		
	9.6	02	9	60	57.	4 17	7.4	10	-		31 9	11-	_	_	-	_	-	201.	- -	1.2	-	249		
1	10,	03	. 2	61	13		7.7	111		100	32.2	11		•	46.			202	2	1.5	62	250	.7 7	6.0
		5 03		62	159	3 1	8.0	12			32.			55.0 56.0	47			203	-	1.8		251		
3	12	4 03	.8		60			-			32.8	11 4	64 1	56.9	47		14	204	8 6:	2.1		252		
- 1	13.		100	66	61	2 1	8.0	14			33.4	11		57.9			15	205	.8 6	2.4		253		
-1	14	-	-	-	3		_	116	_	_	33.	-11		58.9		. 1	216	206		2.6		254		
	15.			66	64	2 1		17	111	2.0	33	ell (67 1	598	48	.4		207		2.9				77.4
		2 0			65			1	11	2,9	34	2	68 1	60.8	48	.7		208		3.2	60	256	,5	77.7
19	-	20	3000	6	1	.0 2	-		111	3.9	34	5		61.7				210		3.5	79			78.3
0		10	-	70	1.	.0 2	0.3	20	11	4.8	34.		-	62.7	_	- 1		-	- -	-	-			
11	-	1 0	_	7	1 67	9 2	0.6	12			35.			63.6				211	- 10	4.1	271	2 26	. 3	78.6 78.9
22		10		11 .	2 68	.9 2	0.9	2:			35.	-11		64.6	49	0.2	1.1	213	- 1	4.4				79.2
23	22.	0	6.7	1 7		9 2			3 1	7.7	35.	7	131	165.6		0.5		214		5.0				79.5
24	23	00	7 0	7		.8 2	11.5	2			36. 36.			167.		8.0		21		5.3	7	5 26	3.2	79.8
25	23	9 6	7-3			-					36.			168.	-	1.0	226	216	5.3	5.5	27	6 26	4.1	80.0
26	44		7.5		1.	-7			7 1	20.1	5 36	8 .		169.	. 12	1,3	27	217	7.2		7	7 26	5.1	80.3
27		.80			7 73	1.6	22.	211	8 1	22.	37	1		170.		1.6		21		66.1	7	8 26	6.0	80.6
29		.80		11.	9 7	5.6	22.	9 2	9 1	23.	5 37	4	79	171.	3 5	1.9		21		66.4 66.7				80.9
30		.70				6.6			0 1	24.	4 37	·7 .		172.		2.2	30	_	-		1	-	-	81.
31	-	1.7	_	-11-	1 7	7.5	23.	5 13	1 1	25.	4 38	.0	181	173.		2.5		1 22		67.0 67.3	11 0			81.
32		.6		3 8	32 7	8.5	23.	8 3	12 1	26.	3130	·311		174		2.8	3			67.6	11 0			82,
33		1.6		6 8	- 10	9.4	1		33 1	27.	3 38		84	175	1 3	3.1	3	-		67.9	8	4 27	1.8	82.
34		1.5				1.3			S 100 A	20.	2 39	.2	85	177		3.7	3		4.9	68.2	1 2	5 2	12.7	82.
35		22	10.	-11-	-	-	-				2 39	-11	186	178		3.9	23	6 22	5.9	68.4				82.
36		1.5		7	86 8	2.3		9 1			1 39		87	179		54.2	3	7 22	6.8.			37 2	74.7	83.
37	3	5,4	10. I I	/	88 8				38	132	.1 40	0.0	88	179	.9	54.5	3	8 22	7.8	69.0		80 2	75.6	83.
38		7.3	11.	2	80 18	5.2	25	.8	39	133	.04	0.3	89	180	.9				8.7	60	6	902	77.	83.
40		8.3	11.		90	36.1	26	.1	40	134	.0 4	0.0		181		55.1	1 20			69.		05	78	84
41		9.2		-11-		37.1			41	134	,9 4	0.9	191	182		55.4		1 2	30.6	69.		92 2	70.	4.84
42	14	0.2	12	.2	92	88.0	26	.7	42	135	.04	1.2	92	183	.7	55.7		2 2	31.6 32.5	70.		93 2	80.	4 85
4:	3 4	1.2	12	.5	93	89.0	27	.0	43	136	,94	- 5	93	184	7	56.		4 2	33.5	70.	8	94 2	81.	4 8 5
4		2.1				90.0			11	137	.8 4	2.1	95		6.6	56.6	5		34.5		- 11	95 2	82,	3 85
4	7 1-	3.1	-	-11	-	90.9			45				196	-		56.1		16 2	35.4	71.	3 2	96 2	83.	3 85
4		4.0			96	91.0	9 27	.8	46	139	0.7 4	2.6	190	18		57.	1 4	47 2	36.4	71.	6	97 3	84.	2 86
4	8 1	15.0	13	0.0	97	93.	8 25	3.4	47	14	.64	2.9	9			57.4	4 4	48 2	37.3	71	911	98	285	2 86
4	0	45.9		9	99	94.	7 2	8.7	49	14	2,64	3.2	9	19	0.4	57-	7 1 4		38.3					1 8
		47-9				95.			150		3.5		20	0 19		58.	- 11-		39.2				-	1 8
10	-	De			_	De			Ditt		p		Di	AlDe	ep	La		lhic	Dep	IL	21	Ditt	Del	L
			-	10	- 40				7.				-			_	7 77 7		2000					

64 Difference of Latitude and Departure for 13 Point.

Dif	Lat Dep	Dift	Lat	Depl	(Dift	Lat	Deul	(Dift)	Lat	Deil	Dif	Lat	Deil	1Dia	Lat	Den
1	-	51	48.0	-	101		34.0					189.2				
2	01.9 00,7		49.0		02	96.0		151	142.2			190.2			236 3	
3	02.8 01,0			17.9	03		34.7	53	144.0		•	191.1		53	237.3	84,9
4	03.8 01.3		50.8	18,2	04		35.2	54	145.0			192.1		54	239.1	85.5
5	04.7 01.7	55	51.8	18.5	05		35.4	55	145.9		1 2	193.0		55	240.I	85,9
6	05.6 02.0	56	52.7	18.9	106		35 7	150	146.9	52,5	206	194,0	69.4	256	241 0	86.2
7	06.6 92.4	57		19.2	07	100.7		57	147.8	52.9		194.9		57	242,0	86.6
8	97.5 02.7	58		19.5	08	101.7		58	148.8	53.2		195.8		58	242.9	86.9
9				199	09	102.6	36.7	59	149.7			196.8		59	243.8	87.2
10	09.4 03.4	60	13	-	10	103.6	_	60	150.6			197.7		00	244.8	87.6
111	1	61	131	20.5	111	104.5		161	151.6			198.7		261	245.7	87.9
13	A RESIDENCE A STREET, SALES	63	58.4	21.2	12	105.4		62	152.5			199.6		62	246.7	88.2
14	The second secon		120	21.6		106,4		63	153-5			200,5		63	247.0	88.6
15	14-1 05.1				15	108.3		65	154.4			201.5		65	248.6	\$8.9 89.2
16	15.1 05.4		_	-		-	-	166		-				266	249.5	_
17	16.005,7	11.			17	110.2		67	156.3			204.3		67	250 4	89,6
18	17.0 06.1	68		22.9	18	111.1		68	158.2			205.2		68	251.4	89.9 90.3
19		69		23.2	19	112 0		69		56.9		206.2		69	253.3	90.6
20	18 8 06.7	70		23.6	20	113.0	10.4	70	160.1	10 0	20			70	254.2	90.9
21	19.8 07.1		66.8	23.9	121	113,9	40.8	171	161.0	57.6	221	208.1		271	255.1	91.3
22			67.8	24.2	22	114.9		72	161.9			209.0		72	256.1	91.6
23	2			24.6		115.8	41.4	73	162.9	58.3	23	310.0	75.1	73	257.0	91,9
24	Total Control	74		24.9		116.7	70.00	74	163.8			210.9		74	258.0	92.3
25	23.5 08.4			25.3		117.	_	75	164.8			211.8		75	258.9	92.6
26	24.5 08.8			25.6	126	118.6			165.7		The second second	212.8		276	259.9	93.0
27	25.4 09.1 26.4 09.4			25.9		119.6	17	77	166.6			213.7		77	260.8	93.3
29	27.3 09.8			26.3		120.5		78	167.6					78	261.7	93.6
30		80		26.9	30	121.5		79 80	168.5	50.6	30	215.6	77.5	79 83	263.6	94.0
31		81		27.3	131			181	170.4		-			_		94.3
32		11		27,6	_	123.3		82	171.4			217.5		82	264.6	94,6
33				28.0	33	125.2		83	172.3		33			83	266,4	95.0
34	32.0 11.5	84	79.1	28.3	34	126.2		84	173.2					84	267.4	95.6
35	33.0 11.8	85	80.0	28.6	35	127.1	45.5	85	174.2	62.3	35	221.3	79.1	85	268.3	96.0
36	33 9 12.1	86		29.0	136	128.0		186	175.1	62.6		222.2	79.5	286	269.2	96.3
37	34.8 12.5	87	81.9	29.3	37	129,0	46.1	87	176.1		37	223.I	79.8	87	270.2	96.7
38	33 1.2.0		82.5	29.6	38	129.9	46.5	88	177.0	63,3	38	224.1	80.2	88	271.3	96.0
39		90	84	30.0	39	1 30,9	46.8	89	177.9	63.7	39	225.0			272.1	
40	37.7 13.5			30.3		131.8			178.9			226.0			273.0	
41			85.7	30.6	141	132,8	47.5	191	179.8			226.9	81.2		274.0	
43		92	87.6	31.0	42	133.7			180.8			227.8			274,9	
44		94	88.6	31.7	44	134.6			181.7 182.6	65.0	43	228.8			275,9	
45				32.0		136.5	48.8	95	183.6	66.7		230.7		94	276.8	100000000000000000000000000000000000000
46	43-3 15-5				146		_					231.6			277.7	
47	44.3 15.8		91.3	32.7		137.5	40.5	97	184.5 185.5	66 .		232.5		97	278.7	99.7
48	45.2 16.2	98		33.0		139.3		98	186.4	66.7	48	233.5	82.5	98	280,6	
49	46.1 16.5	99	93.2	33.3		140.3		99	187.4	67,0	49	234.4	83.0	99	281.5	
	47,1 16.8	100	94.2	33-7	150	141.2	50.5	200	188.3	67.4	250	235.4	84.2	300	282.5	
Dift	L'ep Lat	Dif	Dep	Lat	Dift	Dep	Lat	Din	Dep	Lat		Dep			Dep	
2 3 3		100	7.03				30.33		1000			1000000	MA LOS	1000		-

for 6 Points.

13.00	Lat	Dent	19.6	Lat	Depl	(Din	Lat	De. I	Ditt	Lat	Det	Dif	IIa	D-	110:0		-
-	-	-	-	-		-			-			D1.		_	Diff	Lat	Dep
1	00,9			47,1		101	93,3	38.7	151	139 5		201	185.7		251	231.9	96.1
2	01.8			48.0	1	02	94,2	39.0	52	140 4	58.2	02	186.6		52	232.	96.4
3	02.8		53	49 0	3	03		39.4	53	141,4	58.0	03			53	233 8	96.8
4	03.7		54		20.7	04		39 8	54	142.3		04	188.5		54	234-7	97.2
5	-	01.9	55	50.8	21.0	05	97.0	40.2	55	143.2	59.3	05	189.4	-	55	235.6	97.6
6	05.5	02.3	56	10	21.4	106	97-9	40.6	156	144.1	59,7	20t	190.3	78.8	256	236.5	98.0
7	06.5		57	52 7	21,8	07	98.9	410	57	145.1	50,1	07	191.3		57	237.5	98.4
8	97.4		58	53 6	22.2	08	99.8	41.3	58.	146.0	60.5	08	192.2	79 6	58	238.4	98.7
9	08.3		59		22.6	09	The state of the s	41.7	59	146.9			193.1		59	239.3	99,1
10	09.2	33.8	60	55-4	23.0	10	101.6	42,1	60	147.8	61.2	10	194,0	80.4	60	240.2	99.5
11	10.2	04,2	61	56.4	23.3	111	102.6	42 5	161	148.8	61,6	211	194.9	80.8	261	241.1	99.9
12	11.1	04,6	62	57-3	23.7	12	103.5	12.9	62	149.7	62.0	12	195.9		62	242,1	
13	12.0	0.0		58.2	24.1	13	104.4		63	150.6	62.4		196.8		63	243.0	100.7
14		05.4	64		24.5	14	105.3	43.6	64	151.5	62.8		197.7		64	243.9	101,0
15	13.9	05,7	65	60.1	24.9	15	106,5	44.C	65	152.5	63.1	15	198.6	\$2.3	65	244.8	
16	14.8	26.1	66	61.0	25.3	116	107.2	14.4	166	153.4	62.5	216	199.6	82.7	166	245 8	101.8
17	15.7	06.5	67		25.6		108.1	14.8	67	154.3			200,5		67	246.7	
18	16.6	26.9	68	62.8	26.0	18	109.0	45.2	68	155.2	10		201.4		1	247.6	102.6
19	17.6	07.3	69	63.8	26.4	19	109,9		69	156.1	1 .		202.3			248.5	
20	185	07.7	70	64.7	26.8	20	110.9		70	157,1	65.1		203,3			249.5	
21	19.4	03,0	71	65.6	27.2	121	111.8	_	171	158.0	_		204.2	_		250 4	
22	20.3		72	100	27.6	22	112.7		72	158 9			205.1			251.3	
23		08.8	73	67.5	27,9	23	113.6		73	159.8			206.0		73	252.2	
24	22.2	09.2	74		28.3	24	114.6		74	160.8			207.0		74	253.2	1000000
25	23.1	09.6	75		28.7	25	115.5		75	161.7	67,0		107,9		75	254.1	
26	24.0	10.0	76	-	29.1	126	116.4	-	176	162.6			208.8		276		_
27	24.9	1 1 1 1	77		29.5		117.3	48.6	77	163.5			209.7			255.0	
-28	25.9		78		29.9	28	118.3		78	164.5			210.7		0	255.9	
29	26.8		79		30.2	29	119.2		79	165.4			210.6			256.9	
30	27.7	11.5	80	73,9		30	120.1		80	166.3			211.5			258.7	
31	28.6		81	_		131	121 0		181	167.2	_		213.4	_			-
32		12.2	82		31.4	32	122.0	- 1	82	168.2			214.4			259.6 260.6	
33		12.6	83	76.7	31.8	33	122,9	10 0	83	169.1			215.3		- 1	261.5	
34	-	13.0	84		32.1	34	123.8		84	170.0			216.2		84		108.7
35		13.4	85			35	124.7		85	170.9			217.1	DEC AND I			100,1
36		13.8	86	79.5	-	136	125.7	52.0	186	171.9	-		218.0	00	286	-	-
37		14.2		1	33.3	37	126.6		87	172.8			219.0				109.5
38		14.5	88	81,3	22.7		127.5	52.8	88			- 2			88	265.2	109.8
	36.0	14.0	80	82.2	34.1	30	128.4	52.2		174.6	72.2	30	220.8	91.1	80	266,1 267.0	110.2
		15.3	10	83.2	34.4	40	129,4					40	221.7	91.0		267.9	
40	-						-	-	90								
42	37.9	15.7 16.1	91	8.0	34.8		130,3			176.5			222.7			268.9	
43	39.7			85.0	35.6		131.2		92	177.4	73.5		223.6			269.8	
44	40.6				36.0							43	224.5	93.0		270.7	
45	41.6			87.8	36.4	45	133.0	55.6	94	179.2		45	225.4 226.4	93.4		271.6	
	-	_														272.6	_
46	42.5	17,6	90	88.7	30.7	146	134.9	55.9	196	181.1	75.0	246	227.3	94.1	1000	273.5	113.3
47	43.4			89.6			135.8		97	182.0	75,4	47	228.2	94.5	97	274-4	113.7
48	44 4			90.6		48	136.7			182.9		40	229.1	94.9	98	275,3	114.0
	45.3				37.9	43	137.7	57.0	99	183.9	70.2	49	230.1	95,3	99	276.3	114,4
_	_						138.6			184.8			231.C			277.2	
Dill	L'er!	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat
100		1 2	1 1 1 1	100	4: 1/2	1.2.	1	7 A A A A A			10 - 1		The Control	The same			-

		~ .	0.4			(D:4)	1 1	Da. N	D:41	1	Dank	Dia	Tat	Dan i	Dia		10.
Jin!	Lat	D-1	Dift .		_	Ditt	Lat		Diff	Lat		Dift		Dep	Dift		Dep
	00,9	- I			21,8	101	913			136.5		34.11	181.7	85.9	251		107.3
- 1	8.10				22.2	02	. 20	43.6		137-4			182.0	86.8	52		107.8
-	02.7		The state of		22.7	03		44.0	53		6.4		183.5	87.2	53	2.8.7	
	03.6				23.1	04	- 100	44.5	54	139 2		05	184.4	87.7	54	229 6	
5	04.5	02.1	55		23.5	05		44 9	55	_	-					230.5	
	05.4		56	50.6		106	95.8		150	141.0		100,000	186.2	88.1	256	231.4	
		03.0	57		24.4	08		45.8	57	141,9	67.6	1000	187.1	88.5		232.3	
8	07.2		58	-	24.8	09		46.6	58		68,0		188.9	89.4			110.3
9		04,3	59	54.2	25.2	10		47.0			68 4		0 0	89.8	60	235.0	1110.7
-	_	-	61			1		_	161	-			-		261		
11		04,7	62	55.1	26.1	111	1	47-5	11 0-		68.8		190.7	90.2	62		111.6
12		05.1	63		26.9			47.9	11		69.7	100	192.5		63		112.
13		06 0	64		27.4			48.7			2 70.1		193.4		64		
15		05.4	65		8 27.8			49 2						91.9	65	239.	
16	14.5	-	66		28.2			8 49.6	-		-	1	-			1-30	113.7
17		07.3	67	190	6 28.6								196.1			241.	114.2
18		07.7	68	1	5 29.1			7 50.5					197.0				114,
19		08,1	69		4 29.			6 50.9			8 72.		197.9		4 -		1115.0
20	18 1	1 -	70		3 29.			5 51.3		100000000000000000000000000000000000000				94.1			115.
21	100	09 0	71	-	-	1	100.	4 51.7	171	154.	6 73.1	1 221	199.8				115.0
22		09.4	72		1			3 52.2			5 73.		200,				116.
23		09.8		10-			3 44 4	2 52.6			4 74.		201.				116.
24	21.7	1					112	1 53.0					202.		4		7 117.
25	22,6	10.7	75	67.	8 32.	25	113.	0 53.	75	158.	2 74	2	203,4			248.	5 117.
26	23.	11.1	76	68.	7 32.	126	113.	9 53-9	176	159	1 75,	3 226	204.	96.6	276	249.	5 118.
27	24,							0			0 75.		205.		-		4 118.
28	25.	12.0	78	70.	5 33.			7 54-		160.	9 76.	21	206.	97.5	78		-
29	26.	12.4	79	71.	4 33.	8 29	116.	6 55.1			8 76.	29	207.0	97.9	75	252.	1 119,
30	27.	1 12.8	80	72.	3 34.	30	117.	5 55.		162.	7 77.	30	107,	98.	8.	253.	1 119.
31	28.0	13.3	81	73,	2 34.	6 131	118.	4 56	181	163.	6 77-	4 231	208.	98.8	281	254.	0 120,
32	28.	9 13 7	82	74.	1 35.		119.	3 56.4	82		5 77-	32	209.	99.1			9 120.
33	29	8 14.1			0 35.		1000	2 56.9			4 78.	3	210.			255.	8 121,
34		7 14,5						1 57-	3 34		-	7 34		5 100.1	1 0		
35	31.0	15.0	85	70.	8 36.			0 57.			2 79.	3.	212.	100.	8	-31	-
36	32.			1//			122,	9 58.2	186		1 79,		213.	100.		258.	5 122.
37	33.	4 15.8	87	78.	6 37.			8 58.0			0 80,				8	259.	
38	34.	1 6.2	88	79.	6 37.	6 38	124.	7 59.9	38	109.	9 80.	3,		101.		260.	3 123.
	35.	16.7	1 00	180.	5 30,	1 39	125	59.4	3	170.	- 87	3	310.0	102.		201.	2 123.
40		17.1			4 38.		126.			171.				102.0			
41	37.	17,5	91	82.	3 38.	141	127	4 00.	191	172.	0 31,	7 24	217.	103.0	29	263.	0 124.
42	38.0	18.0	92		2 39	3 42	128.	160.7	92	173	0 02.	1	310.	103.	9	263.	9 124
43	38.	18.4	93		1 39.		129,	161	93	174.	4 83.	4	220	5 104.			
44		18.8	94		0 40.1			162	94	175	3 83,			4 104			7 125
45		19.2			9 40.			_									6 126
46		19.7			8 41.0					177.	2 83.	124	311.	4 105.	2 29	267	6 126
47		20,1			7 41.	3 48	132,	8 62	37	170.	084		224	3 105.		208.	5 127
	43.4	20,5			5 42,	1 40	133.	762	90	179.	085		226	1 106.	9	209	4 127
		21.4	199	09.	427	150	125	6 64	200	180	885	250	226	106.	3 3	270	3 127
	-		D:4	50.		130	D.		Di	D	- 3.	1	Dan	l.a	1	1271	- 20.
リル	L'en	Li	וועון	De	plLat	וועון	Det	Lat	llnu	n Deb	Lat	In	n Dep	, 1.a	11131	IT De	p La

Difference of Latitude and Departure for 21 Points. 67

~		10	110:0		-	.D.C		_			1			Carpe 1	120		4.1
DI	Lat	Del	ווטוו	Lai	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat.	[Dep]	Dift	Lat	Dep
	00.9	00,5	51	45.0	24.0	101	89,1	47.6	151	133.2	71.1	201	177.3	94-7	-	221.4	-
2	01.8	00,9	52	45.9	24,5	02	90.0	48.1	52		71.6		178.2		52	222.3	
3	02.6	01.4	53	46.7	25.0	03	90.8	48.5	53		72.1	03	179.0		53	223.1	
4	03.5	01.9	54	47.6	25.4	04	91.7	49.0	54	135.8		04	179 9	96.1	54		2 Ba 68
5	C4-4	02.4	55	48.5	25.9	05	92 6	49.5	55	136.7	720	05	180.8	96.6	1 25	224.0	
-	05.3	02.8	-	49.4	26.4	106			156	-		-			123		120.1
-		03.3	57	1	26.9	07	93.5	District Co.	57	137.6	73.5	206	181.7	97.1	250		120.0
. 6		03.8		-	27.3	08	94 4	50.4		138.5	74.0	07	182.6	97.5	57	226.7	121.1
		04.2	11-	-	27.8	00		50.9	58	139.4		08	183.5	98.0	58	227 6	121,6
10		04.7		52.0		10	96.1		59 60	140.2	74 9	09	184 3	98.5	59	228.4	122.0
-	-		117	-	-	-	97.0	24.0	-	141.1	75.4	10	185.2	98,9	00	229.3	122.5
-11		05.2		-	28.7	111	97,9	528	161	142.0	75.9	211	186,1	99.4	261	230.2	123.0
12	1	05.7			29.2	12	98.8	52.8	62	142.9	76.3	12	187.0	99.9	62	231.1	123.4
13		06.1	11.4	55,6		13		53.2	63			13	187.9	100.4	63	232.0	123.9
14		06,6		-	30.2	14	100.5	53.7	04	144.6	77-3	14	188.7	100.8	64	232.8	124.4
15		07.1	-	<u>57·3</u>	30.6	15	101.4	54.2	-5	145.5	77-7	15	189 6	101.3	65	233-7	124.9
16		07.5		58.2		116	102.3	54-7	166	146.4	78.2	216	190.5	101.8	266	234.6	125.2
17		08.0	11 40	120	31.6	17	103.2	55.1	67	147.3	78.7	17	191.4	102.2	67	235.5	3.3
18		38.5		60.0	32.0	18	104.1	55.6	68	148.2		18	192.3	102.7	68	236,4	
19		09,0		60.9	32.5	19	105.0	56.1	69	149.1	79.6	19	193.2		69	237-3	126.7
20	17.6	09,4	70	61.7	33.0	20	105.8	56.5	70	149.9	80.1	20	194.0		70	238.1	127.2
21	18.5	09.9	71	63.6	33-5	121	106.7	57.0	171	1 50.8		221	194.9		271	-	
22	19.4		11	63.5			107,6				81.0	22		104.6		239.0	
23	20.3	10,8			34.4		108.5			152.6		23	196.7			239-9	
24	21,2	11.3	74		34,9	24	109.4		74	152.5	82.0	24	- 0	105.5		240.8	
25	22.1	11.8	75	66.2	-	25	110.3	58,9	75	154.3	82.5	25		106.		241.7	
26	32.0	12.3	76	67,0	35,8	126				155.2				_		242.5	
27		12.7		67.9		27	111.0	59.4	200		83.4	226	199.3		270	243.4	Company of the compan
28		13.2			26.8	28	113.9	3,	77	150.1		28		107.0	77	244.3	
29		13.7	79	69.7	37.2	29	113.8				0.	29	201.1		78	245.2	131.0
30	1 2 "	14.1		70.6		30	114.7	1	80	158.8	0 5	30	202.9	107.9	0-	246.1	131.5
31	27.3	14,6	81	-	38.2	_		_		<u> </u>	9				-	247.0	131.9
32	100	15,1	82	71.4		131	115.5	61.7		159.6	\$2.3	231	203.7			247.8	132,4
33		15.5			38.6	32	116,4						204.6		82	248.7	132.9
34		16.0	1 34	73.3	39.1		117.3		3		80 2		205.5			249.6	133.3
35	-	16.5	13	75.0	39.0	34	118.2	03.1		102.3	86.7		206.4			250.5	133.8
	-			-	_	33	119.1	93.0	100		87.2	35	207.3	110.7	85	251.4	134.3
36	31.8	TOTAL SECTION AND PROPERTY.	86		40.5	136	120.0	DESCRIPTION OF THE PERSON NAMED IN		164.1		236	208.2	111.2		252.3	134.8
37	-	17.4			41.0		120,8			164.9	THE RESERVE OF THE PERSON NAMED IN	37	209.0		87	253.1	135.2
3.	133.5	17.9	1	77.0	41.5	38	121,7	05.0	88	105.8	88.6			112.1	88	254.0	135.7
39	34.4	18.4		70.5	41,9	39	122,6						00000	112.6	89	254.9	136.2
40	32.3	18.8		79.4	43-4	40	123.5					40	211.7	113.1	90	255.8	136.6
41	30.2	19,3	91	80.3	42.9	141	124.4	66,4	191	168.5	90.0	241	212.6	113.5	291	256.7	137.1
42	37.0	19.8	92	81.1	43-4	42	125.2	66.9	92	169.3	90.5	42	213.4	114 0	92	257-5	137.6
43	37.9	20.3		52.0	43.8	43	126.1	67,4	93	170.2	90 9	43	214.3	114.5	93	258.4	138.1
44	38.8	20.7			44.3		127.0					44	215.2	115.0	94	259.3	
45		21.2			44.8		127.9			172.0		45	216.1	115.4		260 2	139.0
		21.7		84.7	45.2	146	128,8	68.8	196	172.9	92.4	246	217.0	115.9	296	261.1	120.5
		22.1	97	85.6	45.7	47	129.7	69,3	97	173,8	92.8		217.0	116.4	97	262.0	120.0
		22.6	98	86.4	45.2	48	130.5	69.7	98	174.6	93,3	48		116.8		262.8	140.4
		23.1	99	87.2	46.6	40	121.4	70.2	99	176.6	02.8	40	210.6	777 -	00	263.7	
		23,6	100	88,2	47.1	150	132.3	70.7	200	176.4	94.2	250	320.5	117.8	1300	264.6	141.4
Cin	Dep	I.at	Dif	Dep	Lat	Diff	Dep	La	Dia	Der	Lat	Diff	Den	Lat	Dia	Den	
	1 - 27 =-				-	"		-		,				Dat	105	Бер	Lat
																All the second	4

for 5½ Points.

68 Difference of Latitude and Departure for 23 Points.

iftl	Lati	Depl	Dift	Lat	Dep	Dift	Lat	Deil	Diff	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep
-	_	_	_	_		101	_	51.9		129.5				103.3	251	215.3	120.0
	00.9	1 1			26.7	02		52.4		130.4	78 1	1000		103.8		216.1	
	01.7	01.6			27.2	03		52.9	- 1	131.2	78.€			104.3		217.0	
3	P. P. P. P. P.	02.1	54		27.8	.04		53 4	1 1	132.1	79.1	04		104.8		217.9	1
	-	02.6	11		28.3	05	90.1			132.9	79.7	05		105.4			131,0
-		-	-	-	28.8	-	-	-			80.2	_		105,9		_	131.6
6		03.1	56		1	106		54.5		133.8	80.7			106.4	11	220.4	1 -
7	A .10	03.6	- 12		29.3	08		55.0		134 7	81.2			106.9			132.6
8		04.1	58		30.3	11		56.0		136.4	81,7		179.3	1			133.1
10		05.1			5 30.8	11		56.5		137.2	82.2	11		107.9			133.6
-	-	-		13	-	-		-	-		32.7	211		168.4		-	
11		05.7		1-		111	1 . 3	57.0		138.1		11	11000	109.0			134.1
12		06.2		100	1-	24		57.0		138.9	83.8			109.5		224.	134.6
13	1	06.			0 32.4	11	90.	58.1	64	139.8	0			110.0			135.7
14		07.	. 6.		9 32-9	11		6 59.1		140.7	0 0		1 -	110.			136.2
15	-	07.	_	-	-	-			1	-	-		1	-		_	
16		7 68.			6 33.9					-	0 . 0			1111			136.7
17		603.		1 0	5 34-4	11 0	100.			1 . 3	04			1111.0	6	3229.0	137.2
18	1 2	4 09.	- 4	13	3 35.0	11		2 60.		1	00		1 -	8 112.0			137.7
19	1	3 09		1130	2 35.	· u		161:						7 113.			138.2
20	1-	2 10.	-	-	0 36.0	-11	-	9 61.			-	-	_	-	-1		-
21		0 10.			9 36.			8 62,	-					6 113.	11		4 139.3
22	18.	9 11.			8 37.		13	602.						4 114.			3 139.8
23	19.	7 11.	- 13	- 1 -	6 37.	11		5 63.			10			3 114,			140.3
24	20.	6 12.			.5 38.		106.			1	. 0	111		1 115.			0 140.8
25	21.	4 12.	9 7	5 04	3 38,	2		2 64.	-1	150.	1 89.		-	0 115.			9 141.3
26	122.	3 13.	4 7	6 65	.2 39.	1 12		1 64.	11	151.	0 90.			8 116.			7 141 8
27	123	2 13.	9 7	7 66	0 39.			9 65.			8 91.			7 116.			6 147.4
28	24	C 14	4 7		.9 40.	-11		8 65.		1 -		- 11 -		6 117.			4 142.9
29		0 14	- 11 0		.8 40.	-		6 66.	= 11 -					4 117.	7 7	9 239.	3 143.4
30	25	7 15	41 8	0 68	.6 41.	1 30	0 111	5 66.	8 80	154	4 92.	5 3	197.	-			2 143 9
31		6 15	9 8	1 69	.5 41.	6 13	1 112	4 67.	3 181	22		0 23	1 198.	1 118.			0 144.4
32	27	4 16			.3 42.		2 113	2 67.		1 3		- 11		0 119.			9 144.9
33	1-0	3 17	.0 8	3 71	.2 42.	7 3		1 68.	4 8:	157.	0 94.			8 119,	7 8	3 242.	7 145.4
34	1 29	2 17	28		.0 43.	2 3		9 68.		157.		- 11		7 120.			6 146.0
35	30	.c 18	0 8	5 72	-9 43	7 3	5 115	8 69.	4 8	158.	7 95.	1 3	5 201.	6 120.			4 146.
36	30	.9 18	. 5 8	6 73	.8 44.	2 13	6 116	6 69,	9 180	1 159.	5 95.	6 23	6 202.	4 121.	3 28	6 245	3 147.0
37	10	7 19	.0 8		.6 44.		7 117	5 70.		160.	4 96.	1 3	7 203,	3 121.	8 8	7 246.	2 147.
38	32	.6 19	.5 8	8 75	-5 45	2 3	8 118	4 70.	9 81	161.		6 3		1 122.	3 8	8 247	0 148.0
39	33	5 20	.0 8	9 76	-3 45	7 3	9 119	2 71.		162.	1 97.	1 3		0 122.	8 8	9 247.	9 148.
40	34	3 20	.6 9	0 77	.2 46.	3 4	0 120	.1 72.	9	163.			_	8 123		248	7 149.
41					.1 46.	8 14	1 120	9 72,	5 19	163.	8 98.	2 24	1 206.	7 123	9 29	1 249	6 149.
42	1 .	0 21	6 9	2 78	.0 47.	3 4				164.	7 98.	7 4	2 207.	6 124	4 5	2 250	4 15C.
43		9 22	1 9	3 79	.8 47.	8 4	3 122		5 93	165.	5 99.	2 4		4 124	9 9	3 251	3 150.
44		7 22	6 9	4 80	.6 48.	3 4	4 123	5 74	0 94	136.	4 99.			3 125	4 9	4 252	2,151.
45		6 23		5 81	.5 48.	8 4	5 124	4 74.	6 99	167.	3 100.	2 4	5 210	1 125	9 9	253	0 151.
46		5 23	- 1	6 82	.3 49.	3 14	6 125	2 75.	0 196	168.	1 100.	7 34	6 211	0 126			.9 152.
47		3 24	-		.2 49.									9 126	9 0	7 254	,7 152,
48	41	2 24	7 0	8 84	.1 50.									7 127		18 255	6 153.
49		c 25	2 9	9 84	9 50.	9 4	9 127.	8 76.	6 99	170.	7 102.	3 4	213	6 128		9 256	.5 153.
			11 2		010	- 11	1	1	11	1000	1	011-		10	11 -		
	42.	9 25.	7/10	0 85	.8 51.	4 1 1 5	0 128	7177.	1 200	171.	5 102.	8 2 5	214	41128	5 3	00 257	3 154.
50	42.	9 25.	7 10	0 85	.8 51.												3 154. Lat

for 5 4 Points.

Difference of Latitude and Departure for 3 Points. 69

24			II.		Dayl	D:6	Lat	De	Diff	I La:	Dep	Dia	Lat.	Dep	Dif	La:	Dep
Dit	-	Dep	-	Lat	-	-			-	-		-	-	-	-		-
1	00.8	00,6	51	42.4		101		56.1	151	125.5	83.9	201	167.1			208.7	
2	01.7		52	+3.2		02		56.7	52	120.4	84.4	02	167.9	112.8		209.5	1
3	02.5		53		29.4	03		57.2 57.8	53	127.2	85.5			113.3	1 33	210.3	
4		02.2	54	44.9	30.6	04		58.3	55	128.9	86			113.9	54	211.2	
_5	-	02 8	55	45.7				-			86.7	-	_		-		
6		03 3	56	46.6	,	105	88.1		155	129.7	87.2	11	171.3	1144	256	1	142.2
7 8	. /	03.9		47.4	000	08		60.C	57	130.5	87.8		172.1		57	213.7	
12/1	10000	05.0		49.1		09		60.5	59	132.2	88.3			116.1	59	215.3	
9		05.6	60	1 1 1 1 1 1 1	33.3	10	91.4	10-	60	133.0	88.9	10		116.7	60	216.1	144.4
-		06.1	6:			111	02.2	61.7	161	133.8	89.1		175.4	117,2	261	217.0	145.0
11		06,7	1 -	51.5	33.9	12	93.1	52.2	62	134.7	90.0	12		117.8		217.8	
13		07.2	63	52.4		13		62.8	63	135.5	90.5	13		118.3		218.6	
14		07.8	64		35,6	14		63 3	6.	136.3	91.1		177.9			219.5	
15		08.3	65		30.1	15	95.6	03.9	65	137.2	91.7	15	178.7	119.4	65	220.3	
16	12.2	08 0	66	54.9	30.7	116	96.4	64.4	165	138.0	92.2	216	179.6	120.0	266	221,1	147.8
117	14.1	09.4	67	55.7	37.2	17	97-3		67	138.8	92.8	17				222.0	148.3
15	1	10.0	68	156.5	37.8	18	98,1			139.7	93.3	18	181.2	121.1	68	222.8	148.9
19	15.8	10,6	69	57.4	38.3	19	98.9	66.1	69	140.5	93.9		182.1			223.6	
20	16.5	11.1	70	58.2	38.9	20	99.8	66.7	70	141.3	94.4	20	182.9	-	70	2:4.5	150.0
21	17.5	11.7	71	59 0	39.4	121	100.6		171	142.2	95.0		183.7	122.8	271	225.3	150.5
22	18.3	12.2	72	59.9	40.0	22	101.4	67.8	72	143:0			184.6		72	226.1	151.1
23	19.1	12.8		60.7	40.6	23	102.3	68.3	73	143.8	96.1		185.4	123.9		227.0	
24		13.3	74	61.5	41.1	24	103.1		74	144.7	96.7		186,2	124.4		227.8	-
25	20.8	13.9	75	62.4	41.7	25	103.9	_	75	145.5	97.2	25	187.1		75	228.6	152.8
26	21.6	14.4	76	63.2	42.2	126	104.8		176	146.3	97.8	226	187.9			229.4	153.3
27	1	15,0		64.0		27	105.6		77	147.1	98.3			7135	77	230.0	
28	23.3	1 3		64,8	100.0	1	106.4			148.0		28	189.5			231.1	
30		16.7		66.5	43.9	11	107,2		79	149.6	99.4	1 11	190.4		30	232.8	155.0
	1-	-	-	-	_				-	_					-	-	
31	25.8			67.3	45.6		108.9				100.5		192.0			233.6	
32		17.8			45.1		110.6				101.7		193.7		0.	234.4	-
34	28.3		84		46.7	34	111.4	74.4	84	153.0	102.2		194.5		0.	236,1	157.8
35	29.1		85	70.7		35	112.2	75.0	85	153.8	102.8			130.5		236.9	
36	29,9	-	86	71.5	47.8		113.1	75.8			103.3	236	196.2	131.1	286	237.8	158.0
37		20.6	87		48.3	27	777.0	76.1	87	155.5	103.0	37	197.0	131.7	87	238.6	
38	1 .	21.1	88		48.9	38	114.7	76.7	88	156.3	104.4	38	197.9	132,2	88	239.4	160.0
39		21.7	89	74.0	49.4	39	115.6	77.2	89	157.1	105.0	39	198.7	132.8	89	240.3	160.5
40	33.3	22.2	90	74.8	50.0	40	116,4	77.8	90	158.0	105.5	40	199.5	133.3	90	241.1	161.1
41	34.1	22.8	91	75.7	50 6	141	117.2	78.3	191	158.8	106.1	241	200.4	133.9	291	241.9	161.7
42		23.3			51.1	42	118.1	78.9	92	159.6	106.7	42	201.2	134-4	92	242.8	162.2
43		23,9			51.7	43	118.9	79.4	93	160.4	107.2	43	202.0	135.0	93		162.8
.44		24,4			52.2		119.7	80.0	94	161.3	107.8	44	202.8	135.5	94		163.3
45		25.0	95	79.0	52.8		120.5				108.3		203.7				163.9
46		25.6	96	79.8	53.3	146	121,4	81.1	196	162.9	108.9	246	204.5	136.7	296	246.1	164.4
47	39.1	26.1	97	80.6	53.0	47	122.2	81.7	97	163.8	109.4	47	205.3	137.2	97	246.9	165.0
48		26.7	98	81.5	54-4	48	123.0	82.2	98	164.6	110.0	48	200.2	137.8	98	247.7	165.5
		27.2	99	82.3	55.0	49	123.9	82.8	99	165.4	110.5	149	107.0	138.3	99	248.5	166.1
20	41.0	27.8	100	83.1	55.6	150	124.7	83.3	200	100.3	111.1	30	207.8	138.9	300	149.4	166.7
Lin	Dep	1J.at	Dia	Dep	Lat	Diff	Dep	Lat	HDIH	Dep.	Lat	Diff	Dep	Lat	Dis	t Dep	' Lat
	100	1				7 1 1/2		100	1 1 1		1 5 1 1 1		194				

for 5 Points.

70 Difference of Latitude and Departure for 34 Points.

DI	La	Der	Dit	t La	Der	nD:	Lat	IDe:	IID:	Tat	Den	(Diá	1 [D-	10		
	00	8 00.6	51	-	0 30.				-	-	-	-	-		Dil	Lat	Del
		6 01.2	11 3		8 21.0			60.	1.3.			11		119,7		201.6	
3	1	401.8	11 3		6 31.6			61.4	11 3		1	11		120.3	11	202.4	
4	12.00	02.4			4 32.1	1 3		62,0	1 33	122.9		11 3		120.9	11	203,2	
5	04.0	003.0				. 11	1 0	62.6	1		91.7		163.8	1	1 24	204.0	
6		03.6			-	-11-			-	124.5	92.3	05	164.6		1 -33	204.8	151
7		04.2						63.1		125.3	92.9	11	165.4		256	205.6	152
8		04.8		45.	34.6	08		63.7		126.1	93-5		156.2	33	57	206.4	
9		05.4					,/	64.3		126.9	94.1	08	167.0		58		
10		06.0			35.1			64.9	11 2 -	327.7	94.7	09		124.5	59	208.0	154
11		-			33.1	10	-		60	128.5	95.3	10	168.6	125,1	60	208.8	154
12		06.6			36.			66.1	161	129.3	95.9	211	169.4	125.7	261	209.6	
13		07.1		177	36.9	1		66.7	62	130.1	96.5	12	170.2	126.3	62	210.4	
14		08.3		-	1	11		67.3		130.9	97-1	13	171.0	126.9	63	211.2	
15		08.0			38.1			67.9	64	131.7	97.7	14	171.8	127.5	64	212.0	1 57
-	_	-			30,7	1	92.4	68.5	65	132.5	98.3	15	172.7	128.1	65		157
16		09.5		133.	39-3			69.1	166	133.3	98.9	216	173.5	128.7	266		
17		10.1	1 40	53.8	39.9			69,7	67	134.1	99.5	17	174.3	129.3	67		
77		10.7		54.6	40.5	11 3	94.8	70.3	68	134 9	100.1	18	175.1	129.9	68	215.2	150
19	15.3			55,4	41.1	19		70.9	69	135.7	100.7	19	175.9	130.5	69		160
10	_	11.9	-	56.2	41.7	20	96.4	71.5	70	136.5	101.3	20	176.7	131,1	70		160
21		12.5		57.0		121	97.2	72.1	171	137.3	101.0	22 I	177-5	131.7	2.71		-
22		13.1	72	57.8		22	98.0	72,7	72	138.1		22	178.3	132,3	72	217.6	
23	7	13.7	73	58.6	43.5	23	98.8	73.3		138.9			179.1		73		
24		14.3	1 2 2	1	44.1	24	99.6	73.9	74	139.7	103.7		179.9			220.0	
25	20.1	14.9	75	60.2	44.7	25	100.4	74-5	75	140.5	104.3	25		134.0		220.8	
26	20.9	15.5	76	61.0	45.3	126	101.2	75.1	176	141.3		226	181,5				_
27	21.7	16.1	77	61.8	45.9	27	102.0	75.7	77		105.4		182.3	134.6		221.6	
28	22.5	16.7	78	62.6	46.5	28	103.8	76.3	78	142.9			183.1	125.8		222,4	
29	23.3	17.3	79		47.1	29	103.6		79	143.7			183.9			223.2	
30	24.1	17.9	80	64.2	47.7	30	104.4	77-4	80	144.5			184.7	137.0		224.8	
31	24.9	18.5	81	65.0	48.3	131	105.2		181		107.8				1		_
32	25.7	19.1	82		48.0	32	106.0		82	146.2			185.5	137.6	281	225.7	
33	26.5	19.7	83	66.7	49.4	33	106.8		83	147,0			186.3		82	220.5	
34	27.3	20.3	84		50.0	34	107,6		84		109.6					227.3	
35	28.1	20.9	85	68.3	50.6	35	108.4		85	- 0 4	110.2		187.9				
36	20.0	21,4	86	69.1	CI.2	136	100.2		186						-04	228.9	109
		22.0	87	69.0	51.8	37	110.0	81.6	8-	150 2	110.8	1 22		140.6	0_		170
		22.6	88	70.7	52.4	38	110.8	82.2	88	150.2	112.0	981	190.3	41.2	87	230.5	171
		23.2	89	71.5	53.0	39	1116	82.8	80	157.8	112.6	30	91.1	141 8	88	231.3	171.
10		23.8	90	72.3	53.6	40	112.4	83.4	00	152.6	112.2	40	191.9	144.4		232.1	172.
11		24.4								152.6	-3.5		92.7	-+3.0		232.9	
		25.0			54.2	42	113.2	84.6	191	153.4	113.8	241	93.5	143.6	291	233.7	173
12 1		25.6			54.8 55.4	7-	114 0	04.0	92	J 54.21	114.4	421	194.3	144.2	92	234.5	174
4	35.2	26.2	94	75.5	56.0	44	114.8	8 5 9	93	55.0	115.0	43	195.1		93	235.3	174
5		26 8		76.2	56.6	45	116	86		155.8	115,0		1959	145.4	94	236.1	175.
-		_					116.4	00.2	95	156.6	110.2	45	196.7		95	236.9	175
7		27.4	96		57.2	140	117.2	87,0	196	157.4	16.8	246	197.5	146.6	296	237.7	176
		28.0		77.9	57.8	4/	118.0	07.0	97	158.2	117.4	47	198.4	147.1	97	238.5	176
		28.6		78.7	58.4	48	118.8	88.2	08	150.0	118.0	48	100.2	147.7		239.3	177
19	39.4	29.2	99	79.5	59.0	49	119 7	8.8	00	1 50.811	118.6II	40	10.00	142 -		240.1	178
0	40.2	29.8	100	80.3	59.0	150	120.5. Dep	89.4	200	160.6	10.1	250	18.00	148.9	300	240.9	178.
2.42														1			,

for 4 3/4 Points.

Dia	Lati	De.	D:1	t/La	1 1	Devi	D.al	Lat	Dep	Dn	Lat	Dep	Din	Lat	Der	Ditt	Lat	Dep
_		00 6	-	39.			101		64 0	-	116.7	95.8	201	155.3	127.5	251		159 2
1	100	01.3	-	40.			02	78.8			117.5	46,4			128.1	52		159.8
2		01.9		41.			63		65.3		118.2	97.0			128.7	53	7.1	160 4
3 4		02.5		41.			04	80,4	1	54	119.0			157.6		54	196.3	
5		03.2	11	42,		12	05	81.1		55	119.8	98.3	05	1584	130,0	55	197.1	161.7
6	_	03.8		43.	_	_	10t	81.9	67.0	156	120.6	98.9	206	150.2	130.6	256	197.8	162.3
7		04.4		44			.07	82.7		57	121.3	99.6			131,3	57		163.0
8		05.1		44			c8	83 5			122.1	100.2	08	160 7	131.9	58		163.6
9	07 0	05,7	55	45.	6 3	7.4	09	84.2				100.8	09	161.5	1 32.5	59		164,2
10	07.7	06.3	60	46.	43	8.0	10	85.0	69.8	60	1236	101,5	10	162.3	133.2	60	200.9	164.9
11	08.6	07.0	6:	47.	1 3	8.7	111	858	70.4	161	124.4	102.1	211	163.1	133.8	261	201 7	165.5
12		07.6		47	9 3	9 3	12	86.6	71.0		125.2	102.7	12	163.8	134.4	62	202,5	166.1
13	10.1	08.2	6	48.			13	87.3			126.c	103.4	13	164.6	135.1	63		166.8
14	10 8	08.9		49	5 4	0.6	14		72.3			104.0	1	- 7	135.7	64		167.4
15	116	09 5	6	50,	,2 1	1.2	15	88 9	72.9	65		104.6	15	160.1	136.3	65	204.8	168.0
16	12.4	10.1	6	51.	.04	11.9	116	89.6	73.6	166		105 3			137.0			168.7
17		10,8		51.			17		74.2			105 9			137.6			169.3
18		11.4		52			18		74,8			106.5	1 1 1 12		138,2			170.0
19		12.0		53			19		75.5			107.2			138.9			170.6
20	-	12.7		-	_	14.4	20		76.1		_	107.8			139.5	-	208.6	171.2
11		13.3				15.0	121		76.7	171		108.4			140 1	27.1		171.9
22		14.0		2 55			22		77-4	72		109.1	22		140,8			172.5
23		14.6		3 56			23	95.1	78,0	73		109.7	1 2 2		141.4		16 213 3	173.1
24		15,2		4 57	2	10.9	24		78,6			110.3	24		142.0			173.8
25		15.9		-	-	47.6	25		79-3	75		111.0	25	_	142.7			174,4
26		16.		6 58			126		79.9			111.6	226		143.3			175.0
27		17.1		7 59			27		80.5			112,2	27		144.0		214	
18		18.		8 60 9 61			29		81.8			112.9	29		144 6			176.9
30		19.0		061			30	100.5		80		114.1	30	177.7				
-		-	1	_	-	-	_			181				178.	-	11-	-	-
31		19,				51.4	131	101.2			139.	114.8	32		147.1	11 0	217.	178.2
32		20.				52.6	33	102.8			141.	116.0			147.8			179.
34		3 21				53.3	34	103.6				116.7	34		148.4			5 180.
35		1 22.				53,9	35	104.				117.3	35		6 149.0			180.
36	-	8 22.				54.5	136					7 118.0	_	-	149.7	-		181.
37		6 23.				55.2	37	105.0				5 118.6		182.	1 150.	87		8 182.0
38		4 24.	1 8	8 68	0	55.8		106.				3 119.2			9 150.	-		6 182.
39		1 24.	7 8	9 68	,8	56.4	39		88.	89	146.	1 119.9	39	184,	7 151.	89	223.	3 183.
40		9 25.	4 9	c 69	.6	57.1	40	108.	88.8	90	146,	8 120.5	40	185.	5 152.	2 90	224.	1 183
41	31.	7 26.		_		57-7	141	109.	89,4	191	147.	6 121.1			2 152.		224.	9 184.
42	32.	5 26,	6 9	2 71		58.3					148.	4 121.8	42	187,	0 153.	5 9		6 185.
43	33.	2 27.	3 9	3 7	1.9	59.0	43	110.				1 122.4	43	187.	8 154.	1 9		4 185.
44		0 27	9 9	4 72	2.6	59.6					149	9 123.0	44	188.	6 154.	7 9		2 186.
45		8 28.				60.2			1 92.		150	7 123.	45	189.	3 155,	4 9		0 187,
46		6 29.				60.9		112.	8 92.			5 124.		190,	1 156.	0 29	6 228	7 187
47	36.	3 29.	8 9	7 7	5.0	61.5	47	1113.	6 93.	2 9	7 152	2 124.	9 47	190	9 156.	6 9	7 229	5 188
48	37-	1 30.	4 9	8 7	5,7	62.1	1 48	114.	4 93.	9 9	8 153	.0 125.	6 48	191.	6 157.	3 9	8 230	.3 189
49	37.	9 31.	1 9	9 7	6.5	62.8	49	9 115.	1 94,	5 9	9 153	.8 126	2 49	192.	4 357	9 9	9 231	.1 189
5	38.	6 31.	7 19	7	7.3	63.4	150	115	995.	1 20	0 154	6 126.	8 250	193	2 158	5 30	0 231	.8 190
Di	00	. 1	·In	AT	1	Lat	IID.					La						p La

72 Difference of Latitude and Departure for 3 3 Points.

13.	Lat	De	1.13.4	1/1 0	Dep	10 0	Lat	Dan	H13 4	Lat	IDan.	nDid	Lar	Dan	Ditt	TTar	1 Charte
D11	Lai	De	1011	La	Det	1	-	-	11-	-	-	-			1-	Lit	Dep
,	00.7	00.7	51	37.	34.2	101	74.8	67.3	151	111.9	101,4	101	148.9	135.0	251	135.9	168.5
2	01.5	01.3	52	38.	34-9	02	75.0	68 5	52	112.6	102.1	02	149.6	135.6	52	186.7	169 2
3	02.2	2.0	53	39.3	35 6	03	70.3	69.2	53	113.3	102.7	03	157,4	136.3	53	187.4	169,9
4	03.0	02.7	54	40.0	36.3	04	77.0	69.8	54	114 1	103.4	04	151.1	137.0	54	183.2	170.5
5	03.7	03.4	55	40.7	36.9	05	77.8	70.5	55	114.8	104.1	05	151.9	137.6	55	188.9	171.2
6	OA A	04.0	56	AL	37.6	-	78.5	71.2	156	115.6	104 7	206	1526	138,3	256	189.6	_
-		04.7			38.3		79.3	71.8	57		105 4	07		139.0	57	190.4	7
8	-	05.4			38.9		80,0	72.5			106.1			139.7			1732
9		06,0	11	1	39.6	-	80.7	73.2	59		106.8	1	154.8	10.00	59	191.9	
10		06.7	60		40.3	10	81.5	73.9		118.5		10		141,0	60	1	174,6
-	1	-	-	1	-	-	-	-	-		_	-	-	4.,0	-	192.0	17450
11		07.4	61	143.	41.0	111	82.2	74.5	161	119.3		211	150,3	141.7	261	19.3.3	175.2
12		08.1			41.6	12	83.0	75.2	62		108.8	12	157.0		62	194.1	
13		08.7			42,3	13	83.7	75.9	40	120.7	109.4			143.0		194.8	
14		09.4			43,0		84.4	76.9		121.5		14	158.5	143.	04	195.6	177.3
15	11.1	10.1	05	48.2	43.6	15	85.2	77.2	65	122.2	110 5	15	159.3	144.4	65	196.3	177.9
16	11 9	10,7	66	48.9	44.3	116	85 9	77.9	166	123.0	111.5	216	160.0	145.0	265	197.0	175.6
17	12.6	11.4			45.0	17	86.7	78,6		123.7		17	160.7	145,7	67		179.3
18	13.3	12.1	68	50,4	45,7	18	87.4	79.2	68	124.4	112.8	18	61.5	146.4	68	198.5	179 9
19	14.1	12.8			46.3	19	38.2	79.9	69	125.2	1	19	162.2	147.0	69	199.3	180 6
20	14.8	13.4	70	51 9	47.0	20	88 9	80.6	70	125.9	114.1	20	163.0	147.7	70	200.0	181.3
21	15.6	14.1	71	52.6	47.7	121	89.6	81.2	171	126.7	114.8	221	163.7	148.4	271	200.7	182.6
22	1 2	14.8			48.3	22	90.4	81.9	72	127.4			164.4	140.1	72	201 5	
23		15,4		54.1			91.1	82 6	73		116.2	23	165.2	140.7	73	20:,2	-
24		16.1			49.7	24	91.0		74	128.9		24	165,0		74		184.0
25	18.6		4.7.3		50.4	25	92.6		75		117.5		166.7		75		184.6
26	-	-	76		-	126	-	-			-	-	-	-		-	
	19.3		100		51.0		93.3	84.6	176	130.4		120	167.4		276	204.4	
27		18.8	77		51.7	27	94.1	85.3 85.9	77	131,1	7		168.2		77		186.0
29	Biograffy.	19.5			53.0	29	94.8	000		131.9				0	79	205.9	
30	1	20.1	80				95.6	87,3	80	133.6	3	30	170.4	153.8	80	207.4	
-	-	_	-	3273		30		_	_	133.3	-	-			-	-	-
31	23.0	2 4 7			54-4	131	97.0	88.0			121.5		171.1		181		
32	23.7			60.7		32	97.8	88.6	82	-	122.2		171.9		82	208.9	189.3
33	24.4	- 0		61.5		33	98.5	89,3	-	135.6		33	172.6	150.4	83	209,6	190.0
34	25.2			62.2	10 .	34	99.3	90.0	84	136.3		34	173.3	157.1	84	210.4	190.7
35	25.9	23.5		63.0		35	100.0	90.6	85	137.0	124.2	35	174.1	157.8	85	211.1	191.4
36	26.7	24.2		63,7		136	100.7	91.3	186	137,8	124.9	236	174.8	158.5	186	211.9	192.0
37	27.4		1 87	64.4	58.4	37	101.5	92.0	87	138.5	125.6	37	175.6		87	212.6	192.7
38	28.2	25.5	88	65.2	59.1		102.2				126.2	38	176.3	159.8	83	213.3	
39	28.9	26.2			59.8		103.0		89	140.0	126.9	39	177.0	160.5	89	214.1	194,0
40	29.6	26,9	90	66,7	60.4	40	103.7	94.0	90	140.7	127.6	40	177.8	161,1	90	214.8	194.7
41	30.4	27.5	91	67.4	61.1	141	104.4	94,7	101	141.5	128.2	241	178.5	16118	201	215,6	195.4
42	31.1				61.8		105.2				128.9			162.5		216,3	
43		28.9			62.4		105.9				129.6			163.2		217.0	
44	32.6			69.6			106.7				130.3			163.8		217.8	
45	33.3				63.8		107.4		95		130.9	45	181.5		95	218.5	
46	34.1				64.5		108.2	_			231.6		_	165.2	-		
47	34.8	21.6	97		65.1		108.9				132,3			165,8		219.3	
48	35,6	22.2	08		65,8		109.6				132.9			166.5		220,0	
	36.3	22.0			66.5		110.4							167.2		221.5	
50	37.0	22.6	190	74.3	67.1	150	111.1	100.0	39	148 0	124.2	350	186.2	167.2	100	222.2	
																-	-
DIR	nebl	Lat	DIN	Inet	Lat	Dill	Dep	Lat	חות	Dep	Lat	Dep	Lati	Lat	LIVIE	Dep	Lat
1931		F 1: 17.		1764.73	17 x 1	1 50	ar in the	the said	1 1 1 1	61 Tay	10 TE 14	1388-1	19194	110	41.5.71.	1 1 1 7 3	

for 4 4 Points.

Difference of Latitude and Departure for 4 Points. 73

	7	n	· N. I	7:A:1	97 1	Dep	Die.	Lat	Den II	Diffi	Lat	Den 1	Dirt	Lat	Den	Diff	Lai	Dep
Diff	-	-	-11-	-	_				7		-		-			_	-	
1	00,7	1			6.1	36.8	101	714	71,4		106.8			142.1			177.5	177.5
2	OF.4					37.5	03	72,1	72.0	52	107.5		02	143 5	142.6	53	178.4	178.2
3	02,8		o.H			38.2	04	73.5	73.5	54	108.0		04	144.1	144.2	54	179.t	179.0
4	03	21	5			38.9	05	74.2	74.2	55	109.6	109.6	05	144.9	144.9	55	180.3	
5	01.2	2.1	- -		_	39.6	100	74.9	71.9	156	110.3	110,3	206	145.7	145.7	256	-	131.0
6	04	1. :				43.3	07	75.7	75.7	57	1110		07	146.4	146.4	57	181.7	181.7
7 8	05.		7	-	41.0	410	03	76.4	76.4	58	111.7	111;	03	147.1	147.1	58	182 4	132 4
9	06	1 06	+4	59	41 7	41 7	oy	77-1	77.	59	112,4	112.4	09	147,8	147.8	59		183 1
10	07	137		00	42.4	42 4	10	77.8	77.3	60	113.1	113.1	10	148.5	148.5	60	183.8	123 8
11	07	1 2		- 1		43.1	111	78.5	78.5	161	1138	113.8	211	149.2	149,2	261	184.5	184 5
12		5 38	11	- 1	43.3	43.8	12	79.2	79.2		114 5	114,5	12	149.9	149 9	62	185.5	
13	1-	2 09	- 11	63	44 3	44.5	13	79,9	79.9 80.6	63	115.3		13	150.0	150,0	64	1.44	186.0
14	Ib.	9139	0.6	1	40 D	46.0	15	81.3	81.3	65	116.7		15	152.0	152.0	65	137.4	187.4
15	11		-1	66	46,7	46.7	116	82.0	32.0	166	117 4	117.4	-	152.7	152.7	266	188.1	
16	12	-	.3	67	47.4		17	82.7	82.7	67	118.1	118,1	17	153.4	153.4	67	188.8	
18	12.				48 1		18	83.4	83.4	68	118.8				154,1	68		199.5
19	1.3.	4 1	3.4	69	48 8	48,8	19	84.1	84.1	69	119.5	119.5	19	154.8		69		190.2
20	14	1 14	.1	70	19,5	49.5	20	84 8	84.8	70	120 2	120.2	20	155.6	155.6	70	190.9	190 9
21	14	8 14	4.8	71	50.2	50 2	121	85.6	85.6		120.9	120,9	121		156.3	271	191.6	191.6
22	15.	6 1	5 6	72		50.9	22	86.3				121.6	22	157 0	157.0	72	192.	192.3
23		3 1		73		51,6		870				122.	1	- 0 .	1 9 .	73		193.0
24		91		74	53.0	52.3	24	87.7			123.0			150.4	158.4			193.7
25		7		75				-	-	-						75		194.4
26	1		8.4	77	54.4	53-7		89 8			124.	Thirtie		1-6-	160.5		1	195.2
27		8 1		78	55.		11							1-6-	1-6-	78	195	195.9
20	1	,5 2	-	79	55.	55-9	29							1.6-	161,9	11	197.	
30	1	-	1.2	80	56.	56.6	30	91.9	91.	80	127.	127.	3 30	162.6	162.6	8		198.0
3	-	9 2	1.9	31	57-	3 57-3	131	92.6	93.	181	128.	128	231	163.	163.3	281	198.	198.7
3		.6 2	2,6			58.0			93	3 82		7 128.	7 32	164.0	154,0	11	199.	199.4
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3	8 26	.3 2			10	2 52.						9 132.			3 168.			6 203.6
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		3 2			10	6 63.	40		99.		134.	3 134	3 4	169,	7 169.	90	205.	1 205.1
		0	_	-		3 64.				7 19	135	1 125	1 24					8 205.8
		.7		92	105.	1 65,	1 42		100.	4 9	1 35	135.	811 4	2 171.	1171.	1 92	206	5 206.5
		.4		93	65.	8 65.	8 43	101.	101.	1 9	3 130.	5 136.	5 4	3 171.	8 171.	93	207.	2 207.2
		1.1			100.	5 66.	5 44		101.		4 137	2 137.	2 4	4 172.	5 172.	5 94		9 207.9
		1.8				2 67.	_		5 102.			9 137.			2 173			6 208.6
		1.5			167	9 67	9 146	103.	103.	2 19	138.	6 138.	6 24	6 173.	9 173.			3 209.3
4	7 3	.2	33.1	97	60	0 68,	47	103.	9 103,	9 9	7 139	3 139.			6 174,			0 210,0
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/5				Y	Tea	r	17	66					ys				Y	ea	r	17	67				
Month Days	January	February	March	April	May	June	July	Auguff	September	October	November	December	Month Days	January	February	March +-	April "	May	June	July	Auguft	September	October	November	December
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56 78	33 34 35 36	37	34 35 36 37	37	36 37 38	37 38	38 39 40	39 40 11	11 12 13	11 12 13		13 14 15 16	5678	17	17 18 19 20	17	17 18 19 20	20	20	21	22	24	23 24 25 26	25 26 27 28	2 2 2 2 2
91011	39	39	38	39 40 11	40	11	13	13 14 15 16	17	15	19	17 18 19 20	910	21	22	21	23	23	24	25 26	26	27 28 29 30	25	32	3 3 3
13	11 12 13 14	13 14 15 16	13 14 15	13 14 15 16	16	16	16 17 18	119	21	20 21 22	22	22	13 14 15	24	1	25	26	27	28	30	3c 31 32	31 32 33 34	31 32 33 34	33 34 35 36	3 3 3
17	17	19			19	20	21	2:	2 2	2 2 3 4 2 4 5 2 5 6 2 6	25	26	17	28	13-	30	30	30 31 32 33	31 32 33 34	34	34	35 36 37 38	37	37 38 39 10	3 3 4
21 22 23 24	21	23	21	23	23	24	26	2	2	28	30	30 31 32		33	33 34 35 36	-	1	34 35 36 37	35 36 37 38	37	39	39 40 11	4C	13	1 1 1 1
25 26 27 28	21	26	25	26 27 28	25	28	29	3	13	3 3 3	34	33 34 35 35 36	27	37	37 38 39 40	37 38 39	38 39 40	39	40	11	112		14	17	
30	27 28 29		28 29 30	30	30	132	33	13	3 3 4 3 5	37	37	37 8 38 39	130	39	1	111	12	13	13	15	110	17	17	20	2 2

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Month Days	January	February	March	April	May	June	July	Augutt	September	October	November	December	Month Days	January	February	March	April	May	June	July	August	September	October	Nevember	Tecember
1 2 3 4	22 23 24 25	26	24	25	26	27	27 28 29 30	30	31	31	33 34	33	1 2 3 4	35	36	35	35 36 37 38	37 38	38 39	39 40	40	12	12	14	I
7	27		28	29	3132	32 33	31 32 33 34	33 34 35	35 36 37	35 36 37	37 38 39	37 38 39	5 6 7 8	39	40	39	39 40 11	11	12	13 14 15	13 14 15 16	15	15 16 17 18	17 18 19 20	1 1 2
	30 31 32 33	33	32	34	3 34 39 36 36	35	35 36 37 38	37 38 39	39 40	39 40 11	11	11	111	13	14	13	13 14 15 16	15	16	17	18	20 21	20	22	2
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1	8 30	1 6	2 1	1 1	1 1 2 1	2 1 3 3 L 4	1 1 3 1 4 1 5 1 6	15	18	17	19	18 19 20 21	17	21	22	21	21 22 23 24	23	24	25 26	26 27	28	28	30	3
2	2 1	2 1. 3 1 4 1 5 I	61	4 1	51	71	5 17 7 18 8 19 9 20	19	21	21	23	2 2 2 3 2 4 2 5	21 22 23 24	24	20	25	25 26 27 28	27	28	29 30	30	32	3 z 3 3	34	13
2 2	5 I 6 I 7 I	0 1 7 1 8 2	91	9 2	8 I 9 2	y 2 C 2 1 2	0 2	2 2 3 3 2 4	24	24	26	26 2/ 28 29	27	20	3	30	31 32	31	32	32 33 34	33 34 35	35 36 37	35 36 37	38	3
2	9 2	0 2	2 2		2 2 2		4 2 5 2 2	5 20	28	-	30	-	30	3:	2	33334	33	34	35	36	37	39	39	11	1

ays				Y	ea	r	17	70	•				Days				Y	ea	r	17	71.				
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5678	18	20 21 22	19 20 21	20	21 22 23	22 23 24	23	24 25 26	26 27 28	26 27 28	30	28 29 30 31	5 6 7 8	29 30 31	30 31 32	25 30 31	29 30 31	31 32 33 34	33 34 35	33 34 35	35 36 37	37 38 30	38	39	3 4 1
10	24	25 26 27	25	25 26 27	26 27 28	27 28 29	30	29 30 31	31 32 33	31 32 33	33 34	33	91011	33 34 35	34 35	33 34 35	33 34	35 36 37	37 38 39	37 38 39	39	11	11 12 13 14	13	1 1 1 1
14	27 28 29	30	28 29 30	30 31	30 31 32	31 32 33	32 33	33 34	35 36	35 36	37 38	38	13 14 15 16	38	39	38	38	39 40 11	11	11	13	15	16	19	1
	31	32 33 34 35	33 34	33 34 35	34 35 36	35 36 37		37 38	39 40	39 40	11	iı	17	11 12 13	12	11 12 13	11	13 14 15 16	15 16 17	15 16 17	17 18	19 20 21	19 20 21	21	1 24 23
4	37	36 57 38 39	36 37 38	39	38 39 40	39 40 11	12	11 12 13	15	14	16	14 15 16	23	17	17	16	15	17 18 19 20	19 20 21	19 20 21	21 22 23	23	23	26	2
7 8	39 40 11	11	11	12	12 13 14	13 14 15	14 15 16	15 16 17	17	17 18 19	19 20 21		25 26 27	19 20 21	20 21 22	19 20 21	19 20 21	21 22 23 24	23 24 25	23	25 26 27	27	27	30	2 3 3
0	13		13	14	15 16 17	17	17	19	21	2C 21 22	23	22 23 24	30 31	23 24		23	22	25 26 27	27	27	29	3 1	2 1	33	2

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56 78	10 11 12 13	13	11 12 13 14	13 14 15	13	14 15 16	14 15 16	15 16 17 18	17 18 19 20	19 20 21 22	20 21 22 23	21 22 23 24		7	22 23 24 25	24 25 26 27	22 23 24 25	23 24 25 26	24 25 26 27	25 26 27 28	25 20 27 28	27 28 29 30	28 29 30 31	29 30	31	١
910	14 15 16	19		18	17 18	20	19 20 21	20 21 22	22 23 24	24 25 26	25 26 27	26 27 28		1 2	29	28 29 30 31	26 27 28 29	27 28 29 30	28 29 30 31	29 30 31 32	29 30 31 32	31 32 33 34	33 34 35	35 36	35 36 37 38	
14	21	20 :1 22 23	21	22	21 22 23	23 24 25	24 25	25 26	27 28	28 29 30	30	32	;	-	33	33 34 35	31 32 33	31 32 33 34	33 34 35	34 35 36	34 35 36	35 36 37 38	37 38	-	10	4 1
18	23 24 25	27	26	26 27	27	27 28 2	28	28 29 30	31	32 33	35	35 36	2	9	35 36 37	37 38 39	36 37	36 37 38	37 38 39	38 39 40	38 39 40	4C	12	12	15	1 1 1
23	28	29 30 31	29 30	29 30 31	31	31 32 33	32 33	37 33 34	35	37 38	37 38 39	-	2 2	3 4	39	-	10	10	121	13	12	15 1	6	17 1	9	-
26	30 31 32 31	33 34 35	32 33 34	33 34 35	33 34 35	34 35 36 37	35 36 37	36 37 38	38 39 40	40 11 12	11	13	2 2 2	7 1 8	5 1	16	5 1	5 1	5 1 6 1 7 1	7 1 8 1	161	5 2	9 2	2 2 2	3 2 4 2	2 2 2
30	34 35 36	30	35 36 37	36 37	37 38	38 39	39	39 40	13	14	15	15	3	91	17	1	7 1 8	8 1 2	9 2	9	20 2	2 2 2		3 2 4 2 5	6 2	

AT	ABLE	of	Num-
	bers,	8°c	•

A TABLE answering to any of the foregoing Numbers.

Num- bers	Т	imes anf	wering.
	H.	M.	
11	0-	48)
12	1-	36	I
13	2-	24	
14	3-	124	
15	4-	00	
16	4-	48	
17	5—	36	Afternoon
	3 7 25 7	24 12	, intermoon
19	7 -	00	•
21	8	48	
22	9-	36	
23	10-	24	
24	11-	12	
25	12-	00]	
			•
26 27	o— 1—	48 36	
28	2-	-24	
29	3-	12	
30	4-	00	
31	4	48	Contract of
32	5-	36	After
33	6-	24	Midnight
34	7-	12	8
35	8	-00	
36	8—	48	
37 38	9-	36 24	
39	11-	12	
40	12-	-00	

The Use of the foregoing Tables of Numbers.

In these Tables, each Page is divided into two Parts, by a double Line drawn down the Middle; and each of the Parts are marked at the Top with the Year for which they shew the Numbers, and under that, the Lest-hand Column of each Part is marked with the Days of the Month, and the other Columns with the Months of the Year: So that if you would know the Number for any Day, suppose for Example, on the 20th of March, 1766.

First, Find the given Year 1766, at the Top of the Table, and then under the given Month, which is March, and right against the given Day of the Month (which in this Case is 20) you will find the Number 19, which is the Number for that Day; and if from the Number so sound you subtract 10, the Remainder will be the Moon's Age

for that Day.

The Use of the Table of the Times answering to the foregoing Numbers.

In this Table the Left-hand Column is mark'd with the given Numbers from 11 to 40, and the Figures right against any of these Numbers, give the Time answering to it, in Hours and Minutes.

EXAMPLE I.

I would know what Time answers to the Number 23?

Answer. 10 Hours 24 Minutes Afternoon, that is, at 24 Minutes past 10 at Night.

EXAMPLE II.

What Number and Time answers to the 8th of January, 1774.

First, By the Tables of Numbers, I find the Number to be 36, and against that Number, in the Table of Times, I find 8 Hours 48 Minutes after Midnight, that is 48 Minutes past Eight in the Morning.

At Army — At Amsterdam and Armo	HM	H	N
At Army	-0103	At Cork, Calis, Cape Clear,	1
At Amsterdam and Armon	ntie 02 00	and in the Creek04	20
At Abarwark			
At Abarmorick and Antw			or
At Aldborough			
24,12,000	1313	Between the Cafkets and	
В.		Guernsey, before Cromer, at	
At Beachy, Blacktail,	and	Seven Cliffs, and at Caines - 09	~
		At the Caskets and Cham-	00
Thwart of Reachy	12/45	berness - 09	4 1
At Blackness in Bluet,	and	At Cows, in the Fols of	45
or Rell-Ille	0120	Caen, in Calice and Chamber-	100
Without Rheet and at	Rer	ness Roads ————————————————————————————————————	2
		Before the Haven of Caen,	3
Bourdeaux River, the So		in the Chamber, between	
Coast of Bretaigne, the C	Oan	Cripple Sand, and the Croyle,	
		and at Calfbot 11	13
At Brest, before the B			
and the River of Bourde	aux,	D.	
within the Haven———			
In Breefound, Bloy and		Dunkirk — 12	A 100
timore —		At Denbeigh & Downs Road 02	
Before Bremen and at Bl	the second secon	At Dort - 03	
ney, and in the Channel	be-	At Dungarven	_
fore Purdeaux-	0000	At Darimouth 36	
At Briftol Key-			
At Bridgewater			
Bullen Deep-	10 30		
		At Dover, Diepe and Deal 10	3
C.			
In Condado	12 00		1
In the Chamber of Rye	-00 45	At Emden, before the Elvi	1
Without Calis, at Co	rpus	before the Eyder, and before	-
Christi Point, and at Camf	er-01 30	1177 7 ,	0
Between Calis, and Do	March 1995 Barrier Barrier	At Edam-OI	3
before Conquet, and at		Before the Eastern & West-	20
North Caps	to the second	ern Emes, and at Engoments- 09	13

F.	HIM		H	M
On the Coast of Flanders-	1200	Under Holy Island & at Horn	01	30
At Flushing -	00 4	Before Hartlepoole -		
Before the Fen in the		At Huntcliff-Foot		
Channel —	01 30			
Without Fountny-	02 1	Before Hamborough, at Hull,		
Without the Banks of	11.	at the Holmes, and before		
등일 보고 있으면 하는 이번 경기를 하는 것이 되었다. 그 사람들은 사람들이 되었다면 하는 것이 없는 것이 없는 것이 없었다.		Humbers Mouth -		00
At Flamborough and Brid-		At Haerlem, Havre de Grace		
		and Home-bead	00	00
At the Forn, in Foy at Fal-		At St. Hellens, and Harwich		
		and without the Banks of		
Between Foy & Falmouth in		Harwich -	10	20
the Channel, and at Foulness		At Harwich within -		
Before the Coast of Friez-				
land and the Fly -	07/30	I.	- 3	
Without the Fly			12	00
At Frieze and Fair Isle -			02	00
At the Frith and South	11	In all the Havens on the	1 -5	. 33
Foreland -	1030	South Coast of Ireland	05	11
In Fair Isle Road, & at the				
North Foreland -	11 11	K.	516	
		Kentish Knock -	12	00
G .		At Kelliers -		
In Gibralter Road, Gravel-		At Kingsale —	04	A 1000
ing and before Cherburg -	12 00	At Kilduyn ———	07	1000 1116
Before Goree, at Guernsey &		At Kildive -	09	The Country of the
	01/30			
At Groine, at Gafcoign, and		L	. 80	1
the Coast of Galicia		At Leith	12	00
	094		02	15
In the Chamber, and Goree-		At London -	205	00
end —	1111	Thwart of Londey and be-		
		fore Lynn	05	25
Jan. H. d. Mail.		At Lynn half Tide, at		
Before the Hever, before		11	a6	00
Horn, and at Hampton-Key -	12 00		06	\$3.45EH
and the second and the second	1	II Zerov	其意	13

1	HI	M	O. 1	I	M
At the Lizard by the Land	07 3	30	At Orkness -	22	00
At Lambay			At Orkney	20	00
At Leystoff, and thwart off			At Orfordness -	20	15
it without the Banks	00/4	15	At Orfordness, without the	اور	+3
In Leystoff Road, and at		1	Banks, and between Orford	4	- 3
Long Sand-Head -	10	20	and Orwell Waves -		30
•		7	At Orfordness within the		30
М.			C 1	11	
Within the Maes at Mal-					15
don	00	15	p		
Before the Maes —		20	At Portsmouth Half-Tide-		
At the Maes and before		"			
St Matthew's Point	02	4 5	At the Pens, Porthus and Poistu ————————————————————————————————————	22	
In Mouse-bole, at St. Mat-	3	+3	On the Coast of Postural	03	0
thew's, & within Mount's-Bay		20	On the Coast of Portugal—	03	1+5
In Milford, at Moonless and		3			
			St. Paul's		
at St. Maloes	05	15	In the Haven at St. Paul's		
Between Mouse - Hole, and	200		Before Podessemeck —	06	45
Falmouth, & in Milford-Haven		30		97	30
In St. Magnes Sound and			At the Race of Portland —	09	00
Magnes Caftle					
At the Isle of Man					
Before Margate ———	11	15	At Quinbrough ———	12	00
N.			R.		
At Newport Half-Tide -	12	00	At Rochester —	00	45
At the West-end of the			At Ramkins —	OI	20
Nore-	00	45		1	13"
			bood's-Bay, and from the Race		
At Newcastle			to the Pole-Head -	03	0
	06			03	00
At the Needles, at the Isle		13	In Ramfey		1
	08	10		05	1 5
of Wight — All the Coast of Normandy		. 2			
	A	20	In the Sleeve, between U-		1
and Picardy		30	thant and Scilly, at the Shoe,		1
Between the Naze and			at the Spitts, at Southampton,		14
Warbead of Lower -	111	15	and along the Swin —	12	oc
				U	po

83

A TIDE-TABLE.

l H	IMI	- - - - - - -	H	MI
Upon the Coast of Spain, and in Shetland		Without Ushant	06	00
and in Shetlando	200	St. Vallery	10	20
At Scilly, in the Sound,				
Scarburgh, and at Staples o	345	w		
At Seven Isles, without the	7.7	At Winchelsey —	00	45
Haven in the Broad-Sound - o.	430	At the Weilings, and from	0.50	
At the Mouth of Severn,		the West-end of the Wight -	01	30
between Scilly and the Lizard,		Before the Weilings At Whithy	02	15
at the Spurn and Stockton	5 15	At Whithy -	03	00
Without Scilly, in the		In the Sea of Wales and	-	
Channel, and at Salcomb —— of At Sedmouth & at the Start	600	Severn —	04	30
At Sedmouth & at the Start of	6 45	In Wales —	05	15
Off the Start in the Channel				
Within the Seyn and before	1 1	at Waterford -	06	00
Shelburgh	000	at Waterford — At Weymouth Key — —	06	45
At Shorebom — o	945	At the Ness, by Wiering-		
At Seyn-Head1	030	ben, at Winterton	07	20
		Thwart of the Isle of Wight		3
T.		in the Channel, all within the		63
Within Tervere	045	Wight, between the Wight and		-
Before Tervere, before the	1,3	Beachy by the Shore	08	
Thames and at Tinmouth o	1 20	At the E.end of the Wight,		1.3
Before the Tees & Tinmouth		and on Wieringben-Flats		00
before the Bay of Tinmouth-o		and on // stringers I said	دم	2
At the Cliffs of the Texelo	4 20	Y.	-	
In Torhay and before the	73	Before Yarmouth -	0	0
Texelo	600			30
In the Road of the Texel o		At Yarmouth —	1000	15
	945			*5
111 1018111	45	Yarmouth Haven	4	
U.		I wimouso Haven	- 10	30
	200	Z .	1	
	300			
Between Ushant & the Main		In the Zerick-Sea	200	30
In the Vourd, at the Bay,	3 45	III the Letter-Sea	-03	00
within Ushant ————————————————————————————————————	430	1.00		
	10	•	1	
1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	M	2		The

The Use of the TIDE-TABLE, in finding the Time of High-Water.

I N this Table the Names of the Places being set in Alphabetical Order, they will always be found under the Letter they begin with, as for Example, London, will be found under the Letter L, Torbay under T. Scilly under S, &c. and the Figures right against any Place shews the Time of High-Water at that Place, on the Full and

Change of the Moon.

Then if it be required to find the Time of High-Water at any Place upon any given Day, First, (by the Tables of Numbers and Times answering) find the Number and Time answering for that Day, (as before taught) and to that Time, add the Hours and Minutes that stand in the Tide-Table against the Place you would know the Time of High-Water at, the Sum, if it does not exceed 12 Hours, will be the Time of High-Water required; but if it should be more than 12 Hours, then subtract 12 from it, and the Remainder will be the Time of High-Water.

EXAMPLE I.

Suppose it was required to find the Time of High - Water at London, on 30th of January, 1773

By the Table of Numbers, I find the Number for the 30th of January, to be 17, with which Number entring the Table of Times, I find the Time answering to be 5 H. 36 M. then looking for London in the Tide-Table, I find against it 3 Hours, which added to the Time before found, gives 8 H. 36 M. for the Time of High-Water at London, on the 30th of January, 1773.

EXAMPLE II.

Suppose it was required to find the Time of High-Water at St. Hellens, on the 19th of August, 1774.

Having found the Number (as before) to be 22, and the Time answering to be 9 H. 36 M. I look in the Tide-Table under the Letter H, for St. Hellens, against which I find 10 H. 30 M. which added to the Time (as before) 9.36 gives 20,06, from which subtract 12,00 and the Remainder 8 H. 06 M. is the Time of High-Water required.

A TABLE of the Sun's Declination for the Years 1765, 1769, 1773, and 1777.

M. Day.	•	Jan.	-	rep.	Marris	March	IV	udw		May		June		July		August	,	Septem.		October	:	Novem.	6	Decem.
	Sou	ath	Sou	ith	Sou	th	No	rth	No	rth	No	rth	No	rth	No	orth	No	rth	Soi	ath	Sou	ith	Sou	eth
1	22	58	16	56	07	22	04	45	15	14	22	08	23	07	17	56	08	08	03	23	14	37	21	55
												16												
												23												
												30												
5	22	34	15	45	05	50	00	10	10	24		37		47	10	53	00	39	04	50	15	52	22	2
6	22	26	15	26	05	27	06	39	16	41	22	43	22	41	16	37	06	17	05	19	16	10	22	3
7	22	19	15	07	05	03	07	02	10	57	22	49	22	34	16	20	05	55	05	42	10	28	22	4
												54												
												59												
-	-	53	14	_	03	53	-	_	-	45	-3	04	_	• 3	.>	_		40	-	2,	-	- 9	23	9
												08												
												12												
13	21	23	13	10	02	42	09	14	18	31	23	15	21	48	14	34	03	38	07	58	81	08	23	1
												18												
-	-		-		-	_	-		-		-	-	-	-	-	-	-	-	1-	-	-		_	
												23												
17	20	38	11	47	01	08	10	39	19	27	23	25	21	09	13	10	OZ	05	109	27	19	09	23	2
												26												
												27												
_	-		-	+3	-	_	-		_		-	_	_	-	_		_		_	-	-	<u>.</u>	-	_
21	119	47	10	21	00	27	12	02	20	17	23	28	20	25	11	59	00	31	10	54	20	04	23	2
22	119	33	09	59	00	51	12	22	20	29	23	28	20	13	11	39	00	08	11	45	120	17	23	2
23	19	19	29	37	10	14	12	42	20	41	23	27	20	01	11	19	50	115	111	36	20	29	23	2
34	119	04	109	15	01	38	13	02	20	52	23	26	119	48	10	58	00	39	11	57	20	41	23	2
25	18	49	08	53	02	02	13	21	21	03	23	24	19	30	10	38	21	02	12	18	20	53	23	2
26	18	34	08	30	02	25	13	41	21	13	23	22	19	22	10	17	01	26	12	30	21	05	23	2
27	18	19	08	08	OZ	49	14	00	21	23	23	20	19	09	09	56	10	49	12	59	21	16	23	2
		03		45	03	12	14	19	21	33	23	17	18	5.5	109	34	OZ	13	13	19	21			
		47			03	35	14	37	21	42	23	14	18	41	09	13	oz	36	13	39	21	36	23	
35	17							. 50	21	51	123	10	18	20	80	51	02							
3	1.7	13	1		104	22	1.		122	00			110	11	.00	30	1 .	1	14	18	1		123	-

A TABLE of the Sun's Declination for the Years 1766, 1770, 1774, and 1778.

M. Day.	•	Jan.		reb.	1	March		April		May	•	June	:	July		Augult		oeptem.		October		Novem.	•	Decem.
	Son	ıth	Sou	ıth	Sou	ıth	No	rth	No	rth	No	rth	No	rth	No	rth	No	rth	Soi	ath	Sou	ıth	Sou	ith
								39																
2	22	54	16	43	07	05	05	02	15	27	22	14	23	03	17	45	97	51	03	41	14	52	22	0
3	22	48	16	25	06	42	05	25	15	45	22	21	22	59	17	29	07	25	34	04	15	11	22	11
4	22	42	10	07	00	19	05	48	10	03	22	29	22	54	17	13	07	07	04	2;	15	29	22	19
5	22	35	15	49	05	50	00	11	10	20	ZZ	35	22	48	10	57	30	45	04	5°	15	48	22	20
-	-	- 8			~		6	34	46			_,		4.	16	45	26		~		.6	-6		
								56																
8	22	13	14	53	04	46	07	19	17	10	22	53	22	20	16	07	20	37	05	50	16	41	22	4
0	22	04	14	34	04	25	07	41	17	26	22	58	22	22	15	SC	25	15	06	22	16	58	22	5
10	21	55	14	14	03	59	08	03	17	41	23	03	22	15	15	32	24	52	06	45	17	15	22	5
-	-		1-	-	-		-	—	-	-	-	7	-	_	-	-	-	-		-	-	-	_	-
								25																
12	21	36	13	35	03	12	08	47	18	1.2	23	11	21	59	14	56	04	06	07	30	17	48	23	0
								09																
								30																
15	21	04	12	34	02	01	09	52	10	30	23	-	-	32	14	_	02	57	-	30	10	30	23	
16	20	51	12	1:	101	37	10	13	10	10	23	23	21	22	13	42	02	34	00	00	18	51	23	2
								34																
								55																
14	20	16	11	00	00	.20	11	16	19	50	23	27	20	51	12	44	01	24	10	06	19	34	23	2
20	20	0	10	4	800	02	11	37	20	02	23	28	20	40	12	24	01	00	10	27	19	47	23	2
-	10		1	20	SN	0.2	1	57	20	15	22	28	20	28	12	04	00	17	10	40	20	01	22	2
2	2 10	3	5 10	0	100	4	112	17	20	26	23	28	20	16	11	44	00	14	11	10	20	14	23	2
2	3 19	2	2 00	4	2 01	00	9 12	37	7 20	38	23	27	20	04	11	24	So	110	11	31	20	26	23	2
2	4 10	0	9 00	2:20	001	3	2 1:	2 27	20	49	23	20	919	52	11	03	00	33	11	52	20	39	23	2
2	5 18	5	3 08	3 5	801	5	5 1:	3 17	21	00	23	25	19	39	10	43	00	57	12	13	20	50	23	2
-	6 . 5		801	3 2	602	1		3 30	5 21	11	22	2:	10	26	10	22	01	20	12	24	21	02	22	,
2	7 15	3 2	2 0	3 1	3 02	4	3 1	3 5	21	21	23	2	10	12	10	01	01	44	12	54	21	13	22	2
2	8 1	3 0	70	7 5	001	0	61	4 1	1 21	31	23	18	18	58	09	40	OZ	07	13	14	21	24	23	
1 1 1	911				0	3	014	4 3:	3 21	40	123	15	18	44	109	18	02	30	13	34	21		23	
2.3	0 1	Seed of the			0	5	3 14	4 5	1 21	49	23	11	18	30	08	57	02	54	13		21	44	23	1
-3		7 0				1		1		58		+ 1	18	15	108	35	1	1	114	14		-	23	C

A TABLE of the Sun's Declination for the Years 1767, 1771, 1775, and 1779.

M. Day	1	Jan.	7-2	ren.		March	17.7	Aprıı	Men	May	•	June	1.1	Juny	4	August		Septem.		October		Nøvem.	-	Lec.
	Sou	th	Sou	ıth	Sou	th	No	rth	No	rth	No	rth	No	rth	No	rth	No	rth	Soi	ath	Sou	ith	Sou	ith
																				12				
2	22	56	16	47	07	10	04	57	15	23	22	12	23	04	17	48	07	57	03	35	14	47	22	cc
.3	22	5c	16	30	06	47	25	20	15	41	22	20	23	00	17	33	27	35	03	58	15	ot	22	09
4	22	44	16	12	06	24	05	43	15	58	22	27	22	55	17	17	07	13	04	21	15	25	22	17
5	22	37	15	54	06	01	06	05	16	16	22	34	22	49	17	01	06	50	24	45	15	43	22	25
6	22	30	15	35	05	38	56	28	16	33	22	40	22	44	16	45	06	28	05	08	16	01	22	32
7	22	23	15	17	05	15	o 6	51	16	49	22	46	22	37	16	28	06	05	05	31	16	15	22	39
6	22	15	14	58	04	51	27	13	17	06	22	52	22	31	16	11	05	43	05	54	16	37	22	49
9	22	06	14	39	04	28	07	36	17	22	22	57	22	24	15	54	05	20	06	17	16	54	22	5
10	21	57	14	19	04	04	97	58	17	38	23	02	22	16	15	36	04	58	06	40	17	11	22	5
.,	21	48	13	59	03	41	08	20	17	53	23	06	22	09	15	19	04	35	07	02	17	28	23	0
12	21	38	13	40	03	17	08	42	18	09	23	10	22	01	15	01	04	12	07	25	17	44	23	0
13	21	28	13	20	02	54	09	04	18	23	23	14	21	52	14	43	03	49	07	48	18	oc	23	1
14	21	18	12	59	02	30	09	25	18	38	23	17	21	43	14	24	03	26	08	10	18	11	23	1
15	21	07	12	39	02	06	99	47	18	52	23	20	21	34	14	06	03	02	08	32	18	32	23	1
16	20	56	12	18	10	43	10	08	19	06	23	22	21	24	13	47	02	39	08	55	18	47	23	2
17	20	44	11	57	01	19	10	29	19	20	23	24	21	14	13	28	02	16	09	17	19	02	23	2
18	20	22	11	36	00	45	10	50	19	33	23	26	21	04	13	08	01	53	09	38	19	16	23	2
																				OC				
20	20	00	10	53	00	08	11	32	19	59	23	28	20	42	12	29	10	ot	10	22	19	44	23	2
21	19	53	10	32	No	.16	11	52	20	12	23	28	20	31	12	09	00	43	10	44	19	58	23	2
22	19	40	10	10	00	39	12	12	20	24	23	28	20	19	11	49	00	19	11	05	20	11	23	2
23	19	26	09	48	bi	03	12	32	20	35	23	27	20	07	11	39	So	u04	11	26	20	23	23	2
24	119	11	109	26	10	27	13	52	20	47	23	20	119	55	11	0	00	28	11	47	20	36	23	2
25	18	57	09	0	101	50	13	12	20	58	23	25	19	42	10	48	00	51	12	08	20	48	23	2
26	18	42	08	4	02	14	13	31	21	08	23	23	19	29	10	27	01	14	12	29	20	59	23	2
27	18	26	08	19	02	37	13	51	21	18	23	21	19	15	10	of	CI	38	12	49	21	10	23	2
				50	13	0	14	10	21	. 28	23	19	19	02	09	45	02	01	13	00	21	21	23	
	17																			29			23	5-06-100
	17							47				12						4		49		41	23	
3	117	21	1	10.1	104	. 10	7		121	50	ગ		119) os	4	OI .		114	1 00		1	123	1

A TABLE of the Sun's Declination for the Years 1768, 1772, 1776, and 1780.

M. Day		Jan.		rep.		March	•	April		May	•	June	:	July		August		Septem.		October		Novem.		Dec.
	Soi	ıth	Sou	ith	Sou	th	No	orth	No	rth	No	rth	No	rth	No	rth	No	rth	Soi	ith	Sou	ıth	Sou	ith
					07																			
2	22	57	16	54	06	54	05	13	15	36	22	18	23	01	17	37	07	41	03	52	15	01	22	06
3	22	51	10	35	06	31	05	36	15	54	22	25	22	56	17	21	97	19	04	15	15	20	22	15
4	22	40	15	17	06	08	06	22	16	11	22	32	22	51	17	05	06	50	05	30	15	3:	22	23
_	_	37	-	"	3		_	_	_	_	_		_	4)		77	_	21	-,	_		_		3-
6	22	32	15	40	05	21	06	45	16	46	22	44	22	39	16	32	06	12	05	2:	16	14	22	37
7	22	25	15	22	04	58	07	07	17	01	22	50	22	33	10	10	05	49	25	48	10	32	22	44
6	22	08	15	03	04	34	07	30	17	17	22	50	22	20	15	59	05	20	06	22	17	49	22	50
10	22	00	14	24	04	47	c8	14	17	33 49	23	05	22	11	15	24	04	41	06	56	17	23	23	01
-	-		-		-	200	-		_	1	-	-	-		-	_	-	_	-	-	-			
11	21	51	14	05	03	24	08	58	18	04	23	09	22	03	15	00	04	10	07	41	17	40	23	10
12	21	71	13	45	03	27	00	10	18	19	23	16	21	16	14	10	03	22	08	04	18	12	2 2	14
14	21	21	13	05	02	12	00	41	18	50	22	10	21	37	14	11	03	10	08	26	18	28	23	17
15	21	10	12	44	01	49	10	02	19	03	23	22	21	27	13	52	02	46	08	48	18	43	23	20
16	20	50	12	24	01	26	10	24	10	16	22	24	21	17	12	22	02	22	00	11	18	58	23	2:
17	20	47	12	03	01	02	10	46	10	30	23	25	21	07	13	14	01	59	09	33	19	12	23	25
18	20	35	11	42	00	38	11	05	10	43	23	26	20	57	12	54	01	36	09	54	19	27	23	21
19	20	22	11	20	00	14	11	26	19	56	23	27	20	45	12	34	20	13	10	16	10	40	23	27
20	20	10	10	59	No	.09	11	47	20	08	23	28	20	34	12	15	00	49	10	38	rğ	54	23	28
21	19	57	10	37	00	33	12	07	20	20	23	28	20	22	11	54	00	26	10	59	20	07	23	28
22	119	43	10	16	00	56	12	27	20	32	23	27	20	10	11	34	00	02	11	20	20	20	23	28
					101																			
24	19	15	109	31	01	45	13	07	20	55	23	25	19	45	19	53	00	45	12	02	20	44	23	26
25	19	01	29	09	02	07	13	26	21	05	23	24	19	32	10	32	01	08	12	23	20	56	23	24
26	18	46	08	47	02	31	13	45	21	16	23	22	19	19	10	12	01	31	12	43	21	07	23	2:
				25	22	54	14	04	21	26	23	19	19	26	09	50	CI	55	13	04	2 1	18	23	15
			08		23						23	17	18	70 TO	09	29	02	18	13	24		11/	23	16
			77	39	23	41	14	42	21	44	23	13	18	33	99	08	02	42	13	41			23	12
	17		1-				1 6.					10	18	23	28	40	03			03			2,3	CS
31	17	26			104	27		18	22	OZ		-	1.0	08	00	24	-		114	23		-	123	00

A TABLE of the Variation of the Sun's Declination to every 10 Degrees of Longitude.

Degrees of Longitude from the Meridian of LO	N	D	01	V.
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Daily Vari.	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180
Mın.	min	min	min	min	min	min	min	min	min	min	min	min	min	min	min,	min	min	mn
2	0	0	. 0	0	0	0	0	0	0	I	I	I	I	I	I	1	I	1
3	0	0	0	0	0		I	I	I	1	I	I	I	I	I	I	I	I
4	0	0	0		I	I	I	I	I	I	I	I	I	2	2	2	2	2
4 5	0	0	0	0	I	1	1	I	1	1	I	2	2	2	2	2	2	2
6	0	0	0	I	1	1	I	I	1	2	2	2	2	2	2	2	3	3
7 8	0	0	I	I	I	I	I	2	2	2	2	2	3	3	3	3	3	3
8	0	0	I	I	I	Í	I	2	2	2	2	3	3	3	3	3	4	4
9	0	0	I	1	1	1	2	2	2	2	3	3	3	3	4	4	4	4
10	0	1	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5
II	0	1	1	I	2	2		3	- 3	3	3	4	4	4		5	5	5
12	0	1	I	I	2	2	2	3	3	3 3 4	4	4	4	5	5 5	5 5 6	5	5 6
13	0	1	1	I	2	2	2	3	3 3 3	4	4	4	5	5	5	6	6	6
14	0	1	1	2	2		3	3	3	4	1 4	5	5	5	6	6	7	7
16	0	1	I	2			3 3 3	3	3 4	4	5	5	5 6	6	6	7	7 7 8 8	7 7 8
	0	1	I	2	2	3	3	4	4	4 5	5	5 6			7	7	8	8
17	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	6 7 7 7	8	8
18	ı	1	2	2	3	3	4	4	5	5	6	6	7	7	7	8	9	9
19	I	I	2	2	3	3 3	4	4	5	5	6	6	7			8	9	9
20	I		2		3	3	4	1	5	5 6 6	6	17	7	7 8 8	7 8	9	9	10
21	1	1	2	2	3 3 3	4	4	5	5	6	6	7	8	8	9	9	10	10
22	I	1	2	2	3	4	4	5	6	6	7	788	8	9	9	1.0		II
23.	I	I	2 2 2	3 3	3 3 3	4 4	4	5 5	6	1 6	7 7 7	8	8	9	9	IC	11	11
24	I	I	2	3	3	1 4	. 5	1 5	6	7	17	18	9	19	10	III	11	12

To find the Sun's Declination, by the foregoing TABLES:

ACH Page of the foregoing Tables contains the Sun's Declination for the four Years that it is mark'd with at the Top, and is divided into thirteen Columns; the first of which to the Left-Hand, shews the Day of the Month, and the other Twelve the Months of the Year, so that if it be required to find the Sun's Declination for any Day, at suppose for Example, on the 21st of August, 1767: First I look for that Table that has 1767. at the Top of it, and then right against the 21st Day of the Month, and under August, I find 12, 10. which shews the Sun's Declination to be 12 Degrees 10 Minutes North; according to the Title at the Top of the Column.

The Sun's Declination in these Tables being calculated for the Meridian of London, if you should be considerable to the Eastward, or to the Westward of London, it will cause some Alteration in it; to correct.

which, the

Table of Variation of the Sun's Declination is to be used as follows.

First, Look out the Declination for the given Day of the Month, and for the Day following it, and subtract the lesser from the greater, the Remainder is the daily Variation.

Second, Observe whether the Declination be increasing or decreasing, which you may know thus; if the Declination for the Day following the given Day be biggest, than it is increasing; but if it be least, it is decreasing.

Third, Look for the Daily Variation in the first Column of the Table, and see what Number stands right against it, and under the given De-

grees of Longitude; which Number is to be used as follows.

If the Difference of Longitude be Easterly, and the Declination increasing, it must be substracted from the Declination found in the Tables for the given Day; but if the Declination be decreasing, it must be added.

If the Difference of Longitude be Westerly, and the Declination increasing, it must be added; but if the Declination be decreasing, it must be substracted; the Sum in one Case, and the Remainder in the other will be the Sun's Declination at Noon in the Longitude required.

A TABLE of the Sun's Right Ascension.

M Day	-	Jan.		reb.	1	March	1	April		May		June	I.d.	Juny	A A	ımgnı		oeptem.	- 00	October	None	MOVEIII.	Dec	
																				M				M
1	18	50	21	02	22	51	00	44	22	35	04	38	06	42	80	47	10	43	12	31	14	28	16	32
2	18	54	21	c6	22	54	00	48	02	39	04	42	06	46	08	51	10	47	12	35	14	31	16	36
3	18	58	21	10	22	58	00	51	02	43	04	46	06	50	08	55	10	50	12	38	14	35	16	40
4	19	03	21	14	23	02	00	55	02	47	04	50	06	55	08	5.5	10	54	12	42	14	39	16	45
5	19	07	21	18	23	05	00	59	32	51	04	54	06	5.9	09	02	10	57	12	46	14	43	16	49
6	19	12	21	22	23	06	01	02	02	54	04	59	07	03	09	c6	11	01	12	45	14	47	16	53
7	19	16	21	26	23	13	01	06.	02	58	05	03	07	07	09	10	11	05	12	53	14	51	16	58
8	19	20	21	30	23	17	01	10	03	02	05	07	07	11	وي	14	11	08	12	57	14	55	17	02
9	19	25	21	34	23	20	01	13	03	06	05	11	07	15	09	15	11	12	13	oc	14	59	17	07
10	19	29	21	38	23	24	01	17	03	10	05	15	07	19	59	2.	11	16	13	04	15	03	17	11
11	19	33	21	42	23	28	01	21	03	14	05	19	07	23	09	25	11	19	13	08	15	07	17	1
																				11				
																				15				
14	19	40	21	53	23	39	01	32	03	26	05	32	97	36	09	37	11	30	13	19	15	20	17	20
15	19	51	21	57	23	42	01	35	03	30	05	30	97	40	<u>-9</u>	40	11	33	13	23	15	24	17	3.
																				26				
																				30				
18	20	04	22	09	23	53	01	40	03	41	05	48	07	52	09	52	111	44	13	34	15	30	17	4
10	20	08	22	13	23	57	01	50	23	45	05	52	07	50	109	55	111	40	13	38	15	40	17	5
20	20	12		17	00	00	01	54	-3	49	05	57	08	00	-	59	-	51	1 3	41	15	45	17	5
																				45				
22	20	20	22	24	100	07	02	01	03	57	00	05	08	00	110	Or.	111	59	13	49	15	53	18	0
23	120	25	22	20	00	11	02	05	104	01	00	09	00	12	10	10	12	02	13	53	15	57	10	0
24	120	29	22	32	100	15	02	cg	104	00	05	13	00	10	10	14	12	00	13	57	16	02	10	1
25	20	33		30		19	02	13	-	10	00	17	-0	20	-	1,	-	05	14	00	-		10	
26	20	37	22	39	00	22	02	16	04	14	06	22	08	23	10	21	12	13	14	04	16	10	18	2
27	20	41	22	43	20	26	02	20	104	18	00	26	08	27	10	25	12	17	14	. 08	10	14	18	2
				47	100	30	02	24	104	22	100	30	28	31	10	28	12	20	14	12	10	19	18	3
	1	49			100	33	02	28	lot	20	100	34	28	35	110	. 32	12	24	114	16	10	23	10	3
	1	54					1	31				35	0	. 55	110	30	1 2	2		20		27		
31	20	58	1		130	40	1		104	34	1		100	4:	10	35	1	2	1.4	24	1.6	1	18	4

A TABLE of the Right Ascension and Declination of some of the most noted Fixed Stars.

		ght	Declina-		
The Names of the Stars.	1	en.	ti	on	
	H.	M.	D.	M.	
The Bright Star of Aries	10	53	22	17 N	
Medusa's Head, Algol	02	52	39	59 N	
The Bright-side of Perseus	03	07	48	58 N	
The Bull's Eye, Aldebaran	04	22	15	59 N	
The Goat Star, Capella	04	59	45	43 N	
The Bright-foot of Orion, Regal	05	01	08	285	
The Northern Horn of the Bull -	05	09	28	21 N	
Orion's Left Shoulder —	05	10	06	04 N	
The Southern Horn of the Bull -	05	21	20	56 N	
Middle Star in Orion's Belt -	05	22	101	25 S	
Orion's Right Shoulder——————	05	52	07	20 N	
Auriga's Right Shoulder —————	05	44	44	54 N	
Bright Foot of Gemini—————	06	20	16	38 N	
The Dog Star, Syrius -	06	34	16	23 S	
Castor, or the Head of the Northermost Twin -	07	17	32	24 N	
The little Dog Star, Procyon-	07	24	05	49 N	
Pollux, or the Head of the Southermost Twin	07	28	28	36 N	
Hydra's Heart —	09		07	37 S	
The Lyon's Heart, Regulus-	09		13	09 N	
The Lower of the Pointers -	10	45	57	41 N	
The Upper of the Pointers -	10	46	63		
The Lyon's Tail, Deneb	11	35	15	55 N	
Upper of the two last in the square of Great Bear	12	02	58		
The first in the Great Bear's Tail-	12	41	57	181	
The Virgin's Spike —	13		09	52 S	
The middle of the three in the Great Bear's Tail-	13		56	221	
Last but one in the Tail of Hydra -	13		21	43 5	
Last in the Great Bear's Tail -	13	36	50	311	
Arturus —	14		20	301	
Bright Star in the Southern Ballance-	14		14	538	
Foremost Guard —	15		75	151	
				Brig	

A TABLE of the Fixed Stars.

	ght		lina-
	The state of the s	D.	
15	22	27	33 N
15	31		18 N
16	14		5 · S
17	03	14	40 N
17.	22	12	47 N
17	50	51	32 N
18	27		33 N
19		1	29 N
19		08	14 N
20		44	19 N
21	27		39 N
22	42	30	55 S
22	53		53 N
22	52	26	43 N
23	20	76	07 N
23	54		34 N
23	.58	13	39 N
00	42	88	oo N
00	53	34	05 N
R		Dec	clina-
A			ion
H.	M.	D.	М.
12	03	57	11 8
12		58	
12	16		
12	12	161	31 S
	Afc H. 15 16 17 17 18 19 19 20 21 22 22 23 23 23 23 00 00 RAH.	Afcen. H. M. 15 22 15 31 16 14 17 03 17 22 17 50 18 27 19 17 19 39 20 33 21 27 22 42 22 53 22 52 23 20 23 54 23 58 00 42 00 53 Right Afcen. H. M.	Afcen. H. M. D. 15 22 27 15 31 07 16 14 25 17 03 14 17 22 12 17 50 51 18 27 38 19 17 27 19 39 08 20 33 44 21 27 08 22 42 30 22 53 13 22 52 26 23 20 76 23 54 27 23 58 13 00 42 88 00 53 34 Right Afcen. H. M. D. 12 03 57 12 33 58 12 16 55

To work an Observation, or to find the Latitude of the Place by the Tables of the Sun or Stars Declination, and their Zenith Distance, &c.

Note, WHEN you take an Observation of the Sun, by the common Sea Quadrant, the Degrees and Minutes that your sight Vane stands at, being added to the Degrees that your Shade or Glass Vane stands at, will give the Zenith Distance (or Complement of the Meridian Altitude) with which and the Declination found in the Tables, you may find the Latitude as follows.

First, Take Notice whether the Sun or Star be to the Northward or to the Southward of you at the Time of Observation; if they are to are to the Northward, call your Zenith Distance North; or if they

the Southward, call it South. Then,

Second, If the Zenith Distance and Declination are both North, or both South, substract the lesser from the greater, the Remainder will be the Latitude you are in, of the same Name with the Declination, if that be greater than the Zenith Distance, otherwise of a contrary Name.

Example ist, Being at Sea on the 23d of August, 1767, I observed at Noon, and had on my Quadrant 8.34, (and the Sun to the Northward of me) what Latitude am I in?

Zenith Distance — 8. 34 North
Declination — 11. 30 North
Latitude by Observation — 2. 56 North

Example 2d, Being at Sea on the 23d of December, I took the Altitude of the Dog Star Syrius, (on the Meridian to the Southward of

me) 60 00, I would know the Latitude?

Note, In all Cases (except where the Object is observed on the Meridian below the Pole) if the Meridian Altitude be given instead of the Zenith Distance, (as it is in this Example) then subtract it from 90, 00, and the Remainder will be the Zenith Distance.

Latitude by Observation - 13. 37 North

To work an Observation.

Case the 2d, If the Zenith Distance and Declination be one North, and the other South, add them together, and their Sum will be the Latitude in, of the same Name with the Declination.

Example 1st, Being at Sea, on the third of November, 1767, I observed at Noon, and had on my Quadrant 8.17, (and the Sun to the Northward

of me) I demand the Latitude?

Example 2d, Being at Sea on the 21st of June, 1769, I took the Altitude of the Bright Star in the Harp, Lyræ, (on the Meridian to the Southward of me) 51.00. I demand the Latitude.

Complement Altitude, or Zenith Distance — 39. 00 South Star's Declination — 38. 33 North Latitude by Observation — 77. 33 North

The foregoing Rules are for observing by the Sun or Stars, when they are at their greatest Altitude, or upon the Meridian above the Pole; but as in some Parts of the Earth the Sun does not set for several Days, but some Stars never set; in that Case they may be observed upon the Meridian, twice in the 24 Hours, that is, once at their greatest Height (as before) and again, when they are at the lowest, or upon the Meridian below the Pole; to work which Observation take the following Rule.

Add the Complement of the Declination to the Meridian Altitude, the Sum is the Latitude of the same Name with the Declination.

Example, Being at Sea, I took the Altitude of the Pole Star on the Meridian below the Pole, 46. 21, I demand the Latitude?

Meridian Altitude — 46. 21

Complement Declination — 01. 56 North

Latitude by Observation — 48. 17 North

The

Remarks by the Reviser. The Author in the above Rules and Examples, takes the Sum of the Numbers found on his Quadrant, and works with it, as if true, to find the Latitude: But the Latitude so obtained will be several Minutes from the true Latitude. For obtaining which, the Zenith Distance as found by the Quadrant, must be first corrected, as shewn in the Mariner's Compass rectified.

The Use of the TABLES of the Sun's and Stars Right Ascension, in finding what Time any known Star will be upon the Meridian, on any given Day.

Rule, Look for the Right Ascension of the Sun and Star in the foregoing Tables, and subtract the Sun's Right Ascension from the Star's; but if the Sun's Right Ascension be biggest, add 24 Hours to the Star's Right Ascension, and then subtract the Sun's from it. the Remainder will be the Time of the Star's coming to the Meridian after Noon.

Example 1st, What Time will the Lion's Tail be upon the Meridian, on the 14th of April?

Stars Right Ascension — — — 11. 35
Sun's Right Ascension — — — 01. 32

Time the Star will be on the Meridian - 10. 03 at Night. Example 2d, What Time will the Bull's Eye be on the Meridian, on the 26th of October?

Star's Right Ascension 4h. 22m. add 24h. makes - 28. 22 Sun's Right Ascension — 14.04

Time the Star will be on the Meridian — 14. 18 Afternoon that is, at 18 m. past 2 in the Morning.

To find what Star will come upon the Meridian, at any given Time. Rule, Add the Time from Noon, to the Right Ascension of the Sun. the Sum will be the Right Ascension of the Star required to be known, with which enter the Table of the Star's Right Ascension, and find what Star's Right Ascension agree with, or comes the nearest to it, and that is the Star required.

Example ift, I would know what Star would be on the Meridian,

about Eight at Night, on the 7th of April.

Sun's Right Ascension — — or. 06

Time from Noon — — 08. 00

Right Asc. of the req. Star, the nearest to which og. o6 is Hydra's Heart Example 2d, I would know what Star would be on the Meridian, at past 2 in the Morning, on the 26th of June. h. m.

Sun's Right Afcension - -Time from Noon

Rt. Asc. of req. Star, nearest to which in the Tables 20. 37 is Swan's Tail.

A TABLE of the Latitudes and Longitudes of Places accounting the Longitudes from the Meridian of LONDON.

Places Names	La	titude	Lon	gitude	Places Names.	La	titude	Lon	gitude
The Coast of England.	D.	М.	D.	М.		D.	М.	D.	м.
DErwick —	55	48	01	45W	Aberdeen -	-17	24 N	10	40W
15 Newcastle —	55	12	10	30W	Dundee		28 N		40W
Stockton	54	33	10	25 W	Edinburgh -	-155	58 N		59W
Spurn ———		45	00	13 E					
Yarmouth -		40	01	40 E	The Coal	t of .	Ireland	1.	
London-	51	32	00	00					
North Foreland-	51	25	10	24 E	Dublin	-153	12	106	56
	0	46	00	25 E	Wexford -	- 52	13	07	27
Dunnose -	50	38 0	ioi	23	Waterford-	- 52			40 €
Portland -	50		OZ	44	Cork-	- 51	493	09	303
Start ———			103	47	Cape Clear	- 51	. 17	II	10
Lizard		57 8	1	14	Limeric ————————————————————————————————————	- 52	23 2	09	35 3
Land's End —		06 2	06	00 €	Galway ———	- 53	07 =	29	4009
St. Mary Scilly-			06	10 0	Slime Head -	- 53	200	11	155
Hartland Point-	151	06	04		Londonderry -	- 55	00	07	500
Lundy Isle		20	04	35 1	Bellfast	- 54	39	06	30
Briftol -	l; i	33	04	3 509.	Th- 0-0 -C1	7 11	, ,	r/	,
St. David's Head -		50	05	35 gitud	The Coast of H	ioilan	a and I	clan	aers.
Barfey Ifle -			05	00 0	Scaw	1		110	20
Holy-head -			04	50	Helighland —		30	10	20
Liverpool -	53	20	03	00	Hambrouch	- 54	24	08	35
Whitehaven —	- 54		03	30	Hambrough ————————————————————————————————————	- 53			35 E
Carlifle -	154		103	05	The Fly	- 53	05 0		35 ₽
	7.7		3		The Texel	123		1 0	300
The Coast	of	Scotlar	.1		Amfterdam —				
1 ne coan	01	Otorren			Rotterdam				04 2
-3:-3	1	1	1-		The Brill	-151	55 5		
Glafgow -	5.5	52	04		Shrice	1			000
N. Part of Sky Isle -		45 %	2 05	45 8	Sluice ————————————————————————————————————	- 51	14	103	43
N. Part of Lewis Ifl			07			-150	. 58	101	54
St. Kildry	157		- 09		The Coaft of F	rance	and I	ortz	gal.
Farra Head —	- 58			105	Dien	-,	56 N	1	
Ifles of Orkney			. 03	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	Diep————————————————————————————————————	- 49	47 N		00 W
Shetland S. Point-	Sec. 19.	-04	OZ	00 5		149	50 N		20 W
Buchaness -	-57	45	101	180	Gaskets — Guernsey	- 49	33 N		20 11
	1 -		1		Guernicy	-49	13	IOS	20 11

(98) A TABLE of Latitudes and Longitudes.

						•	,		
Places Names.	La	titude	Lon	gitude	Places Names.	La	titude	Lon	gitude
The Coast of France and Portugal.	D.	м.	D.	м.		D.	М.	D.	М.
Morliax ———	48	33	03	49	Ancona ——	43	40	14	26
Ushant ———	48	30	05	02	Venice —	45	25	12	10
Breast	48	23	04	25	Lepanto -	38	10	22	52
Penmark	47	48	04	24	Cape Matapan	36	33	22	41
Bell-Ife ——	47	20	03	16	Cape St. Angelo -		32	23	56
Nantz	47	14	01	39	Athens	37	58	24	05
Island Dieu -	46	34 Z	02	13 €	Cape Martelo S.]	1		1	118
Ifle of Ree -	46	105	01	300	part of Negropont	38	07	25	03
Rochel -	46	10	10	111	Cape Monte Sancto	40	26	25	02
Bourdeaux -	44	50 8	00	388	Gallipoly —	40	33 Vorth	27	20
Bilboa —	43	29 =	02	5800	Constantinople -	40	59 3	28	56
Cape Ortegal -		29 ude	07	58gitud	Smyrna		285	127	25
Cape Finister -	43	12	09	40 0		38	015	27	530
	41	10	09	25	Antiocheta -		30 =	32	530
Burlings	39	35	09	24	Scanderoon -		34 0		30
Rock of Lifbon -		54	09	50	Tripoli -	134	38	36	15
Cape St. Vincent -			09	06	Alexandria -	31	10	30	19
Cadiz —	36	33	06	01	Cape Rufato-		48	21	25
Cape Trefalgar —	36	10	06	01	Cape Miserato	32	21	16	17
Cape Treamgan	13-				Tripoly-		54	13	10
					Cape Bona	137	03	11	04
On the Main Contin	nent	within	the	Straits	Bona —	37	O2	108	19
					Algier —	37	05	03	16
								02	04 V
Gibralter -		12	04	53W	Tetuan —		30		06 V
Cape de Gat-	- 36	40	10	40W	Ceuta	100	27	05	4-1
Cape Paul	-38	15	00	05		35	54	04	45 V
Cape Martin -	- 38	46	00	40	Tangier -	135	42	105	221
Barcelona -	-41	26 2	02	18	10-1-1-11		- 0		
Marseilles ———————————————————————————————————	-43	18 9	05	27 A	Islands within	in tr	ie Stra	its.	
Toulon -	-43	07 5	06	02 7					
Genoa —	-44	25 5	108	43 5	Alboran —	35		02	29 V
	-43	28 =	10	3500	Formentaria —	-38		101	55
Rome —	-41	25 28 THE S4 CE	12	45 2	Yvica	-38		01	40
	- 40	3.	1.1	40	Majorca City —	-39	30=	03	03
Cape Spartuventure	37	55	16	55	Port Manon —		42	04	12
Cape Collone -	- 38	56	18	05	Gallita —	-37	41 =	.08	44.5
Gallipoli -	- 39	56	18	43	S. end of Sardinia-	-38	46 5	-09	12
Cape St. Mary -	- 39	45	19		N. end of Corfica-	42	56"	09	50 8
1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1		1			+		1.	

A TABLE of Latitudes and Longitudes.

Places Names.	La	titude	Lon	gitude	Places Names.	La	titude	Lon	gitude
Islands within the Straits.	D.	M.	D.	м.		D.	м.	D.	М.
Gorgona ——		34	09	38		04		02	17W
	43	03	14	54	Cape three Points -	-04	287	10	50W
Lilboa ———	42	45	11	00	River Volta -		55 9	03	25.
Messina ———	38	07	16	20	River Formosa -	- 07	00 =	07	20
Maritimo — ——		12	17	09	Cape Formosa -	- 04	15 5	06	40
Cape Passaro——	36	38 7	15	40日	New Callabar -	-04	42 =	108	33 tz
Malta	35		14	32 =	Old Callabar—		10	00	45
Corfu -	39	42 5	20	06 H	River Camaroons -	-03	250	10	10
		15 E	21	00 9	River Angra—	00	50	10	019
Zant-	37	46 =	21	14gitud	Cape Lopez				5509
Morea ———	36		21	32 5	River Congou -		40 5	15	25 5
Lemnos		59 "	25	37 6	Angola —	08	57	1.5	56
Scio ———	-38	22	26	12	Cape Negro -	-16	08 2	12	31
C. St. John West-]	1				Cape St. Thomas-	-24	102		
end of Candia	35	15	24	00	Cape Bona Esperance	24	07 6		43
CapeSolomonEast } end of Candia	35	00	27	08		- 1			3)
					The Wef	tern	lilands	•	
City of Rhodes —	- 30		28	05		1 197			
West end of Cyprus	5 34	57	32	23	Corvo ———	-139	54	130	55
East-end of Cyprus	35	31	35	00	Flores -	- 39	32 2		CAS
		1	1		Fial -	- 38	32 North	28	15
					Pico —	- 38			20 5
The Coast of B	arbo	ary and	G	iney.	St. George	138	52 57 06	26	03
	113,00				Tercera -	-38	57 =	25	34
Cape Spartel -	-135	50.	05	49	St. Michael -	-38	065	23	34 36
Sallee -	- 22	13	26	25		-136	59	23	38,
Cape Cantin-	- 32	36	09	10		.,	- , ,	13	
Cape de Geer -	-30	27 04 2 41. 5 32 5	10	06	The Can	arv 1	Mande		
Cape Bajadore -		04 7	115	35 ₹	I ne can	ary i	manus	1	
Cape Olerado -		41.9	115	500	Ferro	-127	54	1.7	40
Cape Blanco -	20	325	17	35 1		- 28		17	45
Senegal-	- 15	281	16	Jongitu 25 20	Gomera	28		17	30
Cape de Verde-		42	17	2009	Tenariff —	28	23		
River Gambia —	- 13		15	31 8	Madera West-end-		- 3	1 -	28
Sierralion —	- 08	36	12		Porto Sancto	10		17	20
Cape Monferado -				21		23	12	15	26 540 10 36
Cape Palmas	700	05	10		Canaria	27	2 -	15	10
			36		Forteventura	- 28		113	36
Jaque Jaque	- 04	. 16	02	47	Lancerota-	- 29	02	12	AF

A TABLE of Latitudes and Longitudes.

Places Names.	La	titude	Lor	ngitude	Places Names.	La	titude	Lon	gitude
Cape de Verde Islands.	D.	м.	D.	М.		D.	м.	D.	м.
St. Vincent St. Lucia St. Nicholas Brava Fuego St. Jago Isle of May Isle Sal Bonavista The South	17 16 14 14 15 15 16	00 North Latitude 50 8 14 0 05	23 24 23 22 22 22 22	39 West Longitude 48 6 2 2 4 1 6 5 0 2 8 0 7	Cambodia Entrance Cochin — Canton — Amoy or Quemoy — Lampo	20 22 16 02 14 10 14 23 24	23 North Latitude 18 28 05 14 6 35	'87 92 93 102 100 105	35

St. Matthews -	CI	30 S	06	OIW
Ascension ———	07	40 S	14	25 W
St. Hellena -	16	00 S		
Fernandepo -	02	40 N	10	30 E
Princes —	01	40 N	09	15 E
St. Thomas -	00	00	08	20 E
Annabona-	02	10 S	07	27 E

The Coast on the Main Continent in the East-Indies.

Cape Lagulias	34	54 S	21	20
Cape Corientes —	23	40 S	36	17
Mosambique-	15	04 S	41	10
River de Fugos-	00	14 S	41	15
Cape Bassos -	04	06	47	38
Cape Guardasoy -	11	44	51	20 2
Cape Rofulgat -	22	41	59	45 🖺
Cape Muca -	23	32 Z	59	45 €
Buffera	29	45 7	49	2000
Surrat	21	10 =	72	25 €
Goa	15	31 2	73	500
Callicut -	11	165	75	30
Cochin —	09	54 6	75	55
Cape Camarine -	07	50	77	25
Fort St. George -	13	11	80	32
Dew Point -	116	08	81	32

Islands in the East-Indies.

Madagascar S. end or St. Lau	25	47	46	10
rence — N end	12	10	51	05
Mayetta —	13	10	45	38
Mohilla ————	12	05	44	23
Comero —	11	408	43	50
	16	30 €	42	40
Mauritius ———	20	10	52	55
Diego Roys —	19	50 m	61	30
Romiras de Castelamas	28	45	67	17 =
Amfterdam	38	40	72	45 9
St. Brandon ——	16	38	64	3000
	08	40	68	25 E
Quabella —	03	53	52	360
Bassos de Chagos -	06	55	68	45
Yas de Diego Rays	00	20 -	72	00
Maldivia N end	07		73	04
S. end	00	25 5		22
Malique -	00	00 E		58
Sacatra ———	12	21 5	100	05
Abdeleur —	12	04 "	53.	04

Places Names.	Latitude	Longitude	Places Names.	Latitude	Longitude
Islands in the East- Indies.	D. M.	D. M.	The Coast of America in the South		D. M.
C. Gallo, in Zeloan Yas de Amber — Andaman — Nicobar Sumatra NW. end Verkins Island — Nassau Island — Bencola— Sumatra SE. end — Engano Selam — Princes Island — Bantam in Java — Batavia — Java E. end — Straits of Sundy — Borneo S. Point — Bandy Isles —	orth Latitude or 11	52 30	Cape St. Sebastians Cape St. Lucia— Cape Corientes— Aquapulco— Aquatulco— Guatimala— Panama— Bay Bonaventura— Isle Gallopega— Cape del Ajugo— Lima— Arica— La Serena— Juan Fernando— Baldivia— Port Steven— Cape Victory— Cape Horn——	North Latitude 17 05 Latitude 17 05 Latitude 18 29 00 12 15 29 00 12 15 29 00 15 29 46 50 66 50 66 50 66 50 66 50 66 50 66 50 66 50 66 66 66 66 66 66 66 66 66 66 66 66 66	101 00 X 81 52 H 78 06 D 90 10 P 84 50 H 77 30 C 73 10 76 22 83 18
Celebes S. end N. end Mindano W. point Borneo N. point — Luconia SW. point Anian S. point E. point Formofa S. point N. point Piscadore Isles — Island Chusan SE. point SW. point SW. point	05 10 01 40 06 40 07 10 12 30 18 35 07 19 55 1 22 00 11 25 30 10 25 30 10 25 30 10 26 30 10 27 30 10 28 30 10 28 30 10 28 30 10	119 07 121 20 119 15 113 05 120 10 120 05 107 00 109 55 119 56 120 45 118 35 120 35 140 30 128 30	Magellan E. end — River Julian — Cape Blanco near River Camaroons Buenos Ayres or River Plate — River Grand— St. Katherines — Cape Frio— Spirito Sancto — P. Segura— Bay Modos Sanctos River St. Francisco	52 CO 48 40 46 50 Wouth Latitude 36 10 Latitude 27 50 de 19 59	75 ° 5 74 34 72 ° 7 × 5 57 54 5 52 ° 0 ° 9

Places Names.		titude	Lor	Longitude		
The Coast of Brazil, &c.	D.	м.	D.	м.		
Cape St. Augustine Cape Roque Tristian de Cunha Trinidada	08 05 37 20	35 S 00 S 05 S	35	20W 47W 24W 00W		

Main Continent in the West-Indies.

R. Amazons Ent	00	00	49	56
North Cape	02	05	49	56
Surinam	06	25	56	50
Oronoque	08	157	59	25 €
Cape Conquibaca—	12	400		42 9
Carthagena -	10	285	75	21
Scots Settlement -	08	30	78	45 9
Nicaragua Entrance	11	25 0	84	1500.
Cape Catoche -	21	10 5	86	10 5
Campeachy —	19	300	92	100
La Vera Cruz -	19	12	97	48
Efcondido	30	20	89	30
Cape Florida -	24	57	80	30

The Caribbee Islands.

Trinidado	10	15	50	17
Tobago W. end -	11	10	59	10
Granado	11	57	60	20
Barbadoes -	12	58	58	50
St. Vincent	13	12 Z		12 \$
St. Lucia -	13	55 7	60	04 5
Martinico —	14	43	60	545
Dominico-	15	23 2	60	3000
Marigallante-	15	58 2	60	20 =
Guardalupe	16	108	61	15 6
Monferat -	16	45	62	15
Antigua	17	05	61	45
Nevis -	17	05	62	32
St. Christophers -	17	13	62	40
Barbuda -	17	56	50	40

Places Names.	La	titude	Longitude		
	D.	M.	D.	М.	
St. Bartholomew —	-	52	6z	06	
St. Martins -		06	52	10	
Anguilla -	18	17	52	13	
Virgins	18	30 Z	1 7	25 €	
St. Cruz -	17	52 3		30 €	
Bieque —		00 =	153	155	
Porto Rico St Johns		30 2	65	37 5	
St. Domingo Hisp	18	25 =	69	30 =	
Port Royal Jamaica	17	40 0	76	32 2	
East end of Cuba -	4	15	73	55	
Havanna —		40	82	55	
Bay of Hondy -	22	45	82	40	
Cape St. Anthony-	21	45	185	32	

Babama Islands.

Bermudas —	32	25	63	40
N. point of Baha-]	28	00	78	
ma Bank —)		4 7 11	, ,	35
Bahama Island —	26	50	79	36
Abacco S. point -	26	00	73	46
Harbour Island	25	37	76	47
Andros N. point -	25	10	78	50
Providence	125	000		20 \$
Illathera S. point -	- 24	403		56 F
Cat Island	- 24	25	75	095
Watling Island-	- 24	03 1		3509
Rum Key -	23	45		50 5
Exuma —	- 23	22 0	75	55 0
Crooked Ifland			1'3	22.0
N. point -	22	56	74	12
Atkins Key -	- 22	17	74	05
Meraparvouz -	- 21	58	74	45
Atwoods Key	- 23	10	73	35
French Keys	- 22	40	73	40
	- 22	35	72	46
** "	21	17	73	55

Places Names.	Lat	itude	Lon	gitude	Places Names.	La	titude	Lon	gitu
Babama Islands.	D.	М.	D.	м.	The Coast of Hud- Son's Bay and Straits	D.	M.	D.	М
Heneago -	20	52 N	73	46W	Buttons Isle ——	60	25	66	27
Caicos Bank N.]		50 N	1. 15	15 W	Cape Charles -		10	75	35
Point J				o8W		62	35	77	55
Turks Island		35 N	70	06W	Mansfield Isle —	2 / 1	42	80	30
Abrolho N. point-		35 N		00 W		54	55	78	58
Plate Wreck —	- 20	10 N	08	15W	Ruperts River —	51	30 7	79	26
					Albany River -				50
The Coast of Car	olina,	Virgi	ma,	Mary-	The Cubbs ———————————————————————————————————	154	10	82	40
1 J P Cl	- 17	F	-1-	d and	C. Henrietta Maria				30 58
land, Pensilvani	a, IN	ew En	gian	u, and	Port Nelson ————————————————————————————————————	57	10 2		58
Newfoundland.					Cape Churchill——				20
					Cape Southampton Shark Point ———			86	48
Charles Tarra	1.1		1					82	55
Charles Town up-		45	78	46	Nottingham Isle -			79	53
on Afhly River	1				Q. Ann's Foreland	63		74	55
Cape Hatteras —		15	74	20	Resolution Isle —			65	04
Cape Henry ——		00	75	24	Cape Farewell —	159	45	46	45
Cape Charles —		16	74	16					
Cape Hinlopen-		50	74		The Coast of Icela	nd.	Green	and.	No
Long Island -		50	72			,		,	-10
New York —		58	73		Zembla, and	No	rthern	Iffee	1
Cape Cod		12	68	,,	Limoin, and	-10	- and I if	-1103	
Boston ———	- 42	30	69		6 15	100			
Cape Sable —			64	-				14	33
Isle Sable ———	- 44		59	01 🕏	Bargazar Point-			16	35
Cape Britain—	-46	00	58	305	Whales Back -			20	33
Quebec	+ 46	55	69	48 0	Merchants Forelan	d 63	25	17	05
Bay of Breft -	- 52	102	150	57 3	Halliford -			34	43
Bell Island -			55	35 de 48	Fair Foreland —		202	26	27
Cape St. John —			52	48	Grims Island ——	- 67	15	22	43 27 34
Cape Bonavista-			52	12	Westmania Isles -		30	22	24
Trinity Bay Ent			52		Ifles of Fero —	- 62	06	los	00
Conception Bay .	-48	20	52	0	Beerenberg, or				
St. John's Harbou	r 48	00	51		John Main's Isle	71	45	104	30
Bay of Bulls	- 47	50	51		Point Look-out -		25	15	36
Cape Race -	-46	40	51		Horn Sound-	- 76		13	36
Cape St. Mary-	-47	10	53		Fair Foreland -			100	36
Placentia -	-47	45	53	0	Hacluits Foreland-		55	11	00
Cape Roy	-48	00	57		Helie's Sound -	- 78		2	100000
	1	33	1,1			1	55		30

Places Names.	La	titude	Lor	ngitude	Places Names.	La	titude	Lor	gitude
The Coast of Iceland, Greenland, Nova Zembla, and Nor- thern Isles.		м.	D.	м.		D.	м.	D.	м.
Archangle Bar — Crofs Island — Sweetnose — Kilduyn — North Cape — Surroy — Tromsound — Læfort SW. point— Dronton — Stadland — North Bergen — Naze of Norway — The Coast in the	77 74 75 74 75 70 69 65 64 66 68 69 71 70 68 63 62 60 57	19 N	36 34 31 23 16 15 9 10 04 05 07 Bai	57 E	Gottenburgh Elsimore Copenhagen Valsterborn Kalmer Stockholm Wybourg Petersburgh Narva Revel Riga Derwinda Koningsberg Dantzick Wisby in Gotland Bornholm Straelsound Lubeck Anout Lesou Scaw	56 69 50 59 59 57 57 54 54	25 =	28 24 25 22	East Longitude 25 51 56 30 456 50 30 20
Christiana -	58 59 57	54 N 20 N 53 N	10	20 E 00 E 45 E					

The Latitudes of any two Places being given, to find the Diffrence of Latitude between them.

Rule, If the Latitudes are both North, or both South, subtract the Lesser from the Greater, the Remainder will be the Difference of Latitude.

But

But if one Latitude be North, and the other South, then add them together, and their Sum will be the Difference of Latitude.

Example 1st. What is the Difference of Latitude between the

Lizard, and Barbadoes.

Lizard, in Latitude _____ 49° 57' N.

Barbadoes, in Lattiude _____ 12 58 N.

The Difference of Latitude _____ 36 59

Example 2d. What is the Difference of Latitude between Jamaica and Cape Bona Esperance.

Jamaica, in Latitude — 17 40 N. Cape Bona Esperance, in Latitude 34 07 S.

The Difference of Latitude — 51 47which Degrees being multiplied by 60, and the odd 47 Min. 60 taken in, will give the Difference of Lat. in — 3107 Miles.

Rules for Latitude.

The Latitude fail'd from, and the Difference of Latitude being

given, to find what Latitude the Ship is come into?

Case the 1st. When you sail from North Latitude to the Northward, or from South Latitude to the Southward, add the Difference of Latitude (it being first brought into Degrees, if need be, by dividing it by 60) to the Latitude sail'd from, the Sum will be the Latitude you are come into, of the same Name with the Latitude sail'd from.

Example 1st. A Ship from a Place in the Latitude 14 10 N. fails to the Northward till she makes her Difference of Latitude 04 21: What Latitude is she come into?

Latitude fail'd from — 14 10 N.

Difference of Latitude — 04 21

Latitude come into — 18 31 N.

Example 2d. A Ship from Latitude 29 17 S. fails to the Southward, till she makes her Difference of Latitude 374 Miles: What Latitude is she come into?

Latitude fail'd from ______ 29 17 S.
Diff. of Lat. 374 Miles, divided by 60 makes 06 14
Latitude come into ______ 35 31 S.

Case the 2d. When you sail from North Latitude to the Southward, or from South Latitude to the Northward, subtract the Difference of Latitude, if least, from the Latitude sail'd from, the Remainder is the Latitude come into, of the same Name with the Latitude you sail'd from.

But if the Difference of Latitude be biggest, then subtract the Latitude from the Difference of Latitude, the Remainder will be the Latitude come into, of a contrary Name to the Latitude you

fail'd from.

Example 1st. A Ship from Latitude 49 14 N. fails to the Southward, till her Difference of Latitude be 521 Miles: What Latitude is the come into?

Latitude fail'd from
Diff. of Lat. 521 Miles, divided by 60, makes 08 41

Latitude come into — 40 33 N.

Example 2d. A Ship from Latitude 4 18 S. fails to the Northward, till her Difference of Latitude be 10 24: What Latitude is she come into?

Latitude fail'd from — 04 18 S.

Difference of Latitude — 10 24

Latitude come into — 06 06 N.

Rules for Longitude.

The Longitudes of any two Places being given, to find the Difference of Longitude between them..

Rule. If the Longitudes are both East, or both West, subtract the lesser from the greater, the Remainder will be the Difference of

Longitude.

But if one Longitude be East, and the other West, then add them together, and their Sum (if less than 180 Degrees) will be the Difference or Longitude; but if it be more than 180 Degrees, then subtract it from 360.00, and the Remainder will be the Difference of Longitude.

Enample 1st. What is the Difference of Longitude between Cape Finister and Antigua?

Cape Finister, in Longitude — 09 40 W. Antigua, in Longitude — 61 45 W.	
The Difference of Longitude 52 05 Example 2d. What is the Difference of Longitude	between
Barcelona and the Rock of Liston? Barcelona, in Longitude — 02 18 E. Rock of Liston in Longitude — 09 50 W.	

The Difference of Longitude—— 12 08

Example 3d. What is the Difference of Longitude between the

Exceeds 180 00—203 10
Subtract it from—360 00

Remains the Difference of Longitude _____ 156 50

The Longitude fail'd from, and the Difference of Longitude be-

ing given, to find what Longitude the Ship is come into?

Case 1st. When you sail from East Longitude to the Eastward, or from West Longitude to the Westward, add the Difference of Longitude to the Longitude sail'd from, the Sum (if less than 180 Degrees) is the Longitude come into, of the same Name with the Longitude you sail'd from:

But if the Sum should be more than 180 Degrees, then subtract it from 360.00, and the Remainder will be the Longitude you are come into, of a contrary Name to the Longitude you sail'd from.

Example 1st. A Ship from Longitude of 48 21 E. fails to the Eastward, till she makes her Difference of Longitude 287 Miles. What Longitude is she come into?

Longitude fail'd from ______ 48 21 E.

Difference of Longitude 287 Miles, or 04 47

Longitude come into ______ 53 08 E.

Example 2d. A Ship from the Longitude of 178 47 West, sails to the Westward till her Difference of Longitude be 12 17: What Longitude is she come into?

Rules for Longitude.

Longitude fa	- 178	47 V	V.	
Difference of	Longitude-	- 12	17	
	Exceeds 180.00-	- 191	04	
	Subtract it from	360	00	
Remains the	Longitude come into -	- 168	56 F	Ξ.

Case the 2d. When you sail from East Longitude to the West-ward, or from West Longitude to the Eastward, subtract the Difference of Longitude (if it be least) from the Longitude you sail'd from, and the Remainder will be the Longitude come into, of the same Name with the Longitude sail'd from.

But if the Difference of Longitude be the biggest, then subtract the Longitude from the Difference of Longitude, and the Remainder will be the Longitude come into, of a contrary Name to the Longitude sail'd from.

Example 1st. A Ship from Longitude 98 17 East, sails to the Westward till she makes her Difference of Longitude 14 21: What Longitude is she come into?

Longitude fail'd from -	- 98	17 E.
Difference of Longitude -	- 14	21
Longitude come into	- 83	56 E.

Example 2d. A Ship from Longitude 44 21 West, sails to the East-ward till her Difference of Longitude be 81 42: What Longitude is she come into?

Longitude fail'd from	- 44	21 W.
Difference of Longitude ———	- 81	42
Longitude come into	- 37	21 E.

Here follows a Table of Meridional Parts, to every Degree and Minute of Latitude

M	od	1 d	2 d	3 4	4 d	5 d	6 d	7 d)	8,d	9 d	to d	11d	12 d	13 d	M
0	-0	60	120	180	240	300	361	421	482	542	603	66+	725	787	0
4	1	61	121	181	241	301	362	422	483	543	60.	665	716	788	. 1
2	2	(2	122	182	242	302	363	423	484	544	6:5	606	727	789	2
3	3	63	123	183	243	303	364	424	485	545	600	667	728	790	3
4	4	64	124	184	244	304	365	425	485	546	607	668	729	791	4
5	5	65	125	185	245	305	366	426	487	547	608	669	730	792	5
6	6	66	126	186	246	305	367	427	488	548	600	670	731	793	6
7	7	67	127	187	247	307	368	428	484	549	61-	671	732	794	7
8	8	- 68	128	188	248	308	379	429	490	550	611	672	733	795	. 8
9 10	_9	69	129	189	249	304	370	430	491	551	612	673	735	796	9
10	10	70	116	190	250	310	371	431	492	552	613	674	736	797	10
11	11	71	131	191	251	311	372	432	493	553	614	675	737	798	11
12	12	72	132	192	252	312	373	433	494	554	615	676	738	799	12
13	13	73	133	193	253	313	374	434	495	555	616	677	739	800	13
14	14	74	134	194	254	314	375	435	496	556	617	678	740	801	14
15	15	75	135	195	255	315	376	436	497	557	618	679	-41	802	15
16	16	76	136	196	255	316	377	437	498	558	619	680	742	803	16
17	. 17	77	137	197	257	317	378	438	499	559	620	681	743	804	17
18	18	78	138	198	258	318	379	439	500	560	621	682	7+4	805	18
19	19	79	139	199	259	319	380	440	501	561	622	683	745	903	19
20	20	80	140	200	260	320	381	441	502	562	623	684	746	807	20
21	21	81	141	201	261	321	382	442	503	563	624	685	7+7	808	21
22	22	82	142	202	262	322	383	443	504	564	625	686	748	809	22
23	23	83	143	203	263	323	384	444	505	566	625	688	749	810	23
24	24	84	144	204	264	324	385	445	506	557	627	689	750	811	24
25	25	85	145	205	265	325	386	446	507	568	628	690	751	812	25
26	26	86	146	206	266	326	387	447	508	569	629	691	752	813	.6
27	27	87	147	207	267	327	388	448	509	570	63c	692	753	814	27
28	28	88	148	208	268	328	389	445	510	571	632	693	754	816	28
29	29	89	149	205	269	329	390	45C	511	572	633	694	755	817	29
30	30	90	150	210	270	330	391	451	512	573	634	695	756	818	30
31		91	151	211	271	332	392	452	513	57+		696		819	31
32		92	152	212	272	333	393	453	514	575				820	32
33		93	153	213	273	334	394	454	515	576		698			33
34				214	274	335	395	455	516	577					34
35				215	275	330	396	450	517	578				823.	35
36				216	276	337	397.	45?	518	579			762		36
37	37			217	277	338		458	519		641	70:		825	137
38	38			218	278	335	399	455	520		642	70	764	826	38
39	39		159		279	3+0	400	460	521	582	643	704	765	827	35
35					280	341	401	461	522	583		70			40
41	40				281		402	462	523		64	700			14
					282	342 343	403	463	524			2			1
42	42			223	283	344	404	464	525	586					4
4	43		164	224	284	345	405	465	526						44
4.	44					346	405	466							4
4	45				A CONTRACTOR OF THE PARTY OF TH			467	528						40
+	47	1			287	348		468	529						4
4	48					345	409	469				71			4
12	40			229		350		470	531						140
50 5	49	-	_	-	-	-	411	470	531		-		-	-	50
150	50					351			532			1 21			13
5	51					352								839	51
.5						353								840	5
5		11	3 17											8,1	
5									536	59	7 65				
5															
5						35	417				9 66				5
5															5
5											1 66	2 72			
	91, 5	9 ,11	9 17	9 23	255	360	420	48	1 54	1 60	2 66	3 72	41 -8	1 841	5

M	140	15 d	16 d	17 d	18 d	19 d	zod	21 d	22 d	23 d	24 d	25 d	26 d	27 d	IN
C	848	910	973	1035	1098	1161	1225	1289	1354	1419	1484		1616	1584	1
1	844	911	974	36	99	63	26	90	55	20	85	51	18	85	
2	85	913	975	37	1100	64	27	91	56	21	86	52	19	86	1 :
3	852	914	9.6	38	01	65	28	92	57	22	87	53	20	87	
4	853	915	977	39	02	66	29	93	58	23	88	54	21	88	
5	854	916	978	41	03	67	30	95	59	24	90	56	22	89	1
6	855	917	979	42	05	68	32	90	60	25	91	57	23	90	
7	856	918	980	43	06	69	33	97	61	26	92	58	24	. 91	
8	857	919	981	44	07	70	3+			27	93	59	25	93	
9	850	920	982	45	08	71	35	99		28	94	60	26	94	14
10	859	921	983		1109	1172	1236	1 300			1495	1561	1628	1695	10
11	860	922	984	47	10	73	37	01			96	62	29	96	1
12	861	923	985		11	74	38				97	63	30	97	1:
13	862	924	986		12	75	39	03			98		31	98	1
14	863	925	987		13	76					99	65	32	99	11
15	864	926	988		14	77	41				1500	67	33	1700	1
16	855	927	489		15		42				02	68	34	01	10
17	867	928	990		16	79	43				03	69	35	03	1
18	868	929	991	54	17	81	44	08		38	04	70	37	04	1
19	-	930	9/2	55	-		45	10		-	05	7!	38	05	11
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22	871	933	995	58	21	85		1 13			08	74	41	08	2
23	872	934	997	55	22	86	50	1 14			09	75	42	09	2
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25	874	>36	999		25		52	16			11	78	44	12	2.
26	875 876	937	1000	63	26	89	53	18			13		45	13	1.0
27	877	938	1001	64	27	90	54	15			14		47	14	2
18	878	939	1003	60		91	55			49	15	81	48	15	2.
29	-	941		-	29	-3,	50		-		-		49	16	125
30	879	9+2	001		1:30	1193	1257	1321		1451	1517	1583	1050	1717	30
31	880	943	05	68	31	9-	58	22		52	18	84	51	18	3
32	883	544	06	69	32	95	59	24		53	19	85	52	20	32
33		945	07		33	96	61	25		55	20	86	53	21	3
34	884	946	03		34	99	62			56	21	88	54	22	34
15	886	948	10		35	1200	64				22	89	56	23	3.
36	857	9+9	1 11			01	65			58	24	90	57	24	34
37	888	950	12		38		66	30		60	25	91	58	25	3
38	889	951	13	75	39	01		31	56		27	9:	59	26	3
39 +0	_				1-32	120,		-	1.70-		_	93		27	3
40	840	952	1014	1077	1140	120,	1268	1332	1397	1462	1528	1594	1661	1729	4
41	891	953	15		1 4.	03	69	33		63	29	95	62	30	4
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19 50	8.9	962	1025	1438		-		42					71	39	13
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51	901	963			5	16	80	44	10	74	40	06	73	41	51
52	992	964	27					45	11	75	41	08	75	42	50
53	903	965			54			47		76	42	05	75	43	5
54	904	966	. 29			15		48		77	43	10	77	44	54
55	905	968	30			20	84		13	79	44	11	78	45	5
56	906	969	31		57	21	86	45	14	81	46	12	79	47	54
57 58	907	970	32				87	52	16	82	47	13	80 81	48	57
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3	55	23	92	62	32	03	75	48	22	96	72	49	27	05	
4	56	24	93	63	33	04	76	49	2;	98	73	50	28	07	
5	57	25	94	64	34	C5	78	50	21	99	75	51	29	09	
6	58	26	95	65	35	07	79	52	25	2400	76	53	31	10	
7	50	27	96	66	37	c8	80	53	27	01	70	54	32	1:	1
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10	1702	18311		1979	2040	2111	2184	2256	2330	2405	2481	155	2636	2715	1
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112	65	35	02	72	43	14	86	59	35	08	84	60	38	18	1:
13	66	34	03	73	44	15	87	60	34	09	85	6.	40	19	1
14	67	35	0.5	74	45	16	88	6:	35	10	85	6:	41	20	14
15	68	37	06	76	46	17	90	63	37	11	87	64	42	22	1
110	69	38	07	77	47	19	91	64	38	13	89	66	44	23	10
17	70	39	c8	78	48	20	92	65	3.0	14	90	67	45	24	1
18	72	40	CO	79	50	21	93	66	40	15	91	68	46	26	1
19	73	411	10	83	51	22	, 94	68	42	16	92	69	48	2	1
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	78		16	86		28	2200	72	46	31		75	53	32	2
24	80	47	17	87	57	29	13.00	74	48	23	99	76	54	33	24
-	81		100	88	58		C2	75	49		2500	77	55	35	2.
26	82	49	18	90	59	31	03	76	50	29	01	78	57	36	26
27		50	20		60	32	C4	77	51	27	03	80	58	37	2
28	88	52	21	91	61	33	05	79	53	28	0+	81	59	39	28
29	84	58	22	92	68	34	-07	80	54	29	05	82	61	40	25
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32	87	55	25	95	66	38	10	83	58	33	CO	86	65	44	3:
313	80	57	27	97	67	39	11	85	59	34	10	88	66	46	3
34	90	58	28	98	6 _U	40	13	86	60	3.5	12	8,	67	47	
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36	92	6a	30	2000	74	43	15	88	63	38	14	91	70	50	35
3.7	93	612	31	01	72	44	16	90	64	39	15	93	71		30
318	94	62	32	02		45	17	91	65	40	17		73	51	37
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39			34	-	75 2076		19		-		-	- 93		_54	35
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41	98	66	36	06	77.	49	21	95	2368	44	21	91	76	56	41
42	99	68	37	07	78	50	22	56	70	45	22	99	78	2755 56 58 59 60 61 63 64 66 67	41
43	1800	69	31	OB	79 80	51	24	97	71	4	23		79	59	4
44	OI	70	39	10	80	52 53	25	58	73	48	24	02	80	60	44
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40	03	72	42	12	83	55	27	2301	75.	51	27	04	82	63	40
47	05	73	43	13	84	56	28	02	70.	51	28	C.5	84	6	4
116	06	75	44	14	85	57	30	03	78	53	30	07	86	66	1
49	1838	76	45	15	86	58	31	04	79	54	31	08	8,	.62	1
50	18.0	1877	1046	2017	2000	2159	223	2306	2380	2450					=
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54	13	18	51	21	92	14	37	11	85	61		15	94	768 70 71 72 74 75 76	54
54	14	83	52	22	94	65		12		62	38	16	95	75	15
56	16	84	53	24	96		39	13	88	63		17	96	76	5.
57	16	85	55	25	96	- 68	41	14	89	64	41			78	15
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10			2,60		3130	3217	3306	3357	3490	3585	3681	378c	3882	3985	15
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12				47	33	20	09	13400	93	88	85	84	85	89	111
13						22	11	02	95	90		85	87		12
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115	02	84			37	25	14	05	98	93		85	90		14
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27	18	2900	83	68	55	41	32		15	10		07	09	14	26
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31	- 24	06	89	74	60		38	30	23	18	16	16	18	22	34
32	25	07	91	75	62	50	40	31	25	20	17	17	19	24	32
33	26	08	92	77	63	51	41	33	25	22	19	19	21	26	
34	28	10	93	78	65		43	34	28	23	- 21	21	23	28	33
35	29	. 11	95	80	66		44	36	29	25	22	22	25	29	34
36	30	13	95	81	68	56.	46	37	31	26		24	26	31	35
37	32	14	98	83	69	57	47	39	32	28	26	26	28	12	37
38	33	15	59	84 85	71	59 60	49	40		30	27	22	30		37
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40	2836	2918	2002	2087	3173	3262	3352	3443	1.00	2622	2721		-000		32
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142	39	21	05	. 00	76	63	55	45	39	34	24	32	35	40	41 42 43 44
43	40	22	06	91	78	66	56	48		30	34 36 37	34		42	42
144	41	24	07	93		68	58	30	42	30	27	36	38	44	43
145	43	25	09	94	79 81	69	10	51	43	33	39	38	40	45	44
44 45 46 47 49 49 55 55 55 55	44	25	10	95	82	71	59	51	45		39	35	42	47	+5 46 47 48 49 5C
147	45	23	12	07	82 84 85	72	62	51	47	43	41	41	44	49	46
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131	. 21	31	17 19 20	03	50	78	08	60	55 56	-51	49	49	52	58	51
152	52	3.5	191	05	91 92 94	80	70	62	56	52	50	51	54	60	51 52 53 54 55
153	54	30	. 10	05	. 98	. 81	71	64	58	54	52	51	56	6	59
54	5.5	37	21	07	94	83	73	65	59	55	54	55	58	63	23
54	53	39	231	. 08	95	84	74	67	60	57	. 55	56	59	65	39
56	58	40	24	10	97	86	76	68	(2	59	57	58	61	62	23
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3	79	88	4300	15	33	55	81	13	46	8:	31	82	39	03	1
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3	15	25	38	54	74	97	2.	56	92	34	80	33	93	59	1
+	17	27	40	56	70	99	26	58	95	36	83	36	95	62	1
5	19	29	42	58	78	4701	29	60	97	38	85	39	98	65	2
6	21	31	44	60	80	03	31	63	99	41	88	41	5701	68	1
7	22	32	46	62	82	05	33	65	5102	43	90	44	04	71	12
8	24	34	47	64	84	07	35	67	C4	46	93	46	06	74	1
9	26	36	49	66	63	10	37	69	06	48	95	49	09	76	2
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3	33	44	57	74	94	18	44	78	15	58	03	57	17	85	1
4	35	46	59	76	96	20	48	81	18	60	08	62	23		1
5	37	47	61	78	98	22	5c	.83	20	61	11	65	25	91	
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9 0 1	4146	+257	4370	84 86 4488	1608	4733	1861	1994	5132	5275	5423	5578			1
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5 6 7	55	66	80	97	18	43	72	05	43	87	33	91	50	19	1
6	57	68	82	99	20	45	74	08	46	89	38	94	53	22	1
7	59	70		4501	23	47	76	10	48	92	41	96	56	25	1
8	61	72	84 86	03	2.5	50	79	12	51	94	43	59	61	20	B
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1	66	77	4390	4507	+029	4754	1003	3017	5155	5299 5301	5448	5604	5767	5937	1
2	68	79	92	09	31	58	85	19	58	5301	51	07	70	40	1
3	70	81	94		33	60	87		60	04	54	10	72	43	1
		83		13	35	62	90	23	62	06	56	112	75	46	1
4	72	85	98	15	3.7		92	26	65	09	59	15	78	48	1
5	73	87	99	17	39	64	94	28	67	11	61	17		51	
6	75	89	1401	19	41		96	30	69	14	64	20	83	54	
8	77		03	21	: 43	69	98	.33	72	16	66	23		57	
,	79	91	07	23	45	71	4901	35	74	19	69	25		60	НE
	- 50	74	- 0/	-3	47	73	1 03	Q.	1 76	21	71	1 38	1 -92	63	3

M	70 d	71 d	72 d.	73 d	74 d	75 d	76 d	77 d	78d	79d	180 d	81 d	82 d	83 d	N
0	5906	5146	5335	6544	6746	6970	7210	7+67	1745	8046	. 5	8739	9145	9600	-
1	69	49	38	38	49	74	14	72	49	51	6.	45	55	14	
2	72	52	41	41	53	78	18	70	54	55	87	52	60	22	1
3	75	55	45	45	57	82	22	81	59	6	93	58	6	31	
4	78	58	48	49	60	86	27	85	64	67	98	65	74	39	1
5	84	64	51 54	52	68	94	3:	90	69	72	10	71	62	47	
7	85	67	58	55	71	97	35	98	74	83	16	78 84	96	55 64	
8	89	70	61	62	75	7001	43	7503	83	88	22		9203	72	
9	92	73	64	65	79	05	4	0.0	88	93	27	97	11	80	
10	5,95	6177	5367	6,69	5782	7009	7252	7512	7793	8099	5433	8804	9218	9689	7
11	98	80	71	72	66	13	36	16	98	8104	39	10	25	97	1
12	6001	83	74	76	90	17	60	21	1803	09	45	17	33	\$706	li
13	04	86	77	79	93	21	64	25	60	15	51	23	40	14	1
14	07	89	80	83	97	25	68	30	13	20	57	30	48	23	1
15	10	92	84	85	1089	29	73	35	17	25	63	36	55	31	1
16		95	87	90		33	.77	39	22	31	69	43	62	40	10
17	16	98	90	93	06	37	81	. 44	27	36	74	49	70	48	1
18		6201	94	9	12	41	85	48	32	41	80 86	56	77	57	1
15		05	97	6600	15	45	89	53	37	47	_	63	85	65	1
2c	6025	6208	6400			7048	7294	7557	7842	8152	8492	8869	,292	9774	2
21	28	-11	03	07		52	98	62	47	58	98	76	9300	83,	2
12	31	14	07	10		60	7302	65	52	63	8504	83	07	91	2
23	34	17	10	14		64	41	71 76	57 62	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	16	89	15	9800	2
24 25		23	17	17	-0	68	15	80	67	74	22	96 8903	22	09	2
26	43	26	20	24	41	72	19	85	72	85	. 28	09	30	17	2 2
27	46	30	23			76	23	89	77	90	34	16	45	35	2
28	49	33	27	31	49	80	28	94	82	96	40	23	53	44	2
29	52	36	30		53	84	32	99	87	8201	46	30	60	52	2
30	5055	6239	6433	6639	6856	7088	7336		7892	8207	8552		9368	9861	-
31	58	42	37	42	60	92	41	08	97	12	58	43	76	70	3
32	61	45	40	46	64	96	45	12	7902	18	65	50	83	79	3
33	64	49	43	49	68	7100	49	17	07	23	71	57	91	88	3
34	67	52	47	53	71	04	53	22	12	29	77	63	99	97	13
3.5	70	55	50	56	75	08	51	26	17	34	83	70	9407	9906	13
31	73	58	53	60	79	12	62	31	22	40	89	77	14	15	3
37	76	61	57	63	83	16	66	36	27	45	95	84	22	24	3
8	79 82	64	60	,	V F		71	40	32	51 56	86c1	91	30	. 33	,
9	62	68	63	70 6674	90	2+	75	45	_37		07	98	38	42	3
10	6085	6271	5467	6674	98	7128	7379	7650 54	7942 48	8262	8614	9005	9445	9951	4
1.1		74	70	77	98	32	84	54	48	67	20	12	53	59	4
12	91	77	73	81	6901	36	88	59	53	73	26	18	61	69	4
13	94	80.	80	85	90	40	92	64	58	79	32	25	69	78	4
4	6100	83	83		13	45	97 7401	73	68	84	38	32	77	87	4
5	03	90	87	95	17	53	06	78		90	44 51	39	85	9996	1
16	06	93	90	99	20	57	10	83	73	8301	57	46 53	93	10005	4
8	09	96	94	6702	24	61	14	87	83	07	63	60	09	10024	1
9	12	99	97	06	28	65	19	92	89	12	69	67	17	10033	4
9	6115	6303	6500	6710	6932	7169	7423	7697	7994	8318	3676	-	9525	10043	
1	18	05	04	13	36	73	27	7702	99	24	82	9074	33	10052	5
2	- 21	09	07	17	40	77	32	06	8c04	29	88	88	41	10061	5
3	24	12	11	20	43	81	36	11	09	35	95	96		10071	5
4	27	15	- 14	24	47	85	41	16	14	41	8701	9103		10080	5
5	30	19	17	28	51	89	45	21	20	47	07	10		10089	5
6	-33	22	21	31	- 55	94	49	25	25	52	14	17		10099	15
7	36	25	24	35	50	98	54	30	30	58	20	. 24	. 81	10108	5
7 8	40	28	28	38	63	7202	58		35	64	26	31	89	10118	5
9	. 43	32	- 31	42	66	06	63	40	40	69	33	38	98	10127	15

M	184 d	85 d	·86 d	87 d	88 d	89 d	M
	10137	10765	11533	12522	13916	16300	_
0	147	776	547	541	945	357	1
8	157	758	561	561	974	416	2
3	166	799	5-6	580	14003	470	3
4	175	811	.590	599	033	537	4
6	185	822 834	620	619	003	599 662	5
7	205	846	634	659	123	726	7
8	214	858	649	679	154	7,2	8
9	224	869	664	699	184	858	9
10	10234	18891	11679	12719	14216	16926	10
11	244	893	694	739	247	956	11
12	254	905	709	759	279	17067	12
13	264	917	724	780	343	135	13
14	283	941	755	821	376	289	15
16	293	953	770	842	408	366	16
17	303	965	785	863	442	445	17
18	314	978	801	884	475	526	
19	324	990		906	509	609	10
20	10334	014	11832	12927	14543	17693 781	20
21	344	027	863	949	613	870	
22	354 364	039	879	992	648	962	23
24	374	052	895	13014	684	18056	
25	385	064	911	036	720	153	
26	395	089	927	059	756	252	
27	405	102	943	104	830	355 461	28
28	426	115	976	126	868	570	29
30	10437	11127	11992	13149	14906	18682	30
31	447	140	12008	172	943	799	31
32	457	153	025	195	983	920	32
33	468	166	041	219	15022	19045	33
34	478	179	058	242	102	174	34
35 36	489	192	075	290	143	450	35
37	510	218	109	314	184	596	37
37	521	231	126	338	226	749	38
39	532	244	143	362	268	500	39
40	10542	11257	12160	13386	15311	20076	40
41	553	270	177	411	354	253	41
42	564 575	284	194	437	398	439 635	42
43.	586	310	229	486	487	843	44
45	597	324	247	511	532	21065	45
46	608	337	264	537	579	303	46
472	619	351	282	563	625	557	47
48	630	365 378	318	615	673	832 22132	48
49				13641	-		50
50	10652	11392	354	668	15770	22459	51
52	674	420	373	695	869	23226	52
53	685	434	391	721	920	23685	53
54	696	448	409	749	972	24215	54
55	708	462	428	776	10024	24842	55
56	719	476	447	804	132	25609 26598	56
57	730 742	504	484	860	187	27992	58
59	758		503	888		30175	
1	To and the same of	100		TALA			119

The Use of the Table of Meridional Parts.

IN this Table the first and last Column of every Page mark'd M, beginning at o, and ending at 59, contain the Minutes answering to every Degree of Latitude, the other Columns mark'd 1d, 2d, &c. contain the Meridional Parts, answering to the Degree of La-

titude they stand under.

So that if you would find the Meridional Parts answering to any Latitude, suppose for Example, the Latitude 51.32, look in the Column under 51d. and right against 32 (in the Column for Minutes) you will find 20, to which prefix 36, the two Figures in the same Column that stands above 20 towards the Left-hand, and it makes 3620, the Meridional Parts required.

Two Latitudes being given, to find the Meridional Difference of Latitude.

Case 1st, If both Latitudes be North or both South, subtract the Meridional Parts of the Leffer, from the Meridional Parts of the Greater, the Remainder will be the Meridional Difference of Latitude.

Case 2d, If one Latitude be North and the other South, then add their Meridional Parts. together, and the Sum will be the Meridional Difference of Latitude. A Q 2

A TABLE of Amplitudes, from the Latitude oo deg. oo min. to the Latitude 12 deg. either North or South.

1	_	1		1		1	1	he	: D	eg	ree	s c	of	La	titi	uad	-	1		1	79	1	4 T	
Degrees of	1		2		3		4		5		6		7		8		ģ		1	0	1	1	1	2
	D	M	D	М	D	м	D	м	D	м	D	м	D	м	D	М	D	м	D	м	D	м	D	M
																					00			
1	21	co	10	00	01	00	01	00	01	00	01	00	10	00	10	00	01	00	01	01	01	01	10	0
2	22	00	32	00	02	00	02	00	02	00	02	00	02	01	02	01	32	01	02	02	02	02	22	0
3	24	00	34	00	03	00	03	00	03	00	04	01	04	01	04	01	04	03	04	04	03	04	03	0
4	74	_			_	_	_	_	-				_	-	-		-	_	_		_		-	
5	25	0	05	00	05	00	05	00	05	01	05	01	05	02	05	0	05	03	05	05	05	05	25	0
í																					06			
7	27	co	27	00	07	01	97	01	07	02	07	02	97	03	07	04	07	05	07	07	07	07	07	C
8																					08			
9	29	00	09	-00	9	01	139	_	09	02	-	-5	3	_	-		13		39		09	_	9	
10	10	00	10	00	10	01	io	01	10	02	10	03	10	04	10	05	10	07	10	10	10	11	10	1
11	11	00	11	00	11	.01	11	01	11	03	11	03	11	05	11	ct	11	80	11	11	11	12	11	1
12	12	00	12	00	12	01	12	01	12	03	12	04	12	05	12	07	12	Oć	12	12	12	13	12	1
13	13	00	13	00	13	01	13	02	13	03	13	04	13	00	13	00	13	10	13	13	13	15	13	. 1
14	14	00	14	00	14	01	14	02	14	03	14	-	14	00	14	- 09	114	10	14	14	14	10	14	1
15	15	00	15	00	15	01	15	02	115	04	15	05	15	07	15	09	15	11	15	15	15	17	15	2
16	16	00	16	01	16	01	16	02	16	04	16	05	16	07	16	00	16	12	1.6	16	16	18	16	2
17	17	00	17	0	7	01	17	02	17	04	17	05	17	08	17	10	7.7	13	17	17	17	20	17	2
																					18			
19	19	00	-	01	19	01	19	0	-	04	-	-	1.9		.9		-9	-5	-	-	19		19	-
																					20			
																					21			
22	22	CC	22	01	22	0:	2 2 2	0	3 2 2	05	22	07	22	10	22	13	22	17	22	22	22	26	22	3
. 23	23	00	23	01	23	0:	2 3	0	23	05	23	08	23	11	23	14	23	18	23	23	33	28	23	3
23,29	23	25	123	3	123	3	133	3.	1-3	33	1-3	30	1-3	4	1-3	71	-3	45	1-3	34	1-3	3	1-4	C

A TABLE of Amplitudes, from the Latitude 13 deg. oo min. to the Latitude 24 deg. either North or South.

	1		1		-			T	he	D	eg	ree	5	of	La	atic	ud	e.	•						-
Degrees of Declination.	,	•	3	•	4	•	5		6		7		8	-	9		20	1	11		22		23	2	4
es of ation.		D	М	D	м	D	м	D	М	D	М	D	М	D	М	D	M	D	M	D	М	D	M	D	M
																								00	
	3	02	03	02	03	02	06	02	05	02	05	02	06	02	07	02	08	02 03	08	02	09	02	10	01 02 03 04	11
	6		10	06	11	06	13	06	15	06	16	06	19	06	21	06	23	56	26	06	28	06	31	05 06 07	34
	8	08	12	08	15	08	17	08	19	08	22	08	25	08	28	08	31	08	34	08	38	08	42	08 09	45
1	11	1.1	17	11	20	11	23	11	27	11	30	11	34	II.	38	11	43	11	48	11	52	11	58	10	03
1	13	13	21	13	24	13	28	13	32	13	36	13	41	13	47	13	52	13	58	14	04	14	10	14	17
	15	16	26	16	30	16	35	16	40	16	45	16	51	15	57	17	03	17	18	77	18	17	25	16 17 18	34
	18	18	30	18	34	8	40	18	45	18	51	18	57	19	05	119	11	19	20	119	28	19	37	19	46
	21	21	35	21	41	21	46	21	53	22	00	22	08	22	, 16	22	25	22	34	122	44	22	55	21 23 24	06
	23	23	38	23	45	23	51	23	59	24	07	7 24	11	24	24	24	34	24	44	24	55	25	07	25 25	19

A TABLE of Amplitudes, from the Latitude 25 deg oo min. to the Latitude 36 deg. either North or South.

	-		7		-1		1		L he	e L)eg	ree	1	of	Li	atit	ua	e	-		1	_	1		-
Degrees of		2!	5	2	6	2	7	2	8	2	9	3	0	3	1	3	2	3	3	3	4	3	5	3	6
S. C.	D		м	D	М	D	м	D	М	D	M	D	м	D	м	D	М	D	M	D	М	D	м	D	М
									1.11						1,000				1958	195.4		00			00
1																						01			14
2																						02			
4																						04			
5																						06			1
	0	0	37	00	41	00	44	00	48	00	52	00	50	08	00	07	16	07	09	07	15	°7 °8	20	07	2
1																						09			
9	10	9	56	10	ói	10	06	ιó	12	10	18	10	24	ıó	31	10	37	10	45	ιó	52	ıí	00	ıí	ó
																						12			
1	1	2	09	12	15	12	22	12	29	12	36	12	43	12	52	13	00	13	09	13	18	13	28	13	3
																						14			
1	4	5.	29	15	37	15	45	15	54	16	03	16	13	16	23	16	34	16	45	16	57	17	11	17	2
																						18			
																						19			5
i	8	10	45	20	0	20	17	20	20	20	41	20	54	21	08	21	22	21	37	21	53	20	10	22	2
1	9	21	0	21	14	21	20	21	31	21	51	22	0	22	19	22	34	22	50	23	07	23	25	23	4
2	0	22	10	22	2	2 2 2	3	22	4	3 2 3	01	23	10	23	31	23	47	24	. 04	24	21	24	40	25	c
																						25		26	
•	3	25	3	2 2	4	6 26	0	0 26	11	6 26	32	2 26	40	27	07	27	20	27	4	28	9	28	20	28	
23,2	29	26	0	5 2	5 i	9 26	3	4 26	4	9 27	0	5 27	2	3 27	4	2 28	0	28	2	2 28	4	129	of	29	1

A TABLE of Amplitudes, from the Latitude 37 deg. oo min to the Latitude 48 deg. either North or South.

	1		1					T	`he	D)eg	ree	3	of	L	atit	ud	e.	-					<u> </u>	-
Declination.	Dear	3	7	•	8		19		10	4	.1	-	ļ2 	4	13		44		15		46		47	4	48
ation.	200	D	M	D	М	D	M	D	М	D	M	D	М	D	М	D	M	D	М	D	М	D	М	D	M
	1 2 3	01	15 30 45	01 02 03	16 32 48	01 02 03	17 34 51	01 02 03	00 18 36 55 13	01 02 03	19 39 58	01 02 04	21 41 02	01 02 04	22 44 06	01 02 04	47 10	01 02 04	25 50 15	01 02 04	26 53 19	01 02 04	28 56 24	01 02 04	29 59 29
	6 7 8	08	31 46 02	07 08 10	37 54 11	07 09 10	43	09	32 50 09 28 47	07 09 10	57 17 37	08	26 47	08	13 35 58	08	45	90	30 56 21	80	39 06 34	10	49 18 47	10	30
	11	13 15 16	49 05 21	14 15 16	18	14 15 16	12 31 49	15	05 25 45 05 24	14 16 17	39 00 20	14 16 17	53 15 37	15 16 17	97 31 55	15 16 18	48 13	15 17 18	38 06 33	15 17 18	56 25 54	16	15 45 16	18	34
	16 17 18	20 21 22	28	20 21 23	46	20 22 23	06 26	21 22 23	44 05 26 47 09	21 22 24	47	21 23 24	10	22 23 24	08 34 59	22 23 25	32 59 26	22 24 25	56 25 54	23 24 26	23 53 25	23 25 26	50 23 57	24 25 27	5:
	21 22 23	26 27 29	39 58	27 28 29	23	27 28 29	49	27	31 53 16 40 20	28 29 31	45	28 30	16	30 32	48	3 F 3 Z	53 22 51	30 31 33	58 30	31 32 34	37 12	31 33 34	42 18 56	32 34 35	2 0 4

A TABLE of Amplitudes, from the Latitude 49 deg. oo min. to the Latitude 60 deg. either North or South.

		1				7		ne	D	eg	ree	s c	r	La	titt	ade	-	1		-1	·	-1		
Degrees of Declination.	4	9	5	0	5	1	5	2	5	3	5	+	5	5	5	6	5	7	5	8	5	9	6	0
	D	М	D	М	D	М	D	М	D	м	D	М	D	М	D	м	D	M	D	М	D	м	D	М
1 2 3	01	31 03 34	01	33 06 40	01	35 10 46	01	37 15 52	01	39 20 59	01	42 24 06	03	45 29	01	47 34 22	01	50 40 31	01	53 40 40	00 01 03 05 07	56	04	00
6 7 8	10	10 42 14	10	55 29	11	33 09 45	11	24	11	40	11	15 57 41	10	30 15 02	12	47 35 24	11	04 56 48	13	18	09 11 13 15 17	42 41 41	12 14 16	0
11 12 13	18	28	18	52	19	39 18 57	19	44 26	18 20 21	29 12 57	18 20 22	57 43 30	19 21 23	15	19 21 23	56 49 43	20 22 24	29 25 23	21 23 25	04	19 21 23 25 28	43 47 54	22 24 26	3 4
16	24 26 28	28	25 27 28	03	25 27 29	59 41 24	28	21	27 29 30	04	27 29 31	58	30 32	43 39 35	31	31	30 32 34	24 27 34	33	28	30 32 34 36 39	32	33 35 38	4 0
21	33 34 36	48	33 35 37	37	34 36 38	30	35 37 39	27	36 38 40	29	37 39 41	32 26 40	38 40 42	39 47 56	39 42 44	04	41 43 45	27	44	34 59	41 14 46 49 50	40	45 48 51	4 3 2

A TABLE of Amplitudes from the Latitude 61 Deg. 00 Min. to the Latitude 66 Deg. either North or South.

Degrees of Declination.		The Degrees of Latitude.											The Use of the TABLES of Amplitudes.
	61		62		63		64		65		66		The Amplitude of the Sur or any Star, is fo many Degrees
	D	M	D	М	D	M	D	М	D	M	D	M	Distance as they Rise or set. from the East or West Points
·	ပ၁	00	00	00	00	00	00	00	00	00	co	00	of the Horizon, either North-
1	02		02	07	02	12	02	17	02		OZ	27	erly or Southerly.
2	04		04	15			04	33	04	44	04	55	Note, When the Sun or Stars
3	05		06	24	05		06		27		07	23	nam North Declination, the
4	08	17	08	32	08	50	09	09	39	30	09	52	the Amplitude found by these
-	10		10					-0					Tables must be reckoned from
6			12	41 52	11	61	13	. [1]	11		12		the East toward the North a
7	14		15		15		16		14	-	14		their Rifling; or from the Wel
8	16		17	14	17		18	1 - 1	19	*	20	00	toward the North at thei Setting.
9	18		19		20		20	54			22	37	
	-		-		-		-		-		_		clination, then the Amplitude
40.00	20		21		22	27	23		24	13	25	14	must be reckoned from the East
	23		23		24	-	25		26		27	58	toward the South at their Ri
	25		26	17			28		29		30	44	fing, or from the West towar
	27		28		29		30	52	-	09			the South at their Setting.
4	29	50	31	01	32	12	33	30	34	55	36		
15	32	16	33	27	34	45	36		37	46	20	••	To find the true Amplitud
	34		35		37		38	11111	40	42	m. m.	40	
17	137	05	38		40		41		43	46		58	
18	139	36	41	10	42		44		16	59		26	at the Top of the Table, and
19	42	11	43	54	45	49	47		10	23		11	the Declination in the first
	1				.0	-		-	-		-		Column to the Left-hand
	14	100	46		48		51		54	02		14	and in the Common Angle
	50		52		52	26	54	50	62		61	47	of Meeting, you will find the
	53		56	20	59		53		67		73	52	Amplitude required, in De
3,29			58	04			55	1 100	70		78	25	Amplitude required, in De grees and Minutes.
	1		1		2	-				33	1	_,	

Case ist. When the Latitude and Declination are both given in even Degrees, as for Example. Suppose I would know the Sun's true Amplitude at his Rising, in the Latitude of 40 00, his Declination being 17 00 N.

Under Latitude 40, and right against Declination 17 I find 22 26, which is the Sun's true Amplitude, to be counted from the East towards the North (because it is at his Rising, and the Declination

is North) that is E. 22 26 N.

Case 2d. When the Latitude is given in even Degrees, and the Declination in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his Setting, in the Latitude of 57 00, his Declination being 11 33 S.

Find his Amplitude as before, for the Latitude 57, and for the Declination { 11 deg. } which will be { 20 29 } then

fubtract the Lesser from the Greater, the Dist. is 1 56 or 116 m. to which put two Cyphers, and it makes 11600, which Number must be divided by the Number standing against the odd Minutes of Declination (in the following Table) which in this Case is 181, and the Quotient gives the Proportional Parts in Minutes, which Parts are always to be added to the Lesser of the two Amplitudes that you took the Difference of, and the Sum gives the true Amplitude as follows.

181)11600(64 Proportional Parts in Minutes, 740 makes 1 Degree 4 Minutes.

Case 3d. When the Declination is given in even Degrees, and the Latitude in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his Rising, in the Latitude 51 14, his Declination being 14 00 S.

Find his Amplitude as before, to 14 Degrees Declination, and for the Latitude \{ \frac{51}{52} \deg. \} which will be \{ \frac{22}{23} \frac{37}{08} \} and fubtract

the Lesser from the Greater, the Difference is 0 31 Minutes.

To

To the Difference of Amplitudes found on the foregoing Side, which is 31, put two Cyphers and makes it 3100, which must be divided by the Number standing against the odd Minutes of Latitude (in the following Table) which in this Case is 428, and the Quotient gives the Proportional Parts in Minutes, to be added to the Lesser of the two Amplitudes, as in Case the 2d.

428)3100(7 Proportional Parts in Minutes.

Lesser of the Amplitudes —	22	37
Proportional Parts to be added -	00	07
True Amplitude—	E.22	44 S.

Case 4th. When the Latitude and Declination are both given in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his setting, in the Latitude 49 18, his Declination being 19 41 N.

First find his Amplitude for Latitude 49 Degrees, and Declina-

tion 19 41 (as in Case the 2d) which will be 30 53.

In the same Manner find his Amplitude for Latitude 50 Degrees, and Declination 19 41, which will be 31 35.

Then from the Greater Amplitude — 31 35
Subtract the Lesser — 30 53
Remains the Difference — 00 42 Minutes.

Put two Cyphers to this Difference it makes 4200, which must be divided by the Numbers standing right against the odd Minutes of the given Latitude, (in the following Table) which in this Case is 333, the Quotient gives the Proportional Parts in Minutes, to be added to the Lesser of the two Amplitudes, &c.

The Leffer Amplitude— Proportional Parts to be added True Amp. for Lat. 49 18, and Decl. 19 41 NW. 31 05 N. R 2

A TABLE of Numbers for finding the Proportional Parts, to the odd Minutes of Latitude or Declination, in finding the Sun's true Amplitude.

. Odd .	Num- bers.	Odd Minutes	Num- bers.	Odd Minutes	Num bers.	Odd 'Minutes	Num- bers.
1	6000	16	375	31	193	46	130
2	3000	17	353	32	187	47	127
3	2000	18	*333	33	181	48	125
3	1500	1.19	316	34	176	49	122
5	1200	20	300	35	171	50	120
6	1000	21	285	36	166	51	118
7 8	857	22	273	37	162	52	115
8	750	23	261	38	158	53	113
9	666	24	250	39	154	54	111
10	600	25	240	40	150	55	109
11	545	26	230	41	146	56	107
12	500	27	222	42	143	57	105
13	461	28	214	43	139	58	103
14	428	29	207	44	136	59	101
15	400	1 30	200	45	133		

The Use of this Table is to find a Number to divide the Disserence of Amplitudes by, in order to find the Proportional Parts, when the Amplitudes is required for any Latitude or Declination that is given in Degrees and Minutes, (as in the foregoing Cases) to find which Number, look in some of the Columns under the Title of odd Minutes, for your given Minutes of Latitude or Declination, as suppose for 37 Minutes, and right against that you will find 162, which is the Number required.

es or doubt him

To find the Variation of the Compass by an Amplitude.

To do this, you must have given both the true and magnetical Amplitudes.

The magnetical Amplitude is to be found by the Tables us before taught. The magnetical Amplitude is to be found by the Compass, at the Time of the Sun's Rising or Setting, and is so many Degrees and Minutes as you find it to rise from the East, or to set from the West, either to the Northward or to the Southward: As for Examp. Suppose being at Sea, I find by setting the Sun with my Compass, that he rises 10 deg. 15 min. to the Northward of the East, then the magnetical Amplitude is E. 10 15 N. Or Suppose I find by the Compass, that he sets 14 deg. 12 min. to the Southward of the West, then the magnetical Amplitude is W. 14 12 S.

Then if your true Amplitude, and magnetical Amplitude are both to the Northward, or both to the Southward, subtract the Lesser

from the Greater, the Remainder is the Variation.

But if one be to the Northward, and the other to the Southward, add them together, and the Sum will be the Variation.

And thus having found how much the Variation is, it is remains in the next Place to find which way it is, that is, whether it be Easterly or Westerly.

Rule, If the Amplitude be taken at Sun-rising, and the magnetical Amplitude be farther from the North than the true Amplitude is, then the Variation is Westerly, but if it be nearer to the North, it is

Easterly.

If it be taken at Sun-setting, if the magnetical Amplitude be farther from the North than the true Amplitude is, then the Variation is Easterly, but if it be nearer to the North it is Westerly, as may be seen by the two foregoing Examples.

By By keeping a Journal is meant, keeping such an Account of the Ship's Way, that at any Time you may be able to know what La-

titude and Longitude the Ship is in.

When a Ship is bound from any one Place to another that lies so far from it, that she is obliged to go out of sight of the Land for any considerable Time, as suppose from England to Barbadoes, then at the Time she leaves the Land, she is said to take her Departure, and that part of the Land, she then leaves, as suppose the Start, the Lizard, the Land's-end, &c. is said to be the Place they take their Departure from. And at the Time of taking such Departure, the Captain or Mate generally takes the Bearing and Distance of that Land (according to his Judgment) and sets it down on the Log-Board, or in the Log-Book against the Time it was taken, thus,

Lizard, N. by W. Distance 5 Leagues. Or, Start, N. N. E. Distance 6 Leagues, &c.

And in the same manner for any other Place, Bearing and Distance,

as you will fee in the first Day's Log, of the following Journal.

The Log-book being mark'd as follows, with Columns for Course, Distance, Northing or Southing, Easting or Westing, Latitude by Dead Reckoning, Latitude by Observation, Meridian Distance, Longitude made, and Longitude in you are to take Notice.

Longitude made, and Longitude in, you are to take Notice.

That in the Column for Course, you are always to set do

That in the Column for Course, you are always to set down the Course you have made by your Reckoning for that 24 Hours (that is from the Noon of the Day before, to the Noon of the Day you Work on) the Sea Account being always kept from Noon to Noon.

In the Column for Distance, you are to set down the Distance

made by your Reckoning for that 24 Hours.

In the Column of Northing or Southing, you are to set down the Difference of Latitude made that 24 Hours, marking the Column with N. if the Difference of Latitude be Northerly, or with S. if it be Southerly.

In the Column of Easting or Westing, you are to set down the Departure made that 24 Hours, marking the Column with E. if the

Departure be Easterly, or with W. if it be Westerly.

In the Column mark'd Lat. by D. R. you are to fet down the Latitude you reckon yourself in on that Day.

In

In the Column mark'd Lat. by Obs. you are to set down the Latitude you find yourself to be in by Observation, if you have one, if not, then let it stand open.

In the Column for Mer. Dift. you are to fet down (in Degrees and Minutes) how much Departure you have made in all, from the

Place you took your Departure from.

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In

In the Column of Long. made, you are to fet down (in Degrees and Minutes) how much Difference of Longitude you have made in all from the Place you took your Departure from.

In the Column of Long. in, you are to fet down what Longitude

you find yourfelf to be in on that Day by your Reckoning.

Note, The Account of Longitude made, being what is always kept in His Majesty's Navy. And the Account of Longitude in, being most generally kept on Board the Merchant Ships: I shall in this Treatise shew how to keep them both, and shall leave it to the Practitioner's Choice which he will make use of, they both being equally true, and there being no Occasion to keep more than one of them.

And not having (I think) given a fufficient Account of Things that are to be fet down in the feveral Columns, I shall lay down these few necessary Rules following, and then proceed to shew how they are all to be found, or the Method of Working a Days Work at Sea.

Rule 1st, Variation, if there be any, (as most commonly there is,) must be allowed upon all Courses steered, and upon all Bearings, &c. that are taken by the Compass, that is, if it be Easterly Variation it must be allowed to the Right-hand: But if Westerly Variation, then to the Lest hand of the Course or Bearing: Supposing your self placed in the Center of the Compass, and looking directly forward to the Point you are to allow the Variation from.

Example. Suppose I steer SW. and there is one Point Westerly Variation, then my true Course will be SW. by S. or suppose I set a Point of Land, and find it to bear by my Compass ESE. and I know there is half a Point Easterly Variation, then the true Bearing is SE. by E. ½ E.

Rule 2d, Lee-way (which I shall not here describe, because sufficiently known to every Seaman) must be allowed to be the Righthand of the Course steer'd, when the Larboard Tacks are Aboard, and to the Lest-hand when the Starboard Tacks are Aboard.

Ex-

Example. Suppose I steer N. E. by E. with my Larboard Tacks Aboard, and make one Point Lee-way, then my Course made good is E.N.E.

Rule 3d. Lee-way and Variation, when they are both to be allow'd one way, that is, both to the Right-hand, or both to the Left, add them together, and allow their Sum the same way they were to be allow'd.

But if they are to be allow'd one to the Right-hand, and the other to the Left, subtract the Lesser from the Greater, and allow the Remainder the same way as the Greater of them was to be allowed.

Example. Suppose I steer NNW. with my Starboard Tacks Aboard, and make one Point Lee-way, there being at the same Time half a Point Westerly Variation, I would know my true Course?

Lee-way to the Left-Hand — 1 Point. Variation to the Left-Hand — 0 ½ Point.

Their Sum to be allowed to the Left-Hand 1 ½ Point makes

the true Course NW. by N. ½ W.

Example 2d. Suppose I steer SW. by W. with my Larboard Tacks Aboard, and make 2½ Points Lee-way, and I have 1½ Points Westerly Variation, what is my true Course?

Lee-way to the Right-Hand — 2 ½ Points

Variation to the Left-Hand — 1 ½

The Remainder to be allowed to the Right-hand 1 4 Points, makes the true Course WSW. 4 W.

Rule 4th. When a Ship is lying too under a Main-fail, Mizen, &c. then observe how she comes up and falls off, and take the middle between the two Points, and from that allow the Lee-way and

Variation, as in Rule 3d.

Example. Suppose a Ship lying too under a Main-sail, with the Starboard Tack Aboard, comes up E. by S. and salls off to NE. by E. there being a Point Westerly Variation, and she making 5 Points Lee-way, what Course does she make good?

The middle between E. by S. and NE. by E. is E. by N. from which allowing 6 Points to the Left-Hand, (by Rule 3d.) the true

Course will be N. by E.

Rule 5th. Currents, the way they set you, and the Distance you suppose you are driven by them, is to be set in the Traverse Table for the Day, as any other Course and Distance.

Example, Suppose I try the Current and find it to set W by N. per Compass 1 Mile per Hour, the Variation being one Point Easterly, then if I sail in that Current 24 Hours, I set down in the Traverse Table, as a Course WNW. distant 24 Miles.

Rule 6th, Heave of the Sea, is to be accounted for in the same manner as Currents: As suppose, there is a great Sea heaving toward the SW. by my Compass, there being $\frac{1}{2}$ Point Westerly Variation, I then set down in my Traverse-Table SW. by S. $\frac{1}{2}$ W. with so much Distance as I judge the Sea has heav'd the Ship.

Rule 7th, At leaving the Land, the opposite Point to the Bearing (with the Variation allow'd upon it) and the Distance you judge yourself from it, must be set down in the Traverse-Table, as a Course and Distance.

Example, Suppose having 1 4 Westerly Variation, the Start bears by my Compass NNE. distant 4 Leagues: The opposite Point to NNE. is SSW. which with the Variation makes S. 3 W. for the Course to be set in the Trhverse-Table, distant 12 Miles.

Rule 8th, When you make the Land, the Bearing itself (with the Variation allow'd upon it) and the Distance you judge yourself from it are to be set in the Traverse-Table, as a Course and Distance: This needs no Example.

Note, If you keep only the Account of Longitude made, and would at any Time know what Longitude you are in, look out the Longitude of the Place you took your Departure from, and with that Longitude, and the Longitude made, taken as Difference of Longitude, find the Longitude in, by the Rules in Page 107 and 108. And the Longitude fo found must be counted from the same Meridian that the Tables you look'd out the Longitude of the Place departed from, counts it.

RULE S to Correct the Dead-Reckoning by an Observation.

WHEN you have made all the proper Allowances you can, fuch as for Variation, Lee-way, Currents, &c. and still find that your Latitude by Dead-Reckoning will not agree with the Latitude by Observation, within five Minutes, then you must Correct as follows.

CASE the First.

If your Course found by Dead-Reckoning be due North, or due South.

Rule, First find the Difference of Latitude (in Miles) between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude, then will your true Course be the same as the Course by Dead-Reckoning. Your true Distance the same as the true Difference of Latitude. Your Departure oo, and your Meridian Distance, Longitude made, (or Longitude in) will be the same as they were on the Day you had the last Observation.

CASE the Second.

If the Course found by Dead-Reckoning be less than 3 Points, or 33 Degrees.

Rule, First find the Difference of Latitude (in Miles) between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude. Then make your true Course the same as the Course sound by Dead-Reckoning, since the last Observation, and with that Course, and the true Difference of Latitude, find the true Distance and Departure (as in Plain Sailing, Case the 2d,) then to find the Meridian Distance, the Longitude made, and the Longitude in, take the following Rule.

N. B. The Difference of Longitude is to be found by the true Course, and the Meridional Difference of Latitude between the two Observations (as usual) and the Meridian Distance, Longitude made (or Longitude in) are to be found by adding, or subtracting the true Departure and Difference of Longitude to, or from the Meridian Distance, Longitude made (or Longitude in) on the Day you had the last Observation, which is the Day you always Correct from. Case

CASE the Third.

If the Course found by Dead Reckoning, be more than 3 Points, or 33 Degrees, and less than 6 Points, or 67 Degrees.

Rule, First find the Disference of Latitude in Miles between the last Observation, and the Observation on the Day you Correct, which will be the true Disference of Latitude: Then with the Couse found by Dead-Reckoning, since the last Observation, and the true Disference of Latitude, find a new Departure, (by the Second Case of Plain Sailing) add this new Departure to the Departure found by Dead-Reckoning since the last Observation, and take half their Sum, for your true Departure: Then you have given the true Disference of Latitude and Departure to find your true Course and Distance, (by Plain Sailing, Case 6th) read here N. B. In Case the 2d.

CASE the Fourth.

If the Course found by Dead-Reckoning be more than 6 Points, or 67 Degrees.

Rule, First find the Difference of Latitude in Miles, between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude, and make your true Departure the same, as the Departure found by Dead-Reckoning since the last Observation: Then you have given the true Difference of Latitude and Departure, to find the true Course and Distance (by Plain

Sailing, Case 2d.) read here the N. B. in Case the 2d.

Note, As the Knowledge of which Case you are to Correct by, depends upon knowing your Course by Dead-Reckoning, and as when you Correct only for one Day, that Course is always found by the difference of Latitude and Departure in your Traverse-Table for that Day; therefore if you are to Correct for a longer Time than one Day, you must take the Northing, Southing, Easting and Westing that you have made for every Day since the last Observation, (or if it be your first Observation, then for every Day from your leaving the Land) minding not to leave out the Difference of Latitude and Departure for the Day you are Correcting on, and bring them into a Traverse-Table; by which you will find the whole Difference of Latitude and Departure, made by Dead-Reckoning since the last Observation, and with that same Difference of Latitude and Departure

132 Rules to Correct the Dead-Reckoning, &c.

find the Course made by Dead-Reckoning, then observe which of the foregoing Cases that Course comes under, and Correct by the Rules for that Case, finding every Thing except the Distance.

And when you have so corrected, you are to set down in your Book only the Latitude by Dead-Reckoning, the Latitude by Observation, the Meridian Distance and the Long. made (or Longitude in) and rub out the Course, Difference of Latitude and Departure.

Then you have given the Latitude by Observation on the Day you Correct, and the Latitude by Dead-Reckoning on the Day before it, to find the Disserence of Latitude for the last 24 Hours, (by the Rules for Latitude, Page 105.) Also the Meridian Distance on the Day you Correct, and the Meridian Distance on the Day before it, to find your Departure, (by subtracting the Lesser from the Greater, if they are both East, or both West; or by adding them together, if one be East and the other West.) And with that Difference of Latitude and Departure find your Course and Dissance, (by the 6th Case of Plain Sailing) which Course, Dissance, Difference of Latitude and Departure are to be set down instead of them you rubb'd out.

Rules to find the Meridian Distance.

Case 1st, If the Meridian Distance on the Day you Work from be East, and if you have sail'd to the Eastward; or if it be West, and you have sail'd to the Westward, then add the Departure to the Meridian Distance, and the Sum will be the Meridian Distance you have made, of the same Name with that you work'd from.

Example Meridian Distance———— 4 18 W.

Departure Westerly 97 Miles, or—— 1 37

Meridian Distance made in all ——— 5 55 W.

Case 2d, It your Meridian Distance be East, and the Departure be Westerly; or if the Meridian Distance be West, and Departure Easterly, then subtract the Lesser from the Greater, the Remainder will be the Meridian Distance you have made, of the same Name with the Greater of the two.

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JOURNAL

OF

A VOYAGE from ENGLAND

TOWARDS

MADERA

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134 A Journal from England towards Madera.

es and fair	May the 1st, 176	way	VV IIIUS	Courfes	F	нк	K	Н
p. m.) the	Moderate Gales ar Weather, at 6 (p. m	Leag.	dist. 6 1	by E.	N	Start	The	4 6
	Start bore as per Log		NE.	SW.bW.			4	8
	which I take my Depa					I	4	10
	it being in the La						5	1.2
	50 07 N. and Long 3 47 W. from Long	137.14					5	2
London.	3 4/ W. Holli Lona			S.W.		1.	5	4
						1	5	6
nt W.erly	Variation 1 Point V					1	- 5	.8
						1	5	10
							6	12
	Variation 1 7 Point V	at. byO	by D.R. L. 34N.			1	5 6	10

The Manner of working this Day's Work.

The opposite Point to the Bearing of the Land is S. by W. which with the Variation allow'd upon it (as before taught) makes S. \(\frac{1}{4}\) E. and Distance from the Land 6 Leagues, or 18 Miles, which are to be set down for the first Course and Distance in the following Traverse Table.

Then the first Course steer'd being SW. by W. the Variation allow'd upon it will make it SW. by S. \(\frac{1}{2} \) W and the Sum of all the Distances from 8 a Clock where that Course begins, to 2 a Clock where it ends, being 18 Miles and a half, I double that Sum, because the Book is mark'd only for every Two Hours) and it makes 37 Miles for the Distance belonging to that Course. But if the Book had been mark'd for every Hour, as it is in the Navy, and Aboard the East-India Ships, then I must have taken the Sum without doubling it for the Distance, and in the same Manner I reckon the other Course and Distance; all which will be as in the following Traverse-Table.

And then every Thing being found as on the other Side, I set them down in their proper Columns as above.

Course.

Courles.	Dift.	N.	S.	E.	W.
S. ‡ E.	18		180	0.9	
SW. by S. 3 W.	37		27.4		24.8
SSW. 3 W	56 .		48.0		28.8
Difference	of Latiti	93.4	0.9	53.6	
					0.9
					52.7

Dep. W.

The several Courses and Distances in this Table, being look'd out and cast up as in the Rules for Traverse Sailing, (Page 52) I find my Difference of Latitude to be 93 Miles and 4 Tenths, and my Departure 52 Miles and 7 Tenths: Then I mark down (upon my Slate, or the Paper that I work upon) every Thing that is to be found, and as I find what they come to, I fet against them as follows.

Distance - 108 Miles Diff. of Lat. - 93 S. 53 W. By Departure Latitude by D.R. 48 34 N. Latitude Observation Meridian Distance 00 53 W. Longitude made oi 22 W 05 09 W. Longitude in

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Course --- S. 30 00 W. Because the Diff. Lat. is S. and the Depar. W. No:e, When the Tenths in any Side are more than 5, or half a Mile, you must call that Side 1 Mile more than you found it to be, but when they are less than 5, then you need take no Notice of them. As in this Case the Diff of lat. being 93.4 I reject the 4 Tenths, and call it only 93 Miles, and the Dep. being 52.7, instead of the 7 Tenths I put 1 Mile to it, and call it 53 Miles.

But when you take the Difference of Latitude and Departure to find the Courfe by, then take them in Miles and Tenths,

Then in the first Place, with my Difference of Latitude 93.4, and my Departure 52.7 as Taught in Plain Sailing, Case the 6th) I find my Course to be 30 Degrees, and my Distance 108 Miles, which I set down against Course and Distance as above.

Second, For the Latitude by D. R. Take the Latitude fail'd from And the Diff. Lat. 93 Miles, or 1 33 Sub: (asperRules) gives Lat. D.R. 48 34 N. I Third, For the Meridian Distance,

Note, The Meridian Distance on the first Day's Work, is always the same as that Day's Dep. which here is o 53 W.

Fourth, For the Difference of Longitude. The Meridional Parts of 3485 The Latitude fail'd from Of the Lat. by D. R. 3343

Then I look for my Courfe 30 Degrees, in the Tables of Diff. of Lat. and Dep. and for the Merid. Diff. of Lat. 142, in fome of the Diff, of Lat. Columns belonging to that Course, the Dep. 82 which answers to that Diff. Lat. is my Diff Long.

Fifth, For the Longitude made.

Meridional Difference of Lat.

The Long. made on the first Day's Take the Longitude fail'd from Work, is always the fame as that Day's And the Diff. Long 82Miles, or Diff, of Long, which here is - 1 23 W. Sub (as perRules) gives Lon, in

Sixth, For the Longitude in. 3 47 W

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Н	K	H K	F	Courfes	Winds	Lee- way	Transactions, Friday May the 2d, 1762.
2	6			SW.bW.	N.		
6	5	1			NW.		Moderate Gales and fair Weather, at 8 (a. m.) faw
8	5			s.w.			a Ship to the Northward.
10	4	1		3. W.			
2	4	I					
6	4	1					
8	5			SWbS.	WNW		
10	4	1					Variation 14 Point W.erly.

The Variation being allow'd, and the Distances summ'd up as before, the Traverse-Table will be as follows.

Course	Diff.	N.	S.	E.	W.
SWb SI W	43		31.9	1	28.9
SSW 3 W	13.		38.6	- Lav	23.1
S by W W	27		25-4		0.1

First, With my Difference of Latitude 95.9 and Departure 61.1 (by Plain Sailing Case 6,) I find my Course to be 33 deg. and my Distance 114 Miles.

Second, For my Latitude by D.R.

Take the Latitude in yesterday 48 34 N.

And my Diff. Lat. 96 Miles, or 1 36

Gives the Latitude by D.R.—46 58 N.

Third, For the Meridian Distance,
Take the Mer. Dist. yesterday o 53 W.
And the Departure to-day 1 of

Oives the Meridian Distance 1 54 W.

	Courfe S. 33 00 W
	Diftance 114 Miles
	Diff. of Lat 96 S.
By	Departure 61 W.
	Latitude by D.R. 46 58 N
D.R.	Latitude by Observation
	Meridian Distance 1 54 W
	Longitude made 2 55 W
	Longitude in 6 42 W

Fourth, For the Diff. of Longitude.

Take the Mer. Parts of yest. Lat. — 334

And of the Latitude to-day — 320

Gives the Mer. Diff. of Latitude — 14

with which and the Course (as in the fir Day's Work) I find my Diff. of Longitus
to be 93 Miles.

Fifth, For the Longitude made.
Take the Long. made yesterday 1 22 W
And the Diff. of Long. to-day 1 33

Gives the Long. made to-day 2 5: Sixtb, For the Longitude in, Take the Long. in yesterday 5 of And the Diff. of Long. to-day 1 3:

Gives the Longitude in ____ 6 4:

,			-1
			1
fa	ii	•	-
			-
			fair faw

a.

W.erly.

Lon, in 6 42 W

up as

33 00 W. 114 Miles. 96 S. 61 W. 46 58 N. ation

- 1 54 W. - 2 55 W. 6 42 W.

ngitude. it. — 3343 3200

de - 143 in the first Longitude

nade. 1 22 W.

5 09 W.

Н	K	H K	F.	Courfes	Winds	Lee- way	Transactions, Saturday, May the 3d, 1762.
2 4 6	4 4 4			SW	WNW		Moderate Gales and Cloudy.
8	4	1		SWbS	W by N	$\frac{1}{2}$	
10	4	I					
12	4	1				7 50	
2	4	I			ef both To	p-fails	
4	4			SSW	W	1	4 3 2
6	4						
8	4						
10	4						Variation 1 Point Werly
12	1 4	1					- 1 61
Co	urfe	Dift.	S.	W Lat.	byD R.L	at. byO	b. Mer. Dift. Lon. made Lon. i
5 14	ooW	97	95	24 45	23 N		2 18W 3 29W 7 16

The Lee-way and Variation being allow'd, as before taught, the Traverse-Table will be as follows.

Courfes	Dift.	N.	S.	E.	W.
SW. by S.	24		20.0		1.33
S by W & W	36		34.5		10.4
South	40		40.0		
			94.5		23.7

First, The Course and Distance found (by Plain-Sailing Case 6.) as before will The Mer. Parts of yesterdays Lat. - 3200 be as in the other Column.

Second, For my Latitude by D.R. Take the Latitude in yesterday 46 58 N. find the Difference of Lon. to be 34 Miles. And the Diff. of Latitude 95 1 35 Miles, or -Gives the Latitude by D.R.

Third, For the Meridian Distance, Take the Mer. Dift. yesterday 1 54 W. And the Departure to-day -0 24 Gives the Meridian Distance -- 2 18 W. Gives the Longitude in -

	Courfe S.	14	oo W.
	Distance -		Miles:
	Diff. of Lat.—		S.
By		24	
	Latitude by D.R.	45	23 N.
D.R.		n	
	Meridian Distance		18 W.
	Longitude made		
	Longitude in—	7	16 W.

Fourth, For the Diff. of Longitude. Of to days Loticude -The Meridian Difference of Latitude 137 with which and the Course, (as before) I Fifth, for the Longitude made. Take the Long. made yesterday 2 55 W. And the Diff. of Long. to-day o 34 W. Gives the Longitude made - 3 20 W. Sixth, For the Longitude in, Take the Long. in yesterday 6 42 W And the Difference of Longitude o 34

Th

Н	K	HK	F.	Courses	Winds	Lee- way	Transaction, Monday May the 4th, 1762.
2 4 6	4 4 4	1		S	WSW	1	Moderate Gales and Hazy the first Part, the latter fresh
8 10 12	4 4 4			In 2d Ree S S E.	of both To	p-fails	Gales with Rain.
4 6	4 4 4			Handed t	he Fore T	op-fail	
8 10 12	4 4 3	1		S by E	SW byW Tack'd	2	Variation 1 Point W.erly.
Cou		Dift 93		E Lat. b		it. byO	b. Mer. Dift. Lon. made Lon. in

The Ship having her Starboard Tacks aboard, when the Leeway and Variation are allow'd (as before taught) the Traverse Table will stand as follows.

Courses	Dift	N.	S.	E.	W.		Course — S. 39 co E. Distance — 93 Miles
SSE	33		30.5	12.6			Diff. of Lat. 72 S.
SE ½ E	40		25.4	30.9		Ву	Departure—60 E. Latitude by D.R. 44 11 N.
SE	23		16.3 16.3		D.R.	Latitude Observation	
			72.2	59.8			Meridian Distance 1 18 W. Longitude made 2 7 W.
1							Longitude in 5 54 W.

Having been very particular in explaining the Manner of working a Day's Work (in the three foregoing Days) and as all Days Works, where there is no Correction wanting, are to be work'd from the Difference of Latitude and Departure found by the Traverse Table (as before) I have here only fet down the Traverse Table, and what all the other Things come to, and have left the finding of them to exercise the Learner.

Н	K	нк	F.	Courses	Winds	Lee- way	Transaction, Monday, May the 5th, 1762.
2 4 6	4 3 3			NWbyW	SW byW	2	Fresh Gales and Rain all these 24 Hours.
8 10 12	3 3 3	ı		Hand N N W	Main To		
4 6	3 3 3	I					
8 10 12	3 3 3			NW byN	W by S	31/2	Variation 1 Point W.erly.
Co	ourfe	Dift.	N	W Lat.	byD.R.L	at. byO	b. Mer. Dift. Lon. made Lon. in
N29	ooW	75	6	36 45	16 N		1 54W 3 00W 6 47W

The Ship having her Larboard Tacks Aboard, when the Lee-way and Variation allow'd, the Traverse-Table will stand as follows.

Courses	Dift.	N.	S.	E.	W.		Courfe—N. 29 00 W.
NW	32	22.6			22.6		Distance 75 Miles Diff. of Lat. 65 N.
NNW	33	30.5			12.6	By	Departure - 36 W.
N 1 W	12	119			1.2		Latitude by D.R. 45 16 N.
***		65.0			36.4	D.R.	Lat, by Observation Meridian Distance 1 54 W.
							Longitude made 3 00 W. Longitude in 6 47 W.

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To find the Course.

Note, In this Case the Difference of Latitude being just 65 Miles without any Tenths, after you have put two Cyphers to the Departure, you must not divide it by 65, but by 650, the Cyphers being put to supply the Place of Tenths, as directed in the Rule for Plain-Sailing, see the Work.

Diff. Lat. D. with Cyphers. (56 N. 3640 (56 N. 3900 for Courses

H

Н	K	нк	F	Courfes	Winds	Lee- way	Transactions, Tuesday, May the 5th, 1762.
- 2	3			WNW	S W	-3½	Hand Cales and Savalu
6	3		1	Handed	the For	re-fail	Hard Gales and Squaly with Rain.
8	L	ay too	, u	p NW.	off N.	5	
10	Dri	ft 11/2	M	iles per l	Hour.		
2 4			Up	NbyW of	NEbyN		
6							
8 10 12			-	NNW. o	and the second second		Variation 1 Point W.erly.
Co	urſe	Dift.	N	E Lat. 1	y D.R. L	at. byOb	Mer. Dift. Lon. made Lon. in
N 8	ook	35	34	5 45	50N.		1 49W 2 53W 6 40

Having allow'd the Lee-way, and the Variation upon the first Course, and also from the Middle between what she comes up and falls off, (as taught in the Rules for laying too,) the Traverse Table will stand as follows.

Courses	Dift.	N.	S.	E.	W.	1	Course — N. 8 Distance — 35
NW bN &W	18	13.9			11.4		Diffance35 Mi Diff. of Lat34 N.
NNE	12	11.1		4.6		Ey	Departure 5 Latitude by D.R. 45
NEbyE	9	5.0		7.5		D.R.	Latitude Observation
NE	6	4.2		4.2	1 10	Meridian Diftar	Meridian Diftance 1 Longitude made 2
		34.2		16.3	11.4	(Longitude in—— 6
				11.4			
		Depa	artur	e 4.9	E.		

н	K	нк	F.	Courses	Wind	s Lee- way	Transactions, Wednesday May the 7th, 1762.
4 6	3 3 3			N W WNW	wsv sw.		Fresh Gales the first Part, the latter Moderate, with
8 10 12	3 3 3	1			ain To		fmall Showers.
4 6	3 4 4	1		Set Fo W by S	ore To		
8 10 12	4 4 4	1		Out 2d R W.	eef both	Topfails	Variation 1 Point W.erly.
Cou	rſes	Dift.	N	W Lat.	byD.R.	Lat. byOl	Mer. Dift. Lon. made Lon. in
N ₅₄	oo W	72	42	58 46	32 N.		2 47W 4 17W 8 04W

Courfes	Dift.	N.	S.	E.	W.
N by W	12	11.8			2.3
NW by N	12	10.0			6.7
NNW	21	19.4			8.0
W	32				32.0
WbNIW	9	0.9			9.0
		42.1		A.A.	58.0

(Course — N. 54 00 W. Distance — 72 Miles
Mag.	Diff. of Lat. 42 N. Departure 58 W.
	Latitude by D.R. 46 32 N. Latitude Observation
	Meridian Distance 2 47 W.
	Longitude made 4 17 W. Longitude in 8 04 W.

Н	K	нк	F	Courfes	Winds	Lee- way	Transactions, I bursday May the 8th, 1762.
2	4	1		W byN	SWbS	1	
4	4	I		Out 1ft R	eef both T	opfails	Moderate Gales and thick Hazy Weather.
8	4	I		W.	SSW.	1/2	
10	4	1			A CONTRACTOR OF THE CONTRACTOR		
12	4	I					
2	4		14	W by S	S by W	1/2	
4 6	4						
8	4						
10	3	I		WSW	S	1/2	Variation 1 Point W.erly.
12	3				50.0		
Co	urfè	Dift.	S	W Lat. 1	y D.R. L	at byO	b. Mer. Dift. Lon made Lon. in
882	ooW	95	13	95 46	19N.	•	4 22 W 6 33W 10 20V

Courles	Dift.	N.	S.]	E.	W.	1	Course ————————————————————————————————————									
W by N	26	5.1	41 5.15		25.5		Diff. of Lat. 13 S.									
WbS ½W	27		2.6		26.9	Ey	Departure 95 W. Latitude by D.R. 46 19									
WSW ₁ W	32		9.3		30.6	D.R.	Lat tude Observation									
SW by W	13	1.3	13	13	13	13	13	13	13	13		6.1	Vi z	11.5		Meridian Distance 4 22 Longitude made 6 33
		5.1	18.0		94.5		Longitude in 10 20									
			5.1													
Difference	of Lat	itude	12.9													

н	K	нк	F	Courses	Winds	Lee- way	Transactions, Friday May the 9th, 1762.
2	2	I		WSW	S.		
	2	1					Little Wind and small
6	2	1					Showers of Rain.
8	2						
10	2						
12	2						A great Swell from the
2	1.	I					SW. for which I allow 6
4	1	1		SWbW	S by E		Miles
6	I	I					
8	1					1	
10		I			1		Variation 1 Point W.erly.
12		1	-		1	1	

Courfes	Dift.	N.	S.	E.	W.		Course—— Distance —		
SWbyW	30		16.7		24.9		Diff. of Lat.		
SW	10		7.1		7.1	By	Departure - Latitude by I		
NE by N	6	6	6	6	5.0	1	3.3		D.R. Latitude by D.R. Lat. by Observation
		5.0	23.8	3.3	32.0		Meridian Di Longitude m		
			5.0		3.3		Longitude in		
			18.8		28.7				

Note, In this Day's Work the Swell coming from the SW. heaves the Ship towards the NE. and the Variation allowed upon it makes NE. by N. for the last Course in the Traverse-Table.

H	K	H	F	Courfes	Winds	Lee- way	Transactions, Saturday, May the 10th, 1762.
2 4 6 8 10 12				Calm			Tried the Current and found it to fet W.S.W. 1 Mile per Hour, at which Rate I allow it for this 24 Hours.
2 4 6							Zenith Distance 27 52 S. Declination —— 17 41 N.
8 10	1 2 2	1		SSW	w.		Variation 1 Point Werly.

Courses	Dift	N.	S.	E.	W.
S by W	11		10.8		2.1
SW bW	24		13.3		20.0
			24.1		22.1

Course — S. 42 00 W.
Distance — 32 Miles
Diff of Latitude 24 S.
Departure — 22 W.
Latitude by D.R. 45 36 N.
Latitude Observ. 45 33 N.
Meridian Distance 5 13 W.
Longitude made 7 50 W:
Longitude in — 11 37 W.

Note, The Current fetting W.S.W. I Mile per Hour, I allow the Variation upon it, which makes it SW. by W. and fet it in the Traverse Table, with 24 Miles Distance, as above.

	J		1		•	4 12 1 4 1	
Н	K	нк	F	Courses	Winds	Lee- way	Transactions, Sunday May the 11th, 1762.
4 6	3 3 4	I		S by W	W by S		Moderate Gales and fair Weather, at 9 (a. m.) spoke
8 10 12	4 4 4						with a Ship from Barbadoes, and bound for London.
2 4 6	4 4 4		•				
8 10 12	4 4 4		•				Variation 1 Point W.erly.
Cou	ırfe	Dift	S	— Lat. b	yD.R. La	t. byOb	Mer. Dift. Lon. made Lon. in
Sou	ith	103	103	- 44 (00 N. 4	3 50N	1. 5 13W 7 50W 11 37W

1-0	Course — South Distance — 93 Miles Dist. — 93 Departure — 00 Latitude by D.R. — 44 00N. Latitude Observation 43 50N.		Courfe————————————————————————————————————	es
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In this Day's Work, there being 10 Miles Difference between the Latitude by Dead-Reckoning and Observation, I am to Correct, and therefore I do not find the Meridian Distance, &c. by (D.R.) as I did when there was no Correction; but I mark them all down again as above, and Correcting (as in Case the First, of the Rules for Correcting) because my Course by D.R. since the last Observation was due South, I set them all down, as in the above Correction.

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Н	K	нк	F.	Courfes	Winds	Lee- way	Transactions, Monday, May the 12th, 1762.
2 4 6	4 4 4	1		SW b S	WNW		Moderate Gales and fine clear Weather.
8 10 12	4 4 4	1					
2 4 6	4 4 4	1		s s w			
8 10 12	4 4 4	ı					Variation 1 Point W.erly.
Co	urfe	Dift.	s	W Lat.	byD.R.L	at. byO	b. Mer. Dift. Lon. made Lon. in
818	ooW	112	106	35 42	13 N 4	2 04	N 5 48W 8 37W 12 24V

Couries	Dift.	N.	S.	E.	W.
SSW	60		55.4		23.0
S by W	42		41.2		8.2
			96.6		31.2

Corrected.

Courfe-	S. 18 o	oW.
Course————————————————————————————————————	- 112 N	Ailes
Diff. of Lat		
Departure -		
Latitude by D.		
Lat. by Observa	ation 42 o	4 N.
Meridian Dista		
Longitude ma	de 8 3	7 W.
Longitude in-	12 2	4 W.

By D.R. fince laft Obser. Having found as far as to the Latitude by Dead-Reckoning and Observation, I see they differ 9 Miles, therefore I Correct (by Case the 2d.) because my Course found by Dead-Reckoning since the last Observation, is less than 33 Degrees, and the result is as above.

Thanks

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Н	K	нк	F.	Courses	Winds	Lce- way	Transactions, Tuesday May the 13th, 1762.
4 6	4 4 4	1		SW	Nw		Moderate and Fair.
8 10 12	4 3 4	1		swbw			
4 6	4 3 5	I T			N		
8	3	I				100	
10	3 3 3	I			NE		Variation 3 Point W.erly.
Co	urfe	Dift	s	W Lat. b	yD.R. L	at. byOl	Mer. Dift. Lon. made Lon. i
47	oo W	78	53	57 40	59 N. 4	1 11N	N. 6 45W 9 53W 13 40

Courses	Dift.	N.	S	E.	W.	
SWb S&W			26.5		19.7	
SW 4 W	58		38.9		43.0	Cor-
			65.4		62.7	rected

	Course S. 47 00W.
١	Distance — 78 Miles
	Diff. of Lat 53 S.
	Departure cz W
, :	Latitude by D.R.— 40 59 N.
	Latitude Objervation 41 11 N.
	Meridian Distance 6 45 W.
	Longitude made — 9 53 W.
-	Longitude in 13 40 W.

D.K.	Course S. Distance Dist. of Lat	- 91	Miles
lince	Departure	- 63	W.

E

New Departure ————————————————————————————————————	51 63
Their Sum-	114
I Sum, or True Dep.	57 Miles

In this Case, the Course by D.R. since last Observation being more than 33, and less than 67 Degrees, I corrected by Case the 3d.

U 2

Н	K	нк	F.	Courfes	Winds	Lee- way	Transactions, Wednesday, May the 14th, 1762.
2	4		Г	W	SE		C: 1 1 C C D 1
4	4						Cloudy the first Part, the latter Moderate and Fair.
	4						latter Moderate and Fair.
8	4				-		
10	4				E		
12	4						
2	4						
4	4					1	
6	4		_				
8	3	I	12				
10	3	I					Variation 1/2 Point W.erly.
12	3	1 1			NNE		
Co	urfe	Dift	-	W Lat.	byD R. L	at. byO	b. Mer. Dift. Lon. made Lon. in
W	est	93	=	93 41	02 N 4	1 111	N 8 18W 11 56W 15 43W

Courfes	Dift.	N.	S.	E.	W.
WbS1W	93		9.1		92.6
	-		ff L	at.	Dep.

Corrected by Case the 4th, the Course by D. R. being more than 6 Points.

D.R.	Course — W. by S. W. Distance — 93 Miles Difference of Lat. — 9 S. Departure — 93 W. Latitude by D.R. — 41 02 N. Latitude Obser. — 41 11 N.	Cor- rected.	Distance — 93 Miles Dist. of Lat. — 93 W. Latitude by D.R. 41 02 N. Lat. by Observation 41 11 N. Meridian Distance — 8 18W. Longitude made — 11 56W. Longitude in — 15 43W.
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Note, When the Course is due East or due West, as in this Case, then the Difference of Longitude cannot be found by the Course, and Meridional Difference of Latitude as before, but must be found as follows; look in the Tables of Difference of Latitude and Departure, for the nearest Degree to your Latitude, which here is 41, and in some of the Difference of Latitude Columns belonging to that Degree find your Departure, which in this Case is 93, the Distance answering to that which is 123, gives your Difference of Longitude.

Н	K	нк	FC	ourles	Winds	Lee- way	Transactions, Thursday May the 15th, 1762.
2	4	I	S	by W	N.		
6	3 3	1					Little Wind and Hazy all these 24 Hours.
8 10 12	3 3 3		S	s w	NW		
2 4 6	3 3 3		St	w ₁ w	WNW		
8	3						Variation ½ Point W.erly.
12	3					1	
Co	urle	Dift	3 4	Lat. 1	by D.R. L	at byO	b. Mer. Dist. Lon made Lon. in
Sii	00 W	76	7+1	1 39	57N.		8 32 W 12 15 W 16 02 W

Courles.	Dift.	N.	1 5.	E.	W.		Course -
S 1/2 W	28		27.9		27		Diff. of Lat
SbW ¹ / ₂ W	24		23.0		17.0	Ву	Departure - Latitude b
S by W	24		23.5		4.7	D.R.	Latitude O
			74.4		14.4		Meridian I Longitude r
the state of the state of the							

Course — S. 11,00 W.
Distance — 76 Miles
Dist. of Lat. — 74 S.
Departure — 14 W.
Latitude by D.R. 39 57 N
Latitude Observation
Meridian Distance 8 32 W.
Longitude made — 12 15 W.
Longitude in — 16 02 W.

Note, Having in the foregoing Day's Work given an Example to every Case of correcting, (for a single Day) I shall now set down two or three Days Work by D.R. and then shew how to correct them all together by an Observation, that is, how to correct for a longer Time than one Day.

н	K	нк	F	Courfes	Winds	Lee-	Transactions, Friday, May the 16th, 1762.
2	3	1		SSW	W byN		
4	3	I					Little Winds and Cloudy.
6	4						
8	4		*****				
10	4			S by W	W		
12	_3	1_1					
2	3	1					
6	-3	1			*** 0 337		
	_ 3			S	wsw		
8	3				777		W I D. W. I
10	3			S bW ½ W	W		Variation 4 Point W.erly.
12	3	1 1					
Cou	irfe	Dift.	S.	W Lat. b	y D.R. L	at. byOb	Mer. Dift. Lon. made Lon. in
12	woo	83	82	17 38	35N.		8 49W 12 38W 16 25

Courles	Dift.	N.	S.	E.	W.
S b W 3 W	30		28.2		10.1
S 3 W	29		28.7		4.3
SIE	12		12.0	0.6	
S b W W	13		12.6		3.2
			81.5	0.6	17.6
					0.6
			1	Dep.	17.0

	Course ———— S. 12 00 W. Distance ————————————————————————————————————
	Diff. of Lat 82 S.
۱	Departure 17 W.
	Latitude by D.R. 38 35 N.
ı	Lat. by Observation
	Lat. by Observation Meridian Distance — 8 49W
	Longitude made -12 38W
	Longitude in 16 25W

Н	K	нк	F	Courfes	Winds	Lee-	Transactions, Saturday May the 17th, 1762.
2 4 6	3 3 3	1 1		SbWaw	W by N		Little Wind and fair Weather.
8 10 12	3 3 3						
2 4 6	3 2 3			S by W	w.		
8 10 12	3 3 3						Variation 4 Point W.erly.
Co	urfe	Dift	s	W Lat.	by D.R. L	at byO	b. Mer. Dift. Lon. made Lon. in
514	00 V	7 74	7	2 17 37	23N.		9 06 W 13 1W 16 48v

Courses	Dift.	N.	S.	E.	W.
SbyWiW	46		44.0		13.3
S 3 W	28		27.7		4.1
	Y. M	1340	71.7		17.4

By Course —— IS. 14 00 W.
Distance —— 74 Miles
Dist. of Lat.—— 72 S.
Departure —— 17 W.
Latitude by D.R. 37 23 N.
Latitude Observation
Meridian Distance 9 06 W.
Longitude made —— 13 01 W.
Longitude in—— 16 48 W.

Н	K	H	K	F	Courfes	Winds	Lee- way	Transactions, Sunday, May the 18th, 1762.
2	4	1			S by W	W byN		
4	4	1						Moderate Gales and Fair.
6	4	1						
8	4	1						
10	4	-		11			To Tomas	
12	4							
2	4	1			SbWww			
4	4			1 4				
6	. 4							
8	4	1						
10	4	1						Variation 4 Point W.erly.
12	1	1		1	and the second			

Courses	Dift.	N.	S.	E.	W.
S & W			47.5		7.0
S by W	48		47.1		9.4
	100		94.6		16.4

By	Courfe S. 10 00W.
D.R.	Diftance - 96 Miles
fince	Diff. of Lat. 95 S.
yefter-	Departure - 16 W.
day	Latitude D.R. 35 48 N.
Noon.	Latitude Obser. 35 36 N.

Now being to correct from the last Observation, which was on Wednesday, May 14th, I take the Northing, Southing, Easting and Westing for every Day since, and bring them into a Traverse Table as follows,

By D.R. fince the laft Observation.

N.	S.	E.	W.
7.1	74		14
	82		17
	72		17
	95		16
	N.	74 82	74 82

Gives Course by D.R. s. 323 Dep. 64 W. Gives Course by D.R. since last Observ. S. 11.00W.

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My Course found by D.R. since the last Observation, being S. 11 co W. which is less than 33 Degrees, I am to correct by Case the 2d, and to find every thing except the Distance, as follows.

First, For the true Difference of Latitude.

Take the Latitude last Observation			
And the Latitude by Observation To-day-	35	36	N.
Gives the Difference of Latitude	5	35	
Which multiplied by 60, makes -	33	5Mi	les.

Second, For the true Course.

The Course by D. R. since the last Observation, being S. 1100W. I set it down for the true Course, as per Rule in Case 2d.

Third, For the true Departure.

With the true Course 11 Degrees, and the true Difference of Latitude (divided by 2, because too big to be found in the Tables) which makes it 167.5, (by Plain Sailing, Case the 2d) I find the Departure 32.6 which multiplied by the same Number the Difference of Latitude was divided by, viz. 2, gives 65.2 Tenths for the true Departure.

Fourth, For the Meridian Distance.

Take the Meridian Distance last Observation -	8	18	w.
And the true Departure ——————	1	05	
Gives the Meridian Distance To-day	9	23	W.

Fifth, For the Difference of Longitude.

Take the Meridional Parts of last Ob	fervation —— 2716
And Meridional Parts of To-days Ob	Servation — 2288
Gives Meridional Difference of Latitu	de
With the Half of which -	

(because the whole is too big to be found in the Tables) and the True Course 11 Degrees, I find the Difference of Longitude 41.6, which doubled because the other was halv'd gives for the whole Difference of Longitude 83 Miles.

My

on and able

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Sixth

(-3T)	
Sixth, For the Longitude made,	
Take the Longitude made last Observation ————————————————————————————————————	— 11 56 W
Gives the Longitude made ———————	- 13 19 W
Seventh, For the Longitude in,	
Take the Longitude in last Observation ————————————————————————————————————	15 43 W
Gives the Longitude in	
Course — S. 11 00 W. Distance — 335 S. Departure — 65 W. Latitude by D. R. — 35 48 N. Latitude by Observation 35 36 N. Meridian Distance — 9 23 W. Longitude made — 13 19 W. Longitude in — 17 06 W.	S. 9 00 W. 108 Miles 107 S. 17 W.
The Course, Difference of Latitude and Departure what has been made since the last Observation (whi ago) and as it is usual to set them down only as they a Noon to Noon, therefore they are to be rubb'd out, a as follows; First, Take the Latitude by D. R. Yesterday And the Latitude by Observation To-day	ch was 4 Days are made from nd found again
Gives the Difference of Latitude	- I 47
Second, Take the Meridian Distance Yesterday — And the Meridian Distance To-day ————————————————————————————————————	- 9 06 W. - 9 23 W.
Gives the Departure —————————	0 17

Then with the Difference of Latitude 107, and the Departure 17 Miles, (by Plain-Sailing, Case 6.) I find the Course to be 9 Degrees, Distance 108 Miles as above.

S. 19 00W. 213 Miles

H	K	нк	F	Courfes	Wind	Lee	
2	5			S by W	N.		By Reckoning I make
4	5 6	1					my Course from the Start to the Island of Madera,
6	. 6	1				_	S. 32 00 W. Distance 420
8	7						Leagues; Meridian Dif-
10	7	1					tance and Difference of
12	8	!	_		-		Longitude as underneath.
2	8						
6	8 8	1					At Noon faw the Island
-8		1 1	+	-	-		of Madera, bearing S.W.
10		1.	-				by W. Distance 14 Leag. Variation oo.
12	9						Variation 60.
\$19		21		2 70 32			Ob. Mer. Dift. Lon. made Lon. in 10 33W 14 43W 18 30
	y W			178.5		35.5	Course - S. 19 00V
The state of the s	by W			23 3	-	34.9	Distance 213 Mil
!				201.8		70.4	Diff. of Latitude 202 S.
7	he B	earing		f the L	•		Departure — 70 W. Latitude by D.R. 32 14
SW	by	W. di	fta	nt 14 L	eagues.	or	Latitude by D.R. 32 14 Meridian Distance 10 33
42	Miles.		the	em in th			Longitude made 14 43 \\ Longitude in — 18 30 \\
and	Dift	ance t	he	Ship has	s made	by R	the Land, to find what Cou eckoning from the Place fai e done as follows.

CASE the First, When you keep the Account of Longitude in,

With the Latitude and Longitude of the Place you fail'd from; and the Latitude and Longitude you are in by your Reckoning, on the Day you make the Land, find the proper Difference of Latitude, the Meridional Difference of Latitude, and the Difference of Longitude in Miles, and with them find the Course and Distance (as it is shewn at large in Mercator's Sailing) Case the First, Page 55.

CASE

re 17

grees,

CASE the Second, When you keep the Account of Longitude made.

Then the proper Difference of Latitude, and the Meridional Difference of Latitude, are to be found as before, and the Difference of Longitude is to be found by bringing the Longitude made into Miles, with which proceed as in Case the First.

The Agreement between these two Ways may be seen as follows.

On the 19th of May, when I made the Land, my Longitude in was ______18 30 W. Longitude of the Start or

Place I fail'd from 3 47 E.

The Diff. of Longit. 14 43

Which multiplied by — 60

Makes --- 883 Miles

On the same Day my Longitude made was — 14 43 W. Which multiplied by — 60 Makes the Diff. of Lon. 883 Miles the same as in the other Case.

To find the Bearing and Distance of any Place from the Ship, upon any given Day.

Example. Suppose I would know how Madera bore off me, and what Distance on the 14th of May, by the foregoing Journal.

First, Supposing I kept only the Account of Longitude in,

Then, with the Latitude in 41 11 N.

And the Latitude of Madera 32 44 N.

I find the proper Diff. of Lat. 8 27

Which multiplied by 60 makes 507

Which multiplied by 60 makes 507

M. D. L.

And with Lon. in -15 43W.

And the Lon. Madera 17 26W.

I find the Diff. Lon. 1 43

Which makes — 103 Miles.

Then with that Meridional Difference of Latitude, and Difference of Longitude, I find the Course to be S. 09 00 W. and the Distance 510 Miles, (as in Mercator, Case 1.)

But if I had kept only the Account of Longitude made, (which is

Difference of Longitude) Then,

With the Longitude sail'd from _____ 3 47 W.

And the Whole Diff. of Lon. or Lon. made ____ 11 56 W.erly

Pu the Pulse for Longitude (Page 107) L

By the Rules for Longitude (Page 107) I

should have found the Lon. in to be ____ 15 43 W.

And then I have given the Latitude and Longitude in, &c. as before. I have in the foregoing Journal shewn how to Correct either for a single Day, or for a longer Time, and given Examples of every Case, for correcting from one Observation to another; but as it may happen that you may be some Days at Sea, from the Time of your leaving

leaving the Land before you have an Observation, and that when you get that first Observation you may have Occasion to Correct, (and there being much the same Difference between working the Correction from one Observation to another; and between the first Observation and the Land, as there is between working the first Day's Work and any of the following ones) I shall here give an Example from the foregoing Journal.

To Correct from the Time of leaving the Land, to the First Observation.

Example. Suppose that in the foregoing Journal, on the 3d of May, I was by Observation in the Latitude 45 10 N. my Latitude by DR, being 45 23 N. my Southing by D.R. 95. and Westing 24.

Now being to correct, and having no Observation before To-day, I must correct from the very Beginning of my Journal, that is, from the Time of my leaving of the Land, by bringing the Northing, Southing, Easting and Westing, (for every Day I have been at Sea) into a Traverse-Table as follows.

By D.R. from the Time of leaving the Land

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W.

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	N.	S.	E.	W.
On the first Day.		93		53
On the Second Day.		96		61
On the Day I correct.	1	95		24
Whole Diff. of Lat. by D.	R. S. 2	84 De	ер. 13	8 W

Gives the Course by D.R. from the Time of leaving the Land S. 26.00 W.

The Course found by D.R. from the Time of leaving the Land, being less than 33 Degrees, I am to correct by Case the Second, and to find every thing except the Distance, as follows.

First, For the true Difference of Latitude.

Take the Latitude of the Place sail'd from 50 07 N. And the Latitude in by Observation — 45 10 N.

Gives the true Difference of Latitude - 4 57 or 297 Miles.

Second, For the true Courfe.

The Course by D.R. since the Time of leaving the Land being S. 26 00 W. I set down for the true Course, as per the Rules for correcting, Case 2d.

Third

Third, For the true Departure,

With the true Course 26 Degrees, and half the true Difference of Latitude 148.5, (because the whole is too big to be found in the Tables) by Plain Sailing, Case the 2d. I find the Departure 72.3, which being doubled (because the Difference of Latitude was halv'd) gives 144.6 for the true Departure.

Fourth, For the Meridian Distance,

Whenever you correct from the Time of your leaving the Land, (as you do here) the Meridian Distance will always be the same as the true Departure found by correcting, which in this Case is 145 Miles, or 2.25 W.

Fifth, For the Difference of Longitude,

Take the Meridional Parts of the Latitude fail'd from 3485 And of the Latitude in by Observation - 3044 Gives the Meridional Difference of Latitude _____ 441

(because the whole is too big to be found in the Tables) and the true Course 26 Degrees, (as directed in the first Day's Work, p. 124) I find the Difference of Longitude 107.4, which doubled because the other was halv'd gives the true Difference of Longitude 214,8.

Sixth, For the Longitude made,

Whenever you Correct from the Time of your leaving the Land, (as you do in this Case) then the Longitude made will always be the fame as the whole Difference of Longitude found by the Correction, which in this Case is 215 Miles, or 3.35 W.

Seventh, For the Longitude in,

Take the Longitude of the Place you fail'd from — 3 47 W.

Gives the Longitude in ——— -

The Course, Difference of Latitude and Departure as above, being what has been made in the whole, from the Time of leaving the Land (which is three

Days)

159)

Days) and it is usual to set them down only as they are made from Noon to Noon, therefore they are to be rubo'd out, and found again as follows.

First, Take the Latitude by D. R. Yesterday — — — And the Latitude by Observation To-day — — —				46			
	e Difference of Latitude				-	48	

Second, Take the Meridian Distance Yesterday - - 1 54 W. And the Meridian Distance To-day --- 2 25 W. Gives the Departure -----

Then with the Difference of Latitude 108, and the Departure 31 Miles, (by Plain Sailing, Case 6) I find the Course to be S. 16 00W. Distance 113 Miles, as above.

Having in the preceeding Journal shewn how to find what Latitude and Longitude the Ship is in, on any Day, I shall in the next Place shew how,

By that Latitude and Longitude in, to prick off the Place of the Ship on the Mercator's-Chart.

Lay a Ruler a-cross the Chart, in the Latitude your Ship is in, then look upon the Equinoctial, or Line marked with the Degrees of Longitude, for the Longitude your Ship is in by your Reckoning, and fetting one Foot of your Compasses in that Longitude, take the nearest Distance to some North and South Line, and from where that Line crosses the Edge of the Ruler that lays in the given Latitude, lay off that same Distance (by the Edge of the Ruler) to the Right-hand, if the Longitude you are in was to the Right hand of the North and South Line: Or to the Left-hand if it was to the Left, where this falls will be the Place of the Ship. But this will only do when the Longitude mark'd on the Chart and your Reckoning of Longitude in, are both counted from the same Meridian, therefore for a general Rule take the following, viz.

By the Latitude in, and Longitude made, to prick off the Ship's Place, &c.

Rule. Set one Foot of your Compasses in the Place you take your Departure from, and take the nearest Distance to some North and South Line, and from where that Line falls upon the Equinoctial, or Line mark'd with the Degrees of Longitude, set off that Distance, the same way as the Place lays from it, (that is, to the Right-hand, if the Place lay to the Right-hand of the North and South Line, or to the Left-hand if it lay to the Left) and make a Mark with a Black Lead Pencil; this Mark will ferve to prick off by, till you come to take a New Departure, and then you rub it out, and make a new one, as before.

Then lay a Ruler a-cross the Chart in the Latitude you are in, and taking so many Degrees in your Compasses (from the Line of Longitude) as your Longitude made comes to, set them off from your Black Lead Mark, to the Eastward, if the Longitude made be East, or to the Westward if it be West;

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where this falls will be the Longitude the Ship is in by the Chart, from which take the nearest Distance to some North and South Line, and from where that Line, &c. as in the first Case.

The Ship's Place on the Chart being found as before taught; it remains in the next Place to shew how to find the Bearing and Distance of any Place from

the Ship; and First,

To find bow any Place bears from the Ship.

Rule. Lay a Ruler from the Place of the Ship, to the Place you would know the Bearing of, then set one Foot of your Compass in the Center of some Compass near the Ruler, and take the nearest Distance to the Edge of the Ruler; then run one Foot of your Compasses along by the Edge of the Ruler, and observing what Point of the Compass the other comes nearest to, which will be the Bearing required.

To find the Distance of any Place from the Ship.

Case the 1st, If the Place be in the same Longitude that the Ship is in, (that is, if it bears due North or due South) then the Difference of Latitude between them, (found as by the Rules for Latitude, Page 105) and turn'd into Miles of Leagues will be the Diffance.

Case the 2d, If the Place be in the same Latitude that the Ship is in, (that is if it bears due East or due West) then take half the Distance between the Shi and the Place, in your Compasses, and setting one Foot (on the Line mark' with the Degrees of Latitude) in the Latitude the Ship is in, see what Latitude the other Foot will reach to, both above and below it; the Difference between these two Latitudes, (found as per Rules for Latitude) will be the Distance required.

Case the 3d, If the Place be neither in the same Latitude nor Longitude with the Ship, then take the Difference of Latitude between them in Degrees, from the Equinoctial-line, and laying a Ruler from the Ship to the Place, apply on Foot of the Compasses so to the Edge of the Ruler, that the other Foot turn' about may just touch some East and West Line, that is cross'd by the Ruler then take the Distance along the Edge of the Ruler, from the Place where the Compasses rested, to the Place where the Ruler crosses the said East and West Line; that Distance measured on the Equinoctial, or Degrees of Longitude will give the Distance in Degrees, which you may turn into Miles or Leagues and in the same manner as you find the Bearing and Distance of any Place from the Ship; you may also find the Bearing and Distance of one Place from another

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n, (that is, n the Ship ne mark'd tLatitudes e between e Distance

rees, from apply one oot turn'd the Ruler, where the and West Longitude, r Leagues, Place from manother.